FRENETTE GARDENS

SB# 03-22 CU #05-22 STAFF REPORT #2

June 22, 2022

(See May 25, 2022 Report for previous comments)

SITE: 65 Central Street; Map 182 Lot 3

ZONING: Town Residential (TR)

PURPOSE OF PLAN: To show a proposed ten lot subdivision and 705 linear feet of a new dead end roadway.

PLANS UNDER REVIEW:

- Residential Subdivision Plan, Frenette Gardens, Map 182; Lot 3, 65 Central Street, Hudson, New Hampshire; prepared by: Keach-Nordstrom Associates, Inc., 10 Commerce Park North, Suite 3B, Bedford, NH 03110; prepared for: Laura Ripaldi, 46 Bush Hill Road, Hudson, NH 03051 & Kimberly Frenette, 88 Dumont Road, Hudson, NH 03051 & Ricky Frenette, 14 Tate Street, Hudson, NH 03051; consisting of 16 sheets and an additional cover sheet, and general notes 1-22 on Sheet 1; dated April 20, 2022, last revised June 6, 2022.
- Wetland Buffer Impact Plan, Frenette Gardens, Map 182, Lot 3, 65 Central Street,
 Hudson, New Hampshire; prepared by: Keach-Nordstrom Associates, Inc., 10 Commerce
 Park North, Suite 3B, Bedford, NH 03110; prepared for: Laura Ripaldi, 46 Bush Hill
 Road, Hudson, NH 03051 & Kimberly Frenette, 88 Dumont Road, Hudson, NH 03051 &
 Ricky Frenette, 14 Tate Street, Hudson, NH 03051; consisting of a single sheet and
 construction notes 1-8, dated April 15, 2022, last revised June 6, 2022

ATTACHMENTS:

- A. Applicant's Response to Peer Review, dated June 6, 2022.
- B. Conservation Commission recommendation dated June 13, 2022.
- C. CAP Fee Worksheet.
- D. Stormwater Management Report revised June 6, 2022 (provided digitally only)

APPLICATION TRACKING:

- April 28, 2022 Application received.
- May 9, 2022 presentation to Conservation Commission
- May 12, 2022 Conservation Commission conducted a site walk
- May 25, 2022 Planning Board public hearing scheduled, application accepted, continued to June 22, 2022. Waiver from § 289-37.A, phased schedule granted.
- June 9, 2022 Planning Board site walk.

- June 13, 2022 Second meeting with Conservation Commission, recommendation issued.
- June 22, 2022 Continuance scheduled.

COMMENTS & RECOMMENDATIONS:

RESPONSE TO PEER REVIEW

See Attachment A for the Applicant's revisions in response to peer review. Staff has also reviewed the changes with the Peer Review consultant and the Applicant's engineer and has found the revised plan set adequately addresses all comments.

Comment 8.a of the Peer Review stated that an Alternation of Terrain (AOT) and a Wetlands permit will be required. Staff clarified this with the Peer Reviewer who stated they mean to say "may" require AOT if disturbance exceeded 100,000-sf, which the plan does not. Also, by "Wetlands permit" the Peer Reviewer meant the Conditional Use Permit from the town that is part of this application.

CONDITIONAL USE PERMIT

The proposed development requires a Wetlands Conservation Conditional Use Permit for the proposed sewer connection and for a drainage improvement (level spreader). The Conservaion Commission first heard the application on May 9, 2022 followed by a site walk on May 12, 2022 and issued a recommendation at their June 13, 2022 meeting (**Attachment B**). The Commission concluded that the proposed is a minor impact to the buffer and poses no issues with any wetlands or the Brook, and complies with §334-36.C(2) and §334-36.A(2). The Commission also noted the potential for erosion during post construction stabilization and accordingly made recommendations for erosion control. Recommended conditions of approval by the Commission are provided in the Draft Motions section of this report.

ADDITIONAL COMMENTS

Staff recommends the Board determine the desirability of the street light place midway into the proposed neighborhood. The only street light type currently carried by the town is an LED "cobra" light shown in the image below. While this type might be appropriate along highways and corridors, some might not consider it palatable in a small neighborhood context. A more suitable location for the town light type might be at the intersection created by the proposed street.



Figure 1 - Town Streetlight

Staff has asked the Applicant's engineer to consider the possibility of providing a pedestrian easement off of the end of the proposed cul-de-sac through proposed Lot 3-6 in the vicinity of

the former rail-bed. The Town currently controls the former rail-bed from Merrill Park to Gillis Street. Note that in order to complete the connection an additional easement would be required in the vicinity of the existing sewer easement between Gillis Street and the subject lot. The purpose of this suggestion is to further opportunities to improve pedestrian facilities and recreation, a goal noted in the 2006 Master Plan as well as during public outreach for the ongoing update.

Last, it is recommended that "Active & Substantial Development" be defined between the Applicant and the Board as part of a potential approval.

DRAFT MOTIONS

CONTINUE the public hearing to a date certain:

	1 11	lication, CU #05-22, and the subdivision Central Street Map, 182 Lot 3, to date cert	tain
, 2022		contail Street Map, 102 Lot 3, to date cont	, airi
Motion by:	Second:	Carried/Failed:	

APPROVE the subdivision plan application:

I move to approve the conditional use permit and subdivision plans entitled: Residential Subdivision Plan & Wetland Buffer Impact Plan, Frenette Gardens, Map 182; Lot 3, 65 Central Street, Hudson, New Hampshire; prepared by: Keach-Nordstrom Associates, Inc., 10 Commerce Park North, Suite 3B, Bedford, NH 03110; prepared for: Laura Ripaldi, 46 Bush Hill Road, Hudson, NH 03051 & Kimberly Frenette, 88 Dumont Road, Hudson, NH 03051 & Ricky Frenette, 14 Tate Street, Hudson, NH 03051; consisting of 16 sheets and an additional cover sheet, and general notes 1-22 on Sheet 1; and Construction Notes 1-8 on Sheet 1 of the Wetland Buffer Impact Plan; dated April 20, 2022, last revised June 6, 2022; subject to, and revised per, the following stipulations:

- 1. All stipulations of approval shall be incorporated into the Development Agreement, which shall be recorded at the HCRD, together with the Plan.
- 2. The Planning Board finds that the Stormwater Management Report, last revised June 6, 2022, complies with the requirements of §290 Stormwater Management.
- 3. All improvements shown on the Plan, including Notes 1-22 on Sheet 1 of the Subdivision Plan and Construction Notes 1-8 on Sheet 1 of the Wetland Buffer Impact Plan, shall be completed in their entirety and at the expense of the applicant or the applicant's assigns.
- 4. A cost allocation procedure (CAP) amount of \$5,991 per single-family residential unit, shall be paid prior to the issuance of a Certificate of Occupancy.
- 5. All monumentation shall be set or bonded for prior to Planning Board endorsement of the Plan-of-Record.

- 6. Approval of this plan shall be subject to administrative review by the Town Planner and Town Engineer.
- 7. Construction activities involving the proposed undeveloped lots shall be limited to the hours between 7:00 A.M. and 7:00 P.M., Monday through Saturday. No exterior construction activities shall occur on Sundays.
- 8. A pre-construction meeting shall be scheduled with the Town Engineer prior to construction.
- 9. Utilities shall be underground.
- 10. During construction and restoration erosion control barriers shall be installed and maintained to the satisfaction of the Town Engineer. A two layer erosion control barrier should be employed in the construction areas along First Brook.
- 11. The commission recommends that a stipulation and or note be added to the Erosion and Sediment Control Plan that states "Erosion control blankets shall be used as part of slope stabilization after construction".
- 12. The Town Engineer or his representative shall be allowed to inspect the boundaries of the wetland and wetland buffer areas during construction and report any finding to the applicant and the Conservation Commission for remediation.
- 13. The commission recommends that a stipulation and or note be added to the final plan set that states "Stockpiling of construction materials is not allowed in the Wetland Buffer Area".
- 14. The commission recommends that a stipulation and or note be added to the final plan set that states "The wetland buffer boundary shall be identified and marked prior to the start of construction per Hudson Zoning Ordinance, Article IX §334-35 (E.)
- 15. The commission recommends that a stipulation and or note be added to the final plan set that states "No Cut/No Disturb" signage shall be installed along the edge of the wetland buffer boundary of Lots 3-7, 3-8 and 3-9 prior to issuing Certificates of Occupancy per Hudson Zoning Ordinance, Article IX §334-35 (E.)
- 16. This motion is based on the plan(s) submitted by the applicant. It is recommended that if additional impacts are required the plan be returned to the Conservation Commission for further review.

17. For tl	ne purposes of this subdivision pla	an, the term "active and substantial develop	ment" shall
mean	·		
Motion by:	Second:	Carried/Failed:	



KEACH-NORDSTROM ASSOCIATES, INC.

June 6, 2022

Mr. Steven W. Reichert, P.E. Fuss & O'Neill 50 Commercial Street #2S Manchester, NH 03101

Subject:

Frenette Gardens

65 Central Street

Hudson, New Hampshire KNA Project No. 21-0928-1

Dear Mr. Reichert:

We are in receipt of your comments pertaining to the subject project dated May 13, 2022. On behalf of our client, please find attached to this cover revised plan sheets and updated support documents, which we believe serve to address your comments as noted below:

1. Administrative and Subdivision Review Codes (HR 276 & HR 289)

a. Hudson Regulation HR 276-11.1.B.(6). The owner's signature was not provided on the plan set; however, a space was provided for their future signatures.

The owner's signature will be included on the final plans.

b. HR 276-11.1.B.(13). The applicant has not shown any sign locations or details on the plan set other than traffic signs.

No comment.

c. HR 276-11.1.B.(14). The applicant has shown one proposed streetlight on the plan set approximately three feet from the curb line. It is not noted on the plans or in the application documents that the proposed street right-of-way will be public and the responsibility of the Town to maintain. The applicant should confirm that the proposed right-of-way will be public and that the proposed light model is acceptable to the Town for this location and for maintenance responsibilities.

The project does propose to make this a public right-of-way, which is now noted under the street name throughout the set. DPW has reviewed the plans and has not noted any issues with the proposed street light design and layout.

d. HR 276-11.1.B .(14). We note that there are existing street lights on the utility poles on both sides of the proposed street intersection with Central Street, located 80' and 107' from the proposed street centerline. The applicant should confirm that these

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lights will provide enough illumination for drivers to see pedestrians at the proposed crosswalk at night.

Central Street is a well-lit existing street, that promotes public safety. Adequate lighting for both the proposed crosswalk and the overall development has been adequately provided.

e. HR 276-11.1.B.(15). The applicant has not shown any buildings within 50 feet of the site.

Buildings within 50 feet are now shown on the plans (see Sheets 1-4).

- f. HR 276-11.1.B.(16). The applicant has not included information on driveways and travel ways within 200 feet of the site.
 - A GIS image, which shows existing features within 2,000 feet of the site has been added to the cover sheet.
- g. HR 276-11.1.B.(17). & 289-27.B.(7). The applicant has not provided any benchmark information.
 - A benchmark using a granite bound has been added to the plan (see Sheet 5).
- h. HR 276-11.1.B.(20). The applicant has not noted existing building heights on the plan set.

The highest building on site is the existing barn which, at its peak, is approximately 38 feet high. Please see Note #3 on Sheet 1.

- i. HR 276-11.1.B.(20). The applicant has shown an existing sewer easement on the plans. Several utility easements are proposed and shown on the plans. Copies of these easements were not included in the review package.
 - A copy of the existing sewer easement is attached to this letter. Additionally, draft copies of the proposed easements are being prepared and will be submitted to the town for review shortly.
- j. HR 289-15. & 334-83. The applicant had noted that the site is partially located in the flood hazard area. The applicant has delineated this area on the plan set and we note that it is not within the area proposed for development of the road or new lot areas.

No comment.

k. HR 289-17.C. The applicant should review the front eastern corner of proposed lot 3-7 as it appears to intersect the front lot at an angle of less than 45 degrees.

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An additional segment has been added to the lot line so that it intersects the front lot line at an angle of 45 degrees. The subdivision plans and lot areas have been updated accordingly.

1. HR 289-22. The applicant has not proposed any specific open spaces on the plan set. Per the Regulation the Planning Board shall review the plan for open space requirements, which shall generally consist of 10% or less of the total area, and if required this open space shall be deeded to the Town of Hudson and be so indicated on the final subdivision plan.

The area to the south of Limit Brook is unsuitable for development and will be left as open space. The landowners are considering options for granting the town a conservation easement over this land. They will continue to work with staff to determine if this is a direction they would like to go.

m. HR 289-26.B.(5). The applicant has not shown the Right-of-Way width of the existing streets on the plan set.

Existing streets ROW width has been added to the plans (see Sheets 1-4).

n. HR 289-28.A. The applicant should provide a detail for the proposed granite bounds to be set.

Information regarding granite bounds can be found on Note #12 on Sheet 1.

o. HR 289-37.A. The applicant has requested a waiver from the Regulation for phasing of subdivision construction to minimize the disturbance to the abutting parcels.

The planning board voted to grant said waiver at the May 25, 2022 hearing. The waiver note has been updated to reflect this.

2. Driveway Review Codes (HR 193-10)

a. HR 193-10.A. & 193-10.E. The applicant has provided sight distance information for the proposed roadway at the Central Street intersection on the plan set.

No comment.

3. Roadway Design

a. HR 289-18.B.(3). The applicant has proposed a cul-de-sac curb radius of 64 feet and the Regulation requires a minimum of 65 feet.

The cul-de-sac curb radius has been increased to 65 feet to meet the requirement. Additionally, the alignment and edge of pavement have been revised accordingly (see Sheet 5).

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b. HR 289-18.B.(5). The applicant should add a dead-end informational sign to the plan set and a detail for the sign.

A dead-end sign and detail have been added to the plan set (see Sheets 5 & 11).

c. The proposed stop bar at the intersection with Central Street is shown as less than two feet from the crosswalk. A four-foot separation distance is recommended for this location.

The stop bar has been relocated as recommended.

d. The applicant should provide a crosswalk striping detail in the plans.

A crosswalk striping detail has been added to Sheet 11.

e. The applicant should provide a curb ramp construction detail in the plans.

Curb ramp details have been added to Sheet 11.

f. The applicant has proposed a 6.5-foot-wide grass panel between the road and sidewalk. The Town's standard detail requires a five-foot grass panel. The applicant should confirm with the Town that the wider grass panel is acceptable.

The grass panel has been reduced to 5 feet in the typical ROW and 3.5 feet in the culde-sac ROW based on similar comments from the town engineer. The typical roadway section detail on Sheet 11 has been updated accordingly.

- 4. Drainage Design /Stormwater Management (HR 289-20.C. /Chapter 290)
 - a. HR 289-20.C.3. & 290-5.A.9. The applicant should provide test pits located within the footprint of Proposed Infiltration Trenches #1 and #2. Verification of the infiltration rate, SHWT, and ledge is required to ensure long term functionality of the infiltration practice. We note Infiltration Trenches #1 and #2 do not account for treatment, as it appears was the design intent.

Test pits are currently scheduled for Friday, June 10 to be performed in the vicinity of the proposed trenches. All data will be added to the plans ASAP.

b. HR 290-5.A.1. & 290-5.A.3. The applicant should provide language in the Drainage Analysis Report, stating if and how low impact development (LID) strategies for stormwater runoff were evaluated for this project.

The proposed subsurface stormwater system was designed as the first of its kind as part of a pilot program in Hudson, requested by DPW. The intent is to move away

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from intrusive large-scale open detention systems and replace them with less disruptive subsurface systems. This has been noted in the revised drainage report (see attached). Furthermore, all proposed BMPs are considered Low-Impact Development strategies as they utilize infiltration to reduce the volume of stormwater runoff discharged from the site.

c. HR 290-5.A.12. The applicant should provide information on the maintenance of the proposed drainage system and if a homeowner's association is to be created for that purpose. The plans and application documents do not indicate if the proposed right-of- way will be a public way with Town maintenance.

The applicant has proposed drainage and maintenance easements for the benefit of the town of Hudson to maintain the infiltration trenches. Also, the ROW is proposed as public so the town will be able to maintain the underground system.

d. HR 290-6.A.8. We note the requirement of the applicant to coordinate a preconstruction meeting with the Town Engineer.

No comment.

e. HR 290-7.A.6. The applicant should provide information as to how the stormwater system is designed to account for frozen ground conditions of the infiltration trenches as the subsurface system is below the frost line.

A separate HydroCAD model has been developed to demonstrate how the infiltration trenches will operate under frozen ground conditions (see attached). This model does not include infiltration as an outlet for either pond node, which simulates what could happen when the ground is frozen. As the model indicates, neither trench is overtopped in the 50-year storm event. This information has been added to the Stormwater Management Report as well.

f. HR 290-8.A.4. & 5. We note the requirement of the applicant to coordinate the need for a Bond or Escrow with the Town Engineer.

No comment.

g. HR 290-10.A. We note that disturbance, tree clearing/stumping, and grading greater than 100,000 sf disturbance may require an NHDES AoT permit.

The limit of work was evaluated at the start of this project. It was determined to be under the 100,000-sf threshold, which does not necessitate an AoT permit.

h. Engineering Technical Guideline & Typical Details (ETGTD) 920.3.13. The applicant has proposed storm drains that are below the listed minimum velocity of Civil Engineering

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2.0 fps. We note that although it is self-cleaning velocity, it does not meet the regulations.

The slope of the 12" HDPE out of DCB#70 has been increased to 2.00% to ensure that a minimum velocity of 2.0 fps is met. The plans and drainage report have been revised accordingly (see attached).

i. The applicant will be required to comply with all provisions of the Town of Hudson's MS4 permit, including but not limited to annual reporting requirements, construction site stormwater runoff control, and record keeping requirements. The applicant has noted that the project meets 2019 MS4 requirements.

No comment.

j. Please note that this review was carried out in accordance with applicable regulations and standards in place in New Hampshire at this time. Note that conditions at the site, including average weather conditions, patterns and trends, and design storm characteristics, may change in the future. In addition, future changes in federal, state or local laws, rules or regulations, or in generally accepted scientific or industry information concerning environmental, atmospheric and geotechnical conditions and developments may affect the information and conclusions set forth in this review. In no way shall Fuss & O'Neill be liable for any of these changed conditions that may impact the review, regardless of the source of or reason for such changed conditions. Other than as described herein, no other investigation or analysis has been requested by the Client or performed by Fuss & O'Neill in preparing this review.

No comment.

5. Zoning (HR 334)

a. HR 334-14 and HR 276-11.1.B.(20). The applicant has not noted the maximum proposed building heights on the plan set. The applicant should note the maximum building height of 38 feet on the plan set.

As the plan is a conventional subdivision plan, it does not propose the construction of any buildings. Regardless, the maximum building height of 38 feet has been added to Note #3 on Sheet 1.

b. HR 334-20. The site is located in the Town Residence (TR) District. The applicant should provide a formal use note confirming that single family homes are the proposed use.

Please see Note #21 on Sheet 1.

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c. HR 334-27. We note that the subdivision design appears to meet the lot size requirements for the district. The applicant has included a table with calculations illustrating that each lot meets the contiguous lot requirements excluding wetland areas and slopes greater than 25%.

No comment.

d. HR 334-36.C. The applicant has noted in their application that a Conditional Use Permit has been filed for the drainage and sewer construction within the Wetland Conservation District.

Please see Note #22 on Sheet 1.

6. Sewer/Water Design/Conflicts & Utility Design/Conflicts (HR 276-13.E.)

a. HR 276-13. The applicant has proposed one fire hydrant within the site, and there is an existing hydrant approximately 180 feet from the proposed intersection on Central Street. The applicant should coordinate with the Hudson Fire Department to verify that there is adequate fire protection coverage for the proposed lots.

The Hudson Fire Department has reviewed the plans and has not requested an additional fire hydrant.

b. ETGTD Section 801. The applicant should verify with the Town that the existing water main in Central Street has adequate flow and pressure to meet both domestic and fire hydrant requirements for the proposed subdivision.

Both the Fire Department and Department of Public Works reviewed the plans and did not note the need for a hydrant flow test.

c. The applicant has not provided any typical details for water and sewer connections to the proposed lots.

Service connection details have been added to Sheets 14 and 15 accordingly.

d. The applicant has not shown utility service connections to the two small existing houses located within proposed lot 3, other than adjacent tank covers. The applicant should verify if these are septic tanks, or if these houses are already connected to the Town sewer system with the main house on that lot.

These buildings were not labeled correctly on the original plan. One is an existing chicken coop and the other is an existing greenhouse, neither of which require utility service connections. Labels have been added to the plan set for clarity,

e. The applicant is proposing four new sewer manholes within a space of less than 60 feet, included internal drop SMH #3 which is located within the steep slope down

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towards First Brook which will make maintenance difficult.

The town engineer has reviewed and accepted the proposed sewer design as proposed. Furthermore., a Sewer Connection Permit is currently under review by DES.

f. The applicant is proposing a drop over sewer manhole (SMH #1) for the connection to the existing sewer main adjacent to First Brook. The applicant should review this proposed installation with the Town to confirm that this is acceptable. Also, connection of the proposed sewer to the existing sewer manhole 15 feet upstream from SMH #1 would eliminate the need for this drop over manhole.

The town engineer originally requested this drop over manhole be installed in this location rather than coring into the existing manhole further upstream. After recent discussions with the state and town engineer, the sewer design has been revised to now core into said manhole rather than install a drop over manhole. The revised sewer layout can be found on Sheets 5 & 10.

g. ETGTD Detail S-3. The proposed internal drop sewer manhole doesn't quite match the Town of Hudson detail (cross used at inlet instead of Tee).

The previous detail has been replaced by the town detail (see Sheet 14).

h. The SMH#5 to Existing Sewer Main Profile should show the proposed water main that crosses the sewer at approximate station 1+95. The applicant should also include a water/sewer crossing detail in the plans.

The proposed water main has been added to the profile (see Sheet 10). Additionally, a water crossing detail has been added to Sheet 14.

i. ETGTD Detail R-5. The applicant has proposed a pavement repair detail that doesn't quite match the Town of Hudson detail (base courses should step out 12" beyond the trench width, pavement course cutbacks vary from the detail). The applicant should also coordinate with the Town to show the minimum required pavement depth for the patch across Central Street.

The previous detail has been replaced by the town detail (see Sheet 11).

7. Erosion Control/Wetland Impacts

a. HR 290-5.A.10. Due to the close proximity of the onsite wetlands, and as to avoid unwanted additional wetland impacts, we recommend that the applicant add a note stating that orange construction fence will be placed at all wetland buffers within 50-feet of proposed grading. This fence is recommended during build out, and kept up until the site is complete.

Note #11 has been added to Sheet 7 reflecting this recommendation.

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b. The Town should reserve the right to require additional erosion control measures.

No comment.

8. State and Local Permits

a. HR 290-10.A. The applicant has noted the need for a NHDES Sewer Connection permit on the plan. The applicant should list all required permits on the plan. We note that an Alteration of Terrain Permit and a Wetlands permit will be required also.

As disturbance is under 100,000 square feet, an AOT Permit is not required. Also, no disturbance to the existing wetlands is proposed therefore, no Wetlands Permit is required either.

b. HR 290-10.B. The applicant has noted the need for a NPDES Notice of Intent. The applicant should expand this to also note the need for a SWPPP on the plan set.

Note #16 on Sheet 1 has been expanded accordingly.

c. Additional local permitting may be required.

No comment.

9. Other

a. The applicant has shown a lot of design elements on the Roadway Plan. There are locations where lines and symbols are overwritten by other notes. We recommend that the applicant review the plan to more clearly show the information for ease of use by the construction contractor.

The plan has been revised to remove as many overlaps as possible.

b. ETGTD Section 565.1.1. The applicant is reminded that the Town of Hudson has specific requirements for the importing of off-site fill materials for use in constructing this project. We recommended that these requirements be stated on the plans for the Contractors attention.

Please see the additional notes on Sheet 5 stating the town requirements for importing off-site materials.

I trust you will find the attached revised plans and documents address all of your concerns as noted above. As always, should you have any additional questions or require further information, please do not hesitate to contact me directly.

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Respectfully,

Peter Madsen

Project Engineer

Keach-Nordstrom Associates, Inc.





TOWN OF HUDSON

Conservation Commission

William Collins, Chairman

Dave Morin, Selectmen Liaison

12 School Street ' Hudson, New Hampshire 03051 ' Tel: 603-886-6008 ' Fax: 603-816-1291

To: Town Planner, Brian Groth

Planning Board Chairman, Tim Malley

Date: June 13, 2022

Case: Conditional Use Permit for Frenette Gardens, 65 Central St.

Hudson, New Hampshire Map 182, Lot 003-000 Zone: Town Residential (TR)

Site Walk Observations and Conclusions

On May 12, 2022 members of the Hudson Conservation Commission conducted a site walk of property owned by the following individuals Laura Ripaldi, 46 Bush Hill Road, Kimberly Frenette 88 Dumont Road and Ricky Frenette 14 Tate Street (all of Hudson NH). The purpose of the site walk was to evaluate proposed permanent wetland buffer impacts at two locations that would be required as part of a planned 10 lot residential subdivision. Buffer impact area #1 requires that approximately 790 square feet is disturbed for the purpose of constructing an overflow system for the proposed storm water infiltration system. Buffer impact area #2 requires that approximately 1,450 square feet is disturbed to connect a new sewer line to an existing sewer line running through the property. If built as designed there will be a permanent wetland buffer impact of 2,240 sq.

The commission concludes that this is a minor impact to the wetland buffer area along First Brook and poses no issues with any wetlands or the brook itself and complies with Hudson Zoning Ordinance §334-36 C (2) and §334-37 A (2). The proposed sewer line connection point and proposed storm water management level spreader appurtenances are placed in areas that are already maintained periodically by the town of Hudson as part of an existing sewer line easement running through the property. With that said both impact sites are located in areas that exceed 25% grade and have a potential for extreme erosion during the post construction stabilization period. Redundant erosion control barriers should be employed in the construction areas to prevent silt and other materials from entering First Brook. Lastly, the commission recommends that Erosions Control Blankets be used over exposed soils of the buffer impact areas in place of standard seeding practices to further mitigate the possibility of excess erosion during unforeseen storm events.

HCC Recommendations to the Planning board as part of a Condition of Approval

After review of the actual site conditions and a post site walk meeting with Applicant's Representative on June 13, 2022 the Conservation Commission members ask that the Planning Board take into consideration the following recommendations.

- 1. During construction and restoration erosion control barriers shall be installed and maintained to the satisfaction of the Town Engineer. A two layer erosion control barrier should be employed in the construction areas along First Brook.
- 2. The commission recommends that a stipulation and or note be added to the Erosion and Sediment Control Plan that states "Erosion control blankets shall be used as part of slope stabilization after construction".
- 3. The Town Engineer or his representative shall be allowed to inspect the boundaries of the wetland and wetland buffer areas during construction and report any finding to the applicant and the Conservation Commission for remediation.
- 4. The commission recommends that a stipulation and or note be added to the final plan set that states "Stockpiling of construction materials is not allowed in the Wetland Buffer Area".
- 5. The commission recommends that a stipulation and or note be added to the final plan set that states "The wetland buffer boundary shall be identified and marked prior to the start of construction per Hudson Zoning Ordinance, Article IX §334-35 (E.)
- 6. The commission recommends that a stipulation and or note be added to the final plan set that states "No Cut/No Disturb" signage shall be installed along the edge of the wetland buffer boundary of Lots 3-7, 3-8 and 3-9 prior to issuing Certificates of Occupancy per Hudson Zoning Ordinance, Article IX §334-35 (E.)
- 7. This motion is based on the plan(s) submitted by the applicant. It is recommended that if additional impacts are required the plan be returned to the Conservation Commission for further review.

Mr. Dickinson moved to forward recommendations 1 through 7 above to the Planning Board for their consideration as Conditions of Approval for the Conditional Use Permit application submitted for Frenette Gardens, 65 Central Street, Hudson.

Motion Second Mr. Pinsonneault Motion carried 4/1/0 Commission member Saundra Rumbaugh voted against the recommendations stating the project pose undue stress on the First Brook watershed

William Collins

William Collins, HCC Chairman



TOWN OF HUDSON

OPPORATED TO

Planning Board

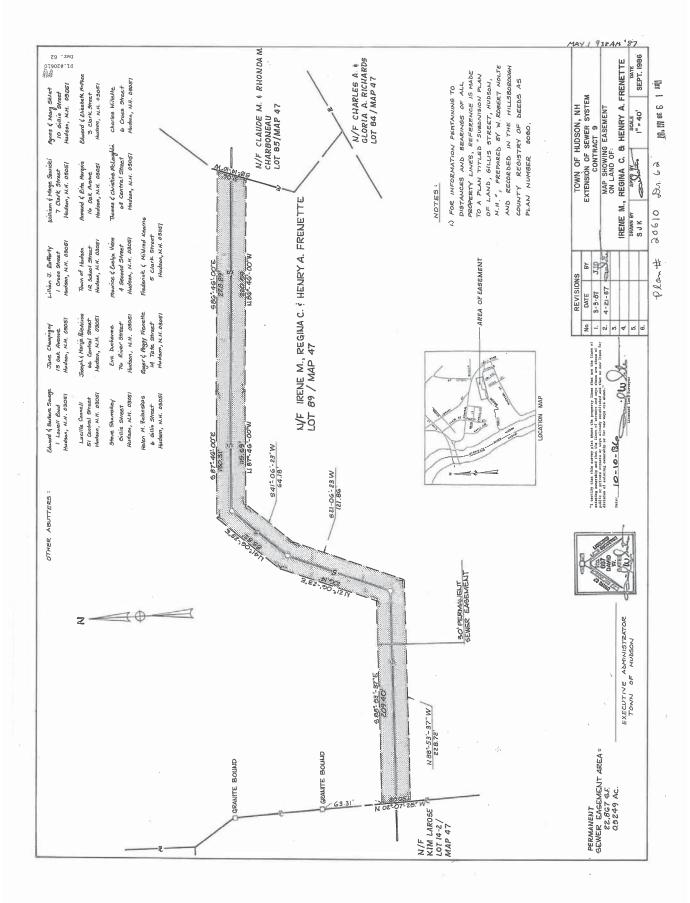
Timothy Malley, Chairman

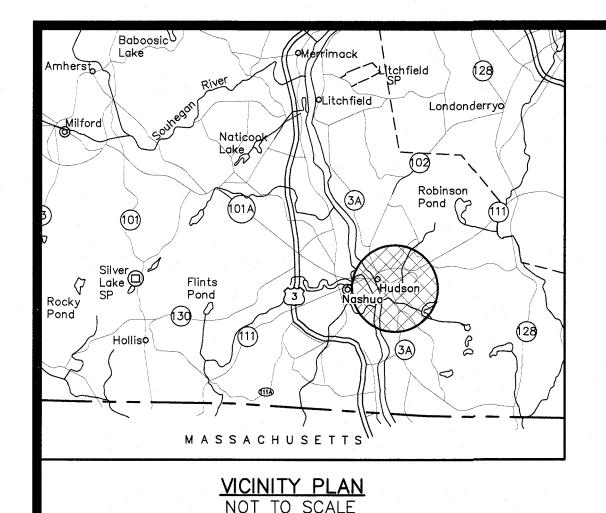
12 School Street · Hudson, New Hampshire 03051 · Tel: 603-886-6008 · Fax: 603-594-1142

CAP FEE WORKSHEET - 2022

Date:	06-16-22 Z	one # <u>1</u>	Map/Lot: _	182	2/003	_
	Name: Frene			65 Ce	entral Street	t
Propose	ed ITE Use #1:	Single Family	Residential Lo	ot		
Propose	ed Building Area	(square footage)	:	N/A		<u>S.F.</u>
CAP FI	EES: (ONE CHE	CK NEEDED)				
1.	(Bank 09) 2070-701	Traffic Impr	ovements	\$	2,013.00	
2.	(Bank 09) 2050-182	Recreation		<u>\$</u>	400.00	
3.	(Bank 09) 2080-051	School		\$	3,578.00	
		Total CAP F	ee	\$	5,991.00	

Check should be made payable to the **Town of Hudson**.

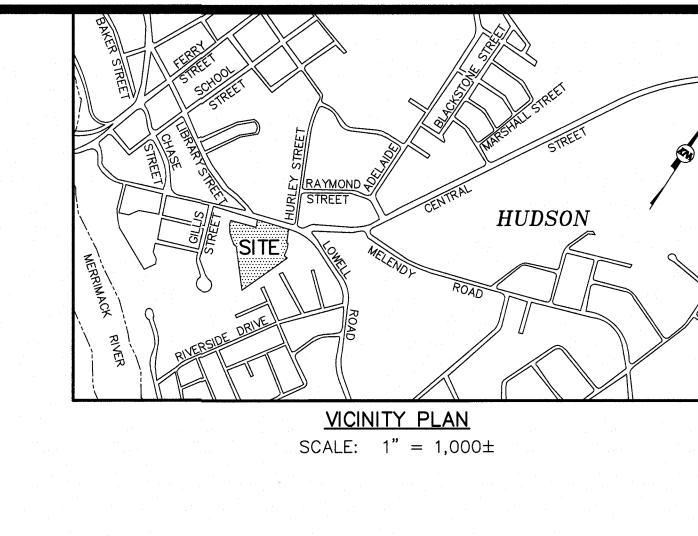


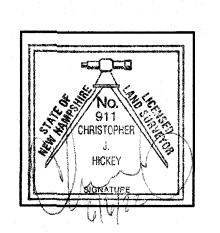


RESIDENTIAL SUBDIVISION PLAN FRENETTE GARDENS

MAP 182; LOT 3

65 CENTRAL STREET HUDSON, NEW HAMPSHIRE







NOT TO SCALE



APRIL 20, 2022 LAST REVISED: JUNE 6, 2022 PROJECT NO. 21-0928-1

OWNERS/APPLICANTS: LAURI RIPALDI 46 BUSH HILL ROAD HUDSON, NH 03051

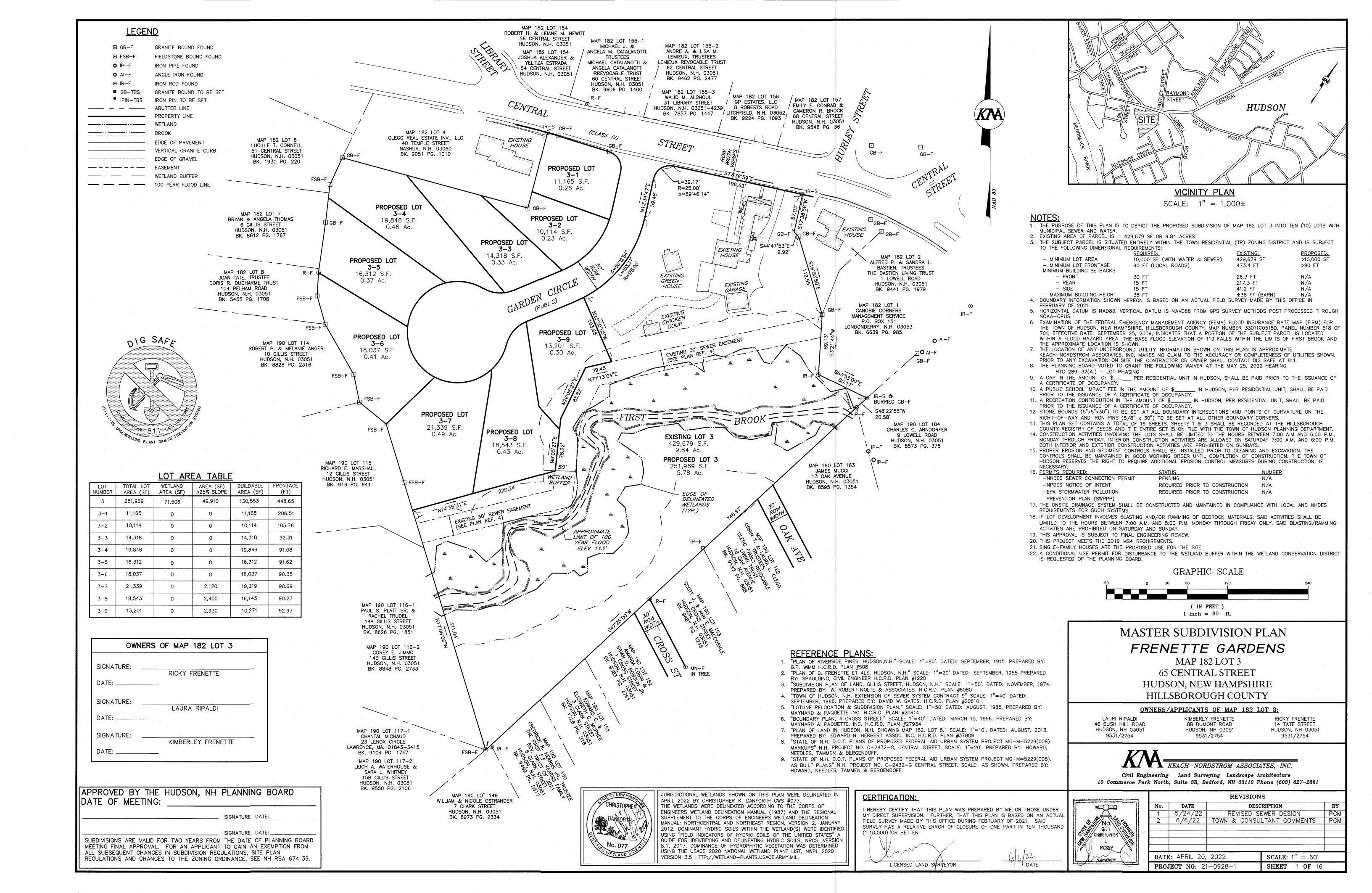
KIMBERLEY FRENETTE 8B DUMONT ROAD HUDSON, NH 03051

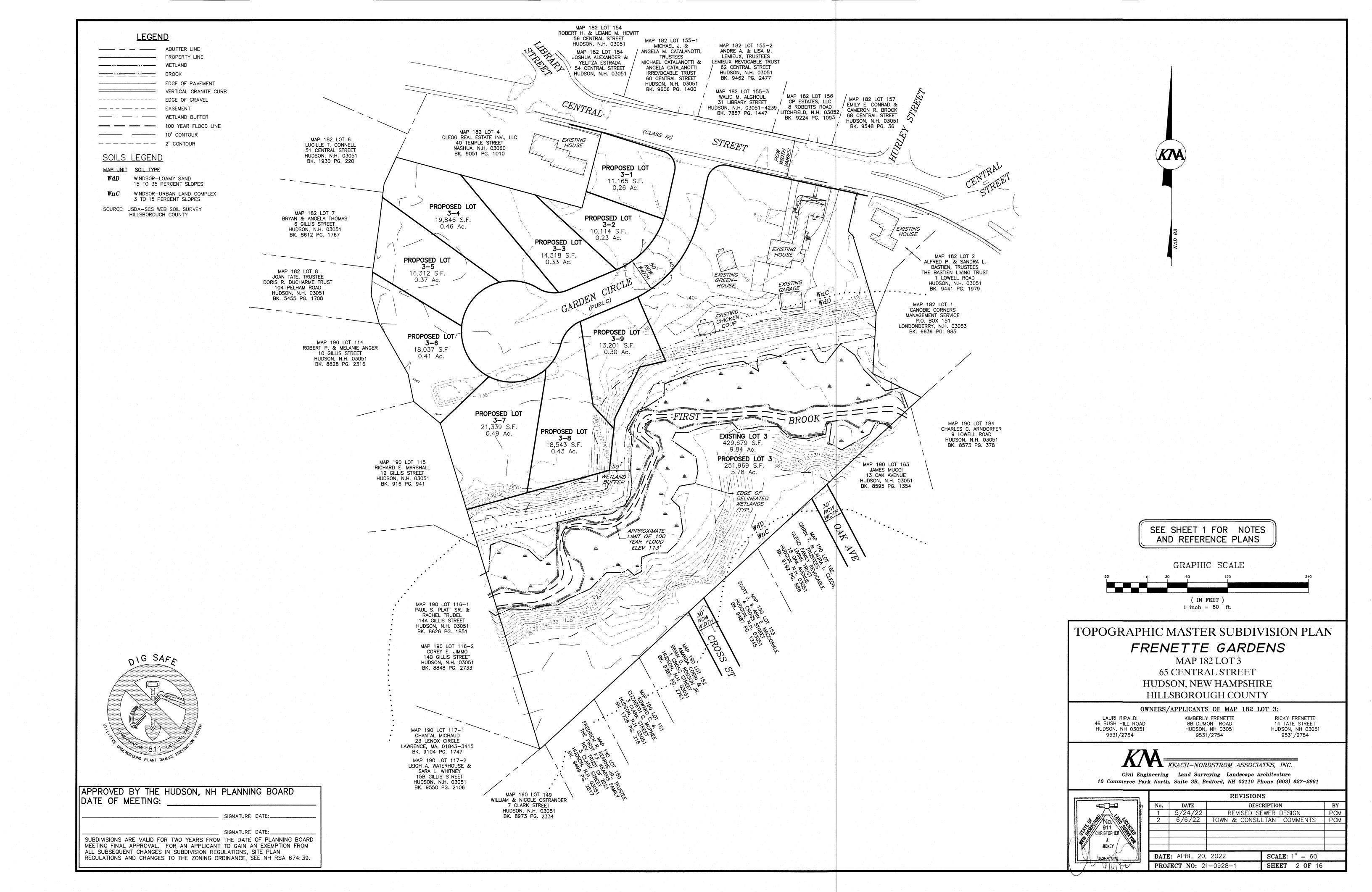
RICKY FRENETTE 14 TATE STREET HUDSON, NH 03051

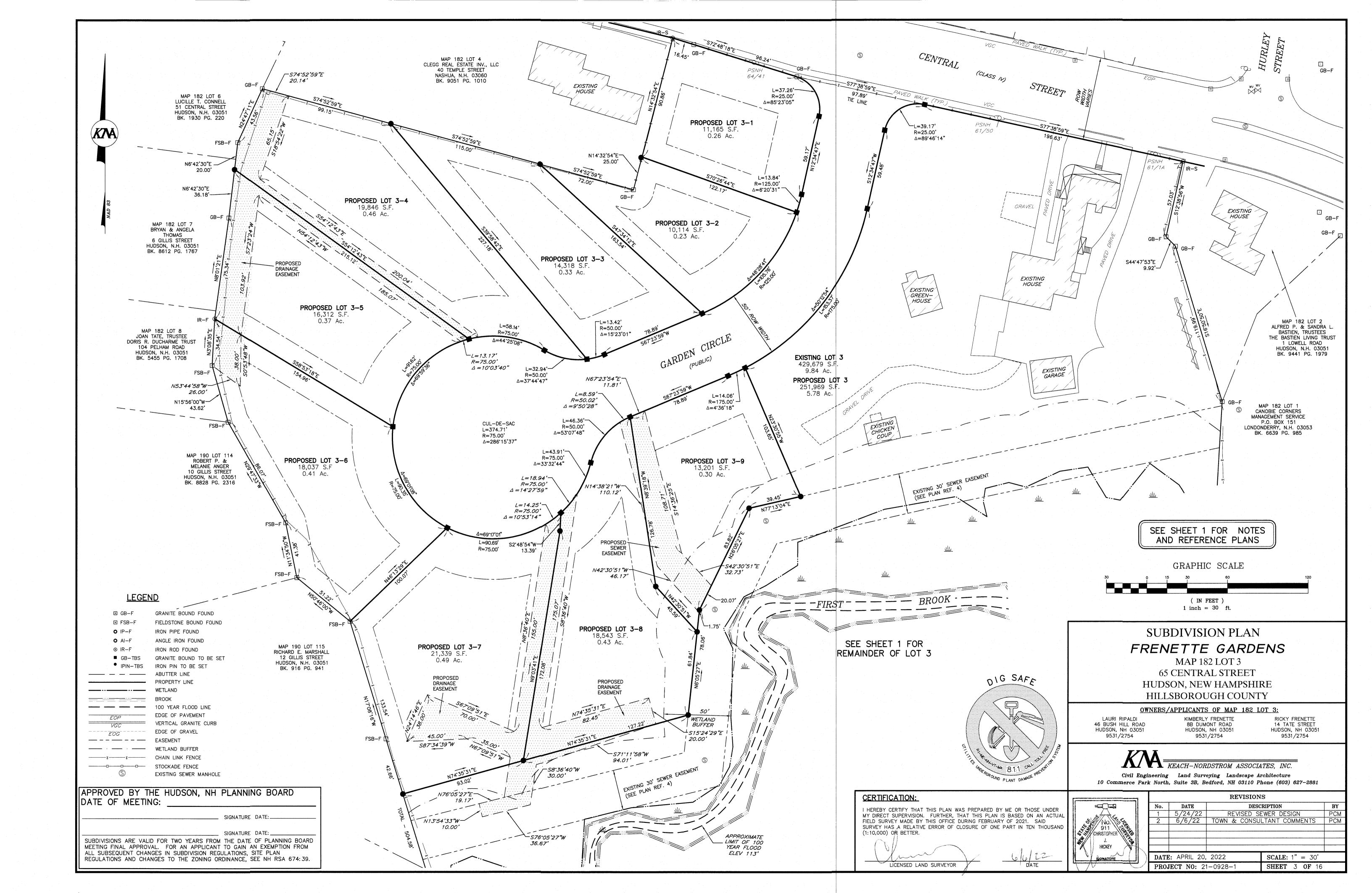
PREPARED BY:

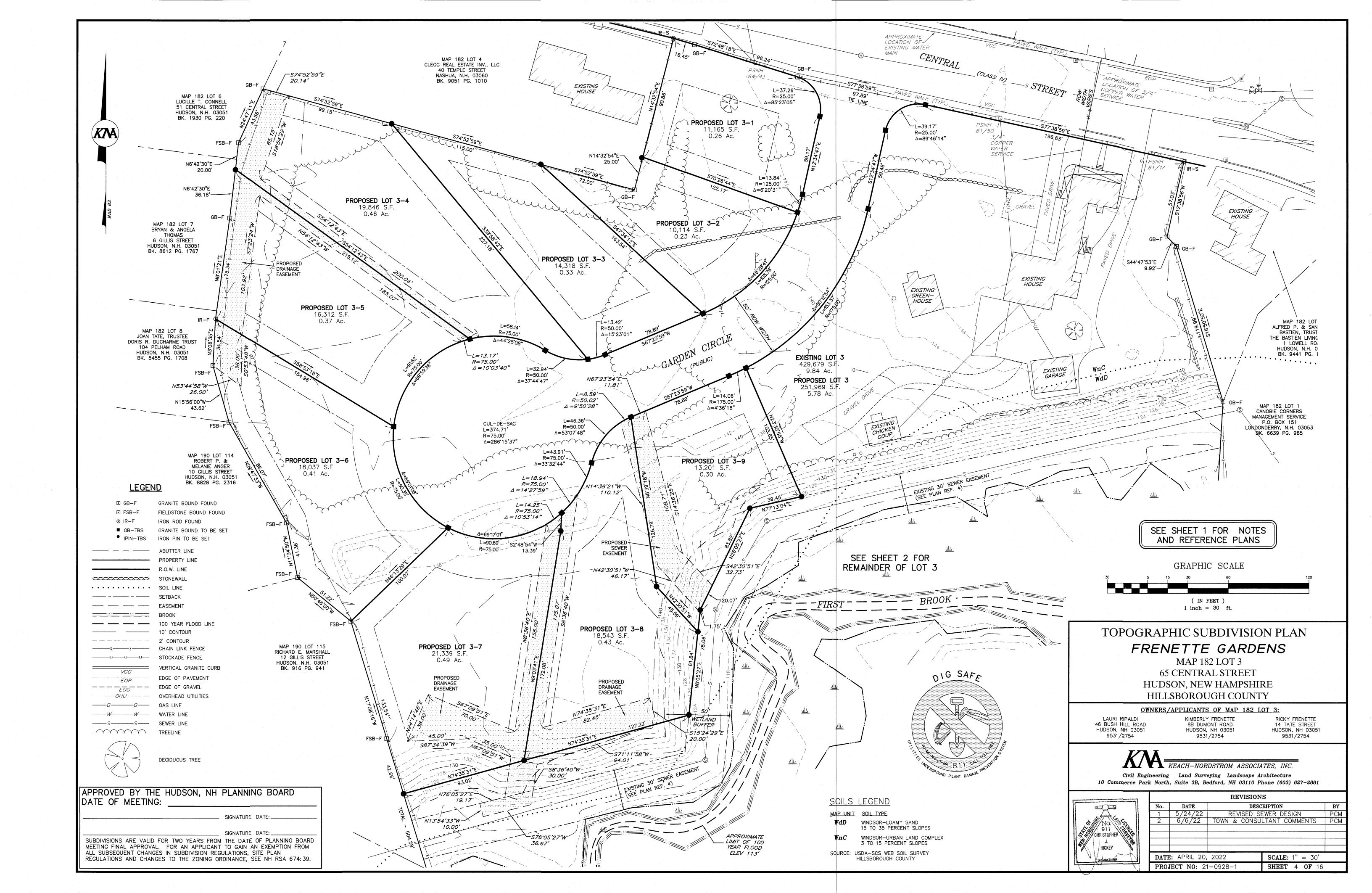
KEACH-NORDSTROM ASSOCIATES, INC. 10 COMMERCE PARK NORTH, SUITE 3B BEDFORD, NEW HAMPSHIRE 03110 (603) 627-2881

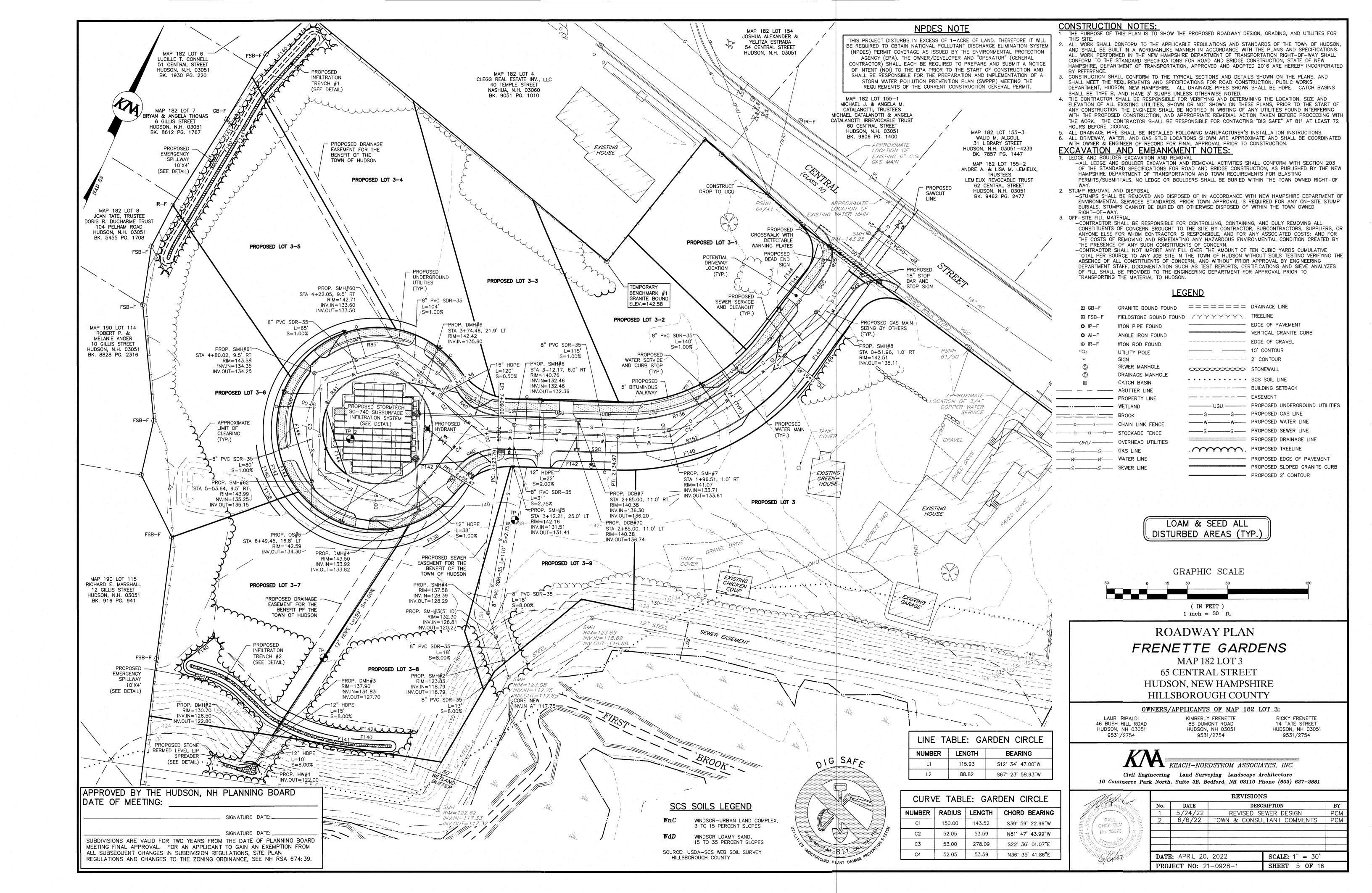
SHEET TITLE	SHEET No.	<u>•</u>
MASTER SUBDIVISION PLAN		
TOPOGRAPHIC MASTER SUBDIVISION PLAN	V 2	
SUBDIVISION PLAN	3	
TOPOGRAPHIC SUBDIVISION PLAN	4	
ROADWAY PLAN	5	
ROADWAY PROFILE	6	
EROSION CONTROL PLAN	7	
LANDSCAPING & LIGHTING PLAN	8	
SIGHT DISTANCE PLAN & PROFILE	9	
SEWER & DRAINAGE PROFILES	10	
CONSTRUCTION DETAILS	11 - 16	

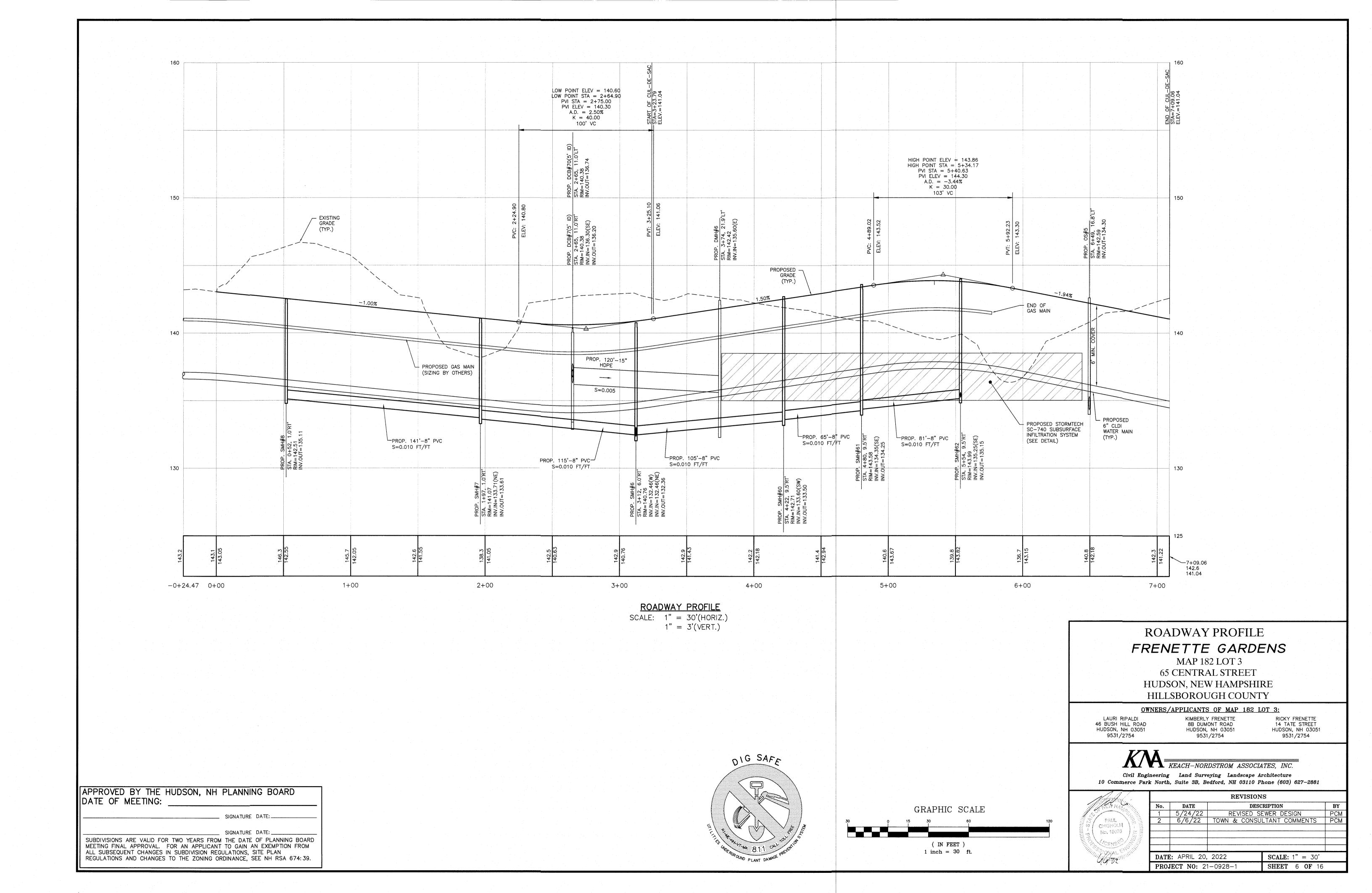


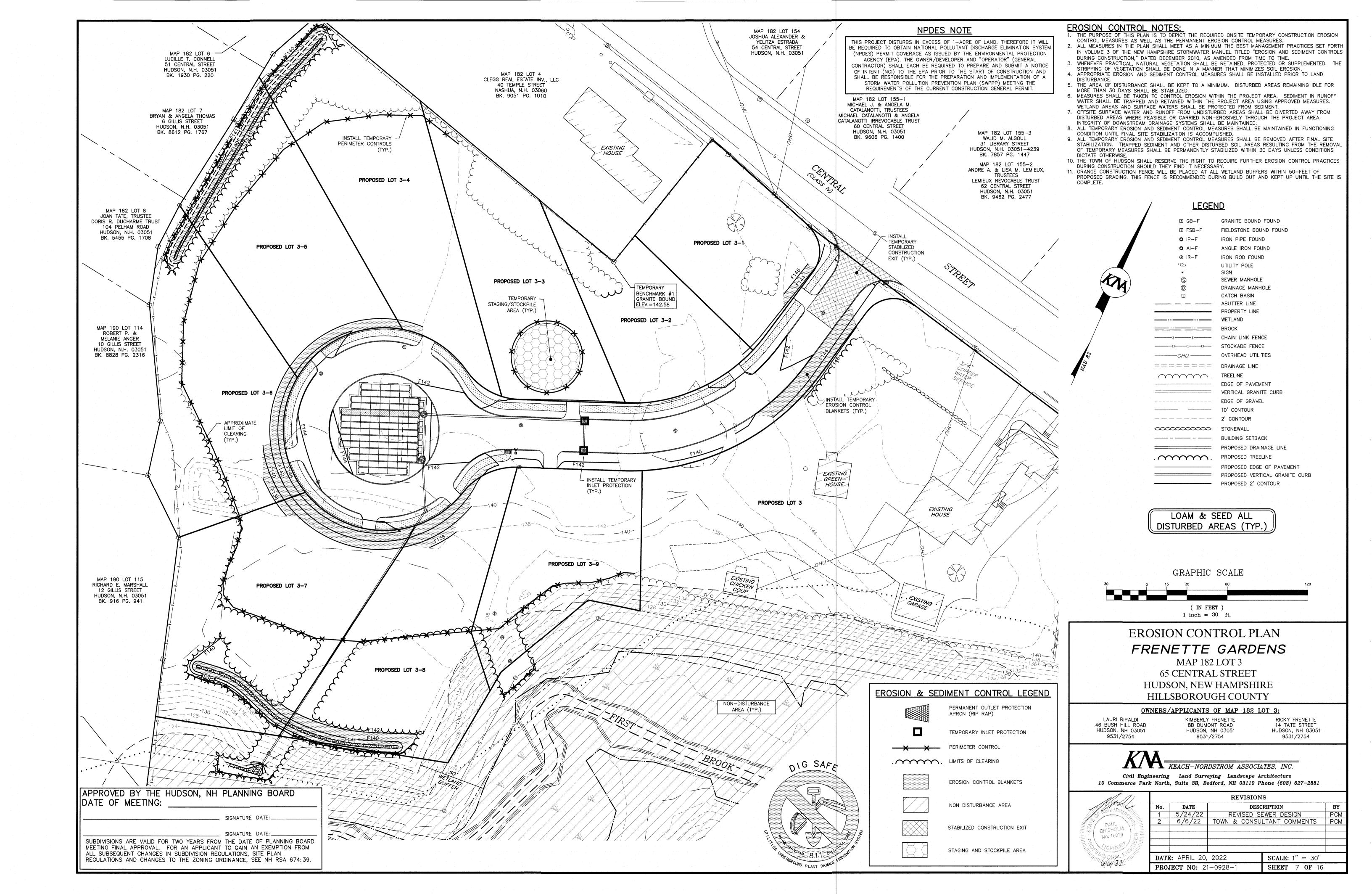


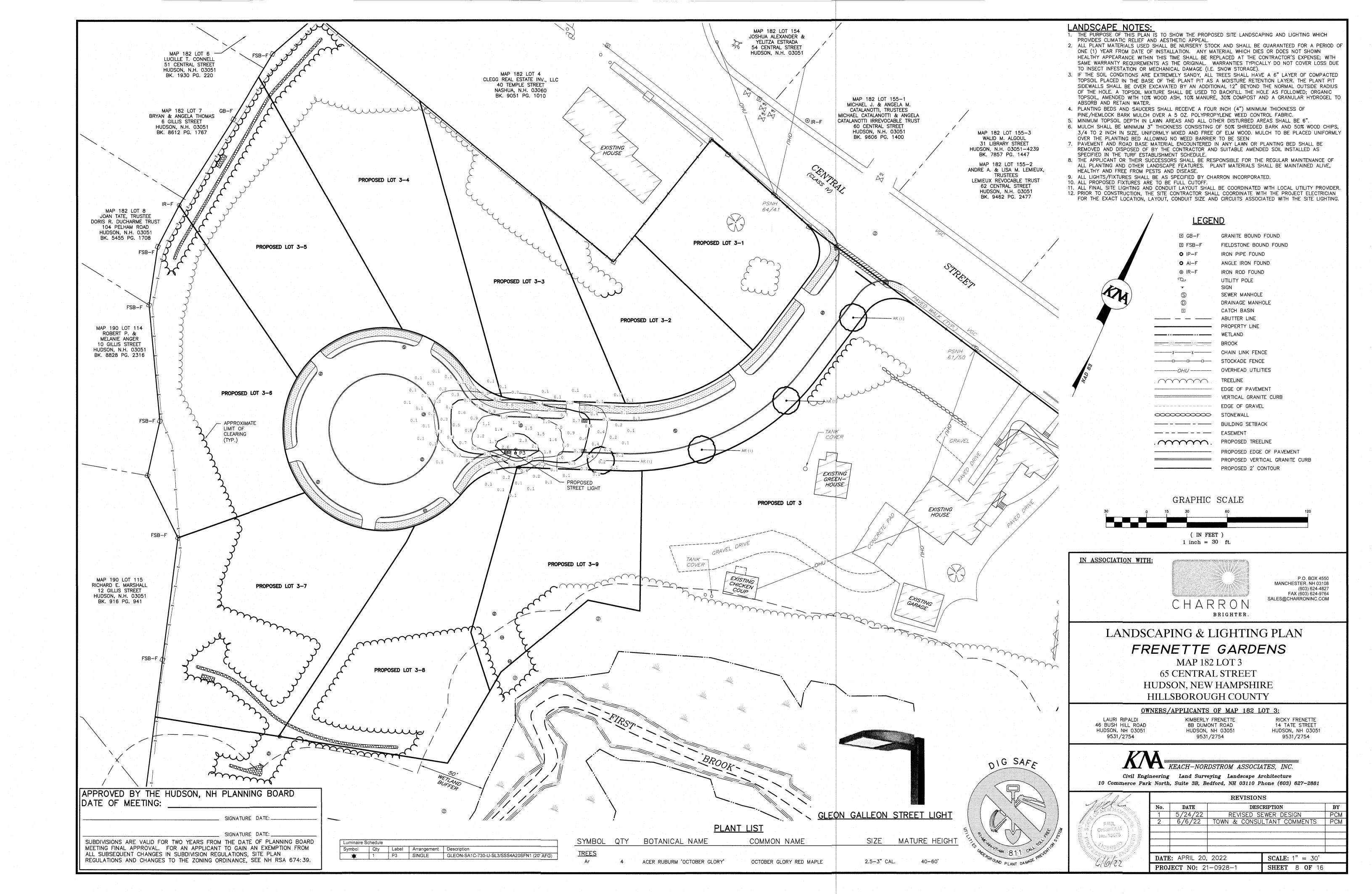


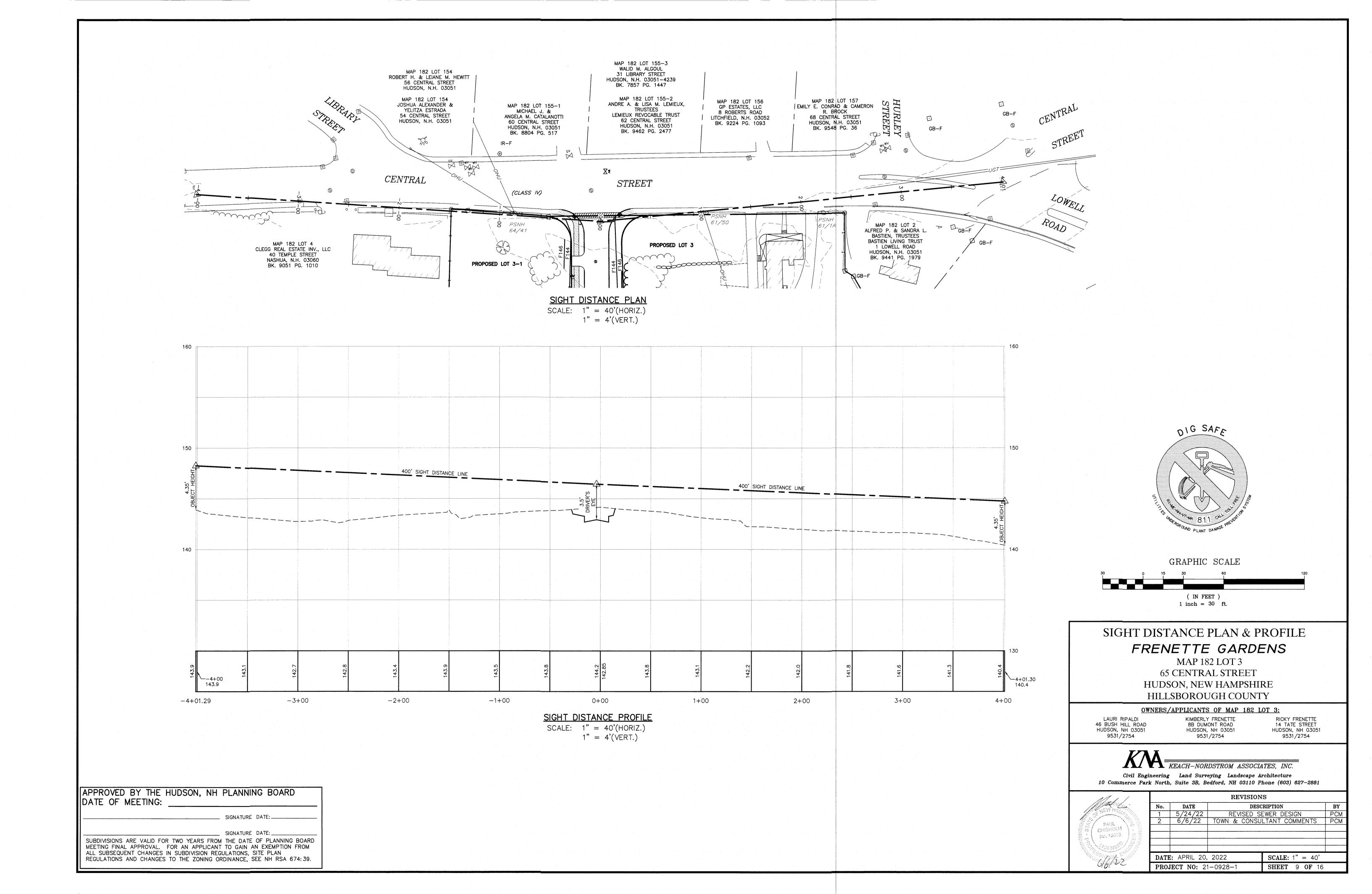


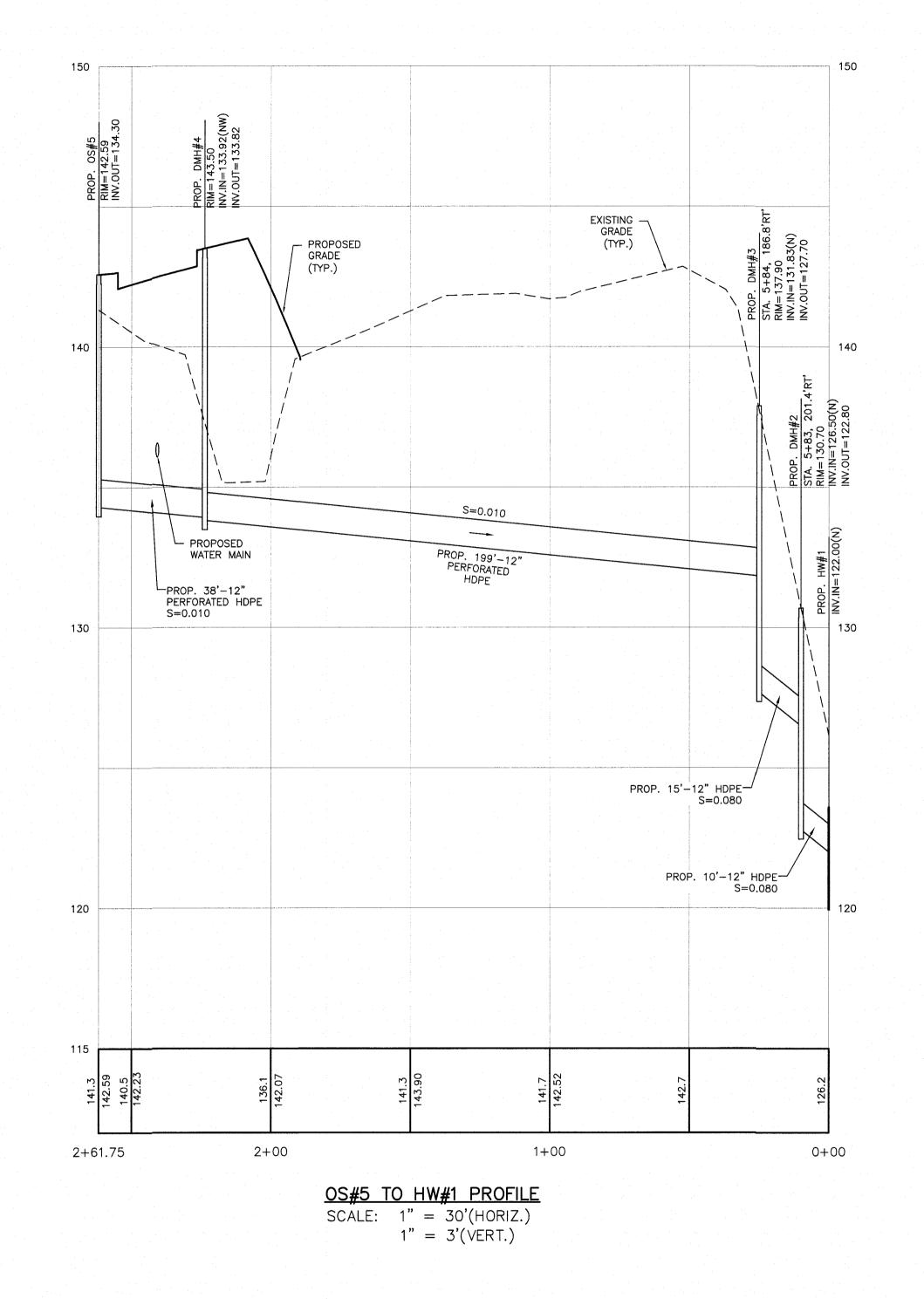












PROPOSED – GRADE (TYP.) - EXISTING GRADE (TYP.) PROPOSED -WATER MAIN PROP. 32'-8" PVC S=0.0275 FT/FT - INSTALL INSULATION WHERE SEPARATION IS LESS THAN 18" (SEE DETAIL) PROP. 19'-8" PVC-/ S=0.080 FT/FT PROPOSED — CLAY TRENCH DAM (TYP.) (SEE DETAIL) 120 PROP. 19'-8" PVC-/ S=0.080 FT/FT PROP. 14'-8" PVC-S=0.080 FT/FT 1+00 0+00 1+90.78

SMH#5 TO EXISTING SEWER MAIN PROFILE

SCALE: 1" = 30'(HORIZ.)

1" = 3'(VERT.)

DIG SAFE



GRAPHIC SCALE

MAP 182 LOT 3
65 CENTRAL STREET
HUDSON, NEW HAMPSHIRE
HILLSBOROUGH COUNTY

OWNERS/APPLICANTS OF MAP 182 LOT 3:

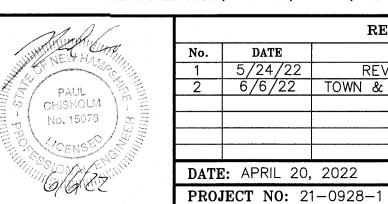
LAURI RIPALDI 46 BUSH HILL ROAD HUDSON, NH 03051 9531/2754 KIMBERLY FRENETTE
8B DUMONT ROAD
HUDSON, NH 03051
9531/2754

RICKY FRENETTE 14 TATE STREET HUDSON, NH 03051 9531/2754

KEACH-NORDSTROM ASSOCIATES, INC.

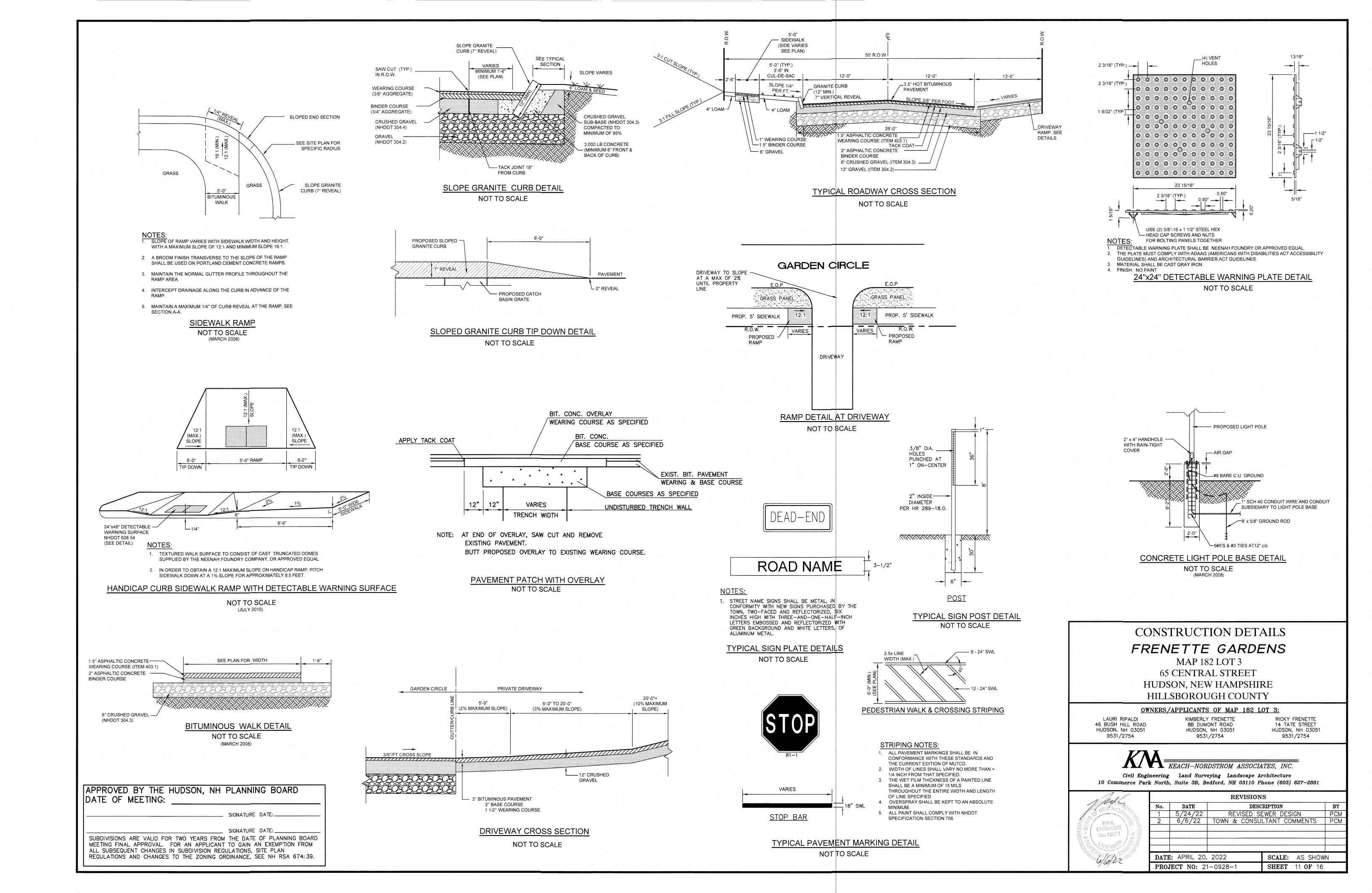
Civil Engineering Land Surveying Landscape Architecture

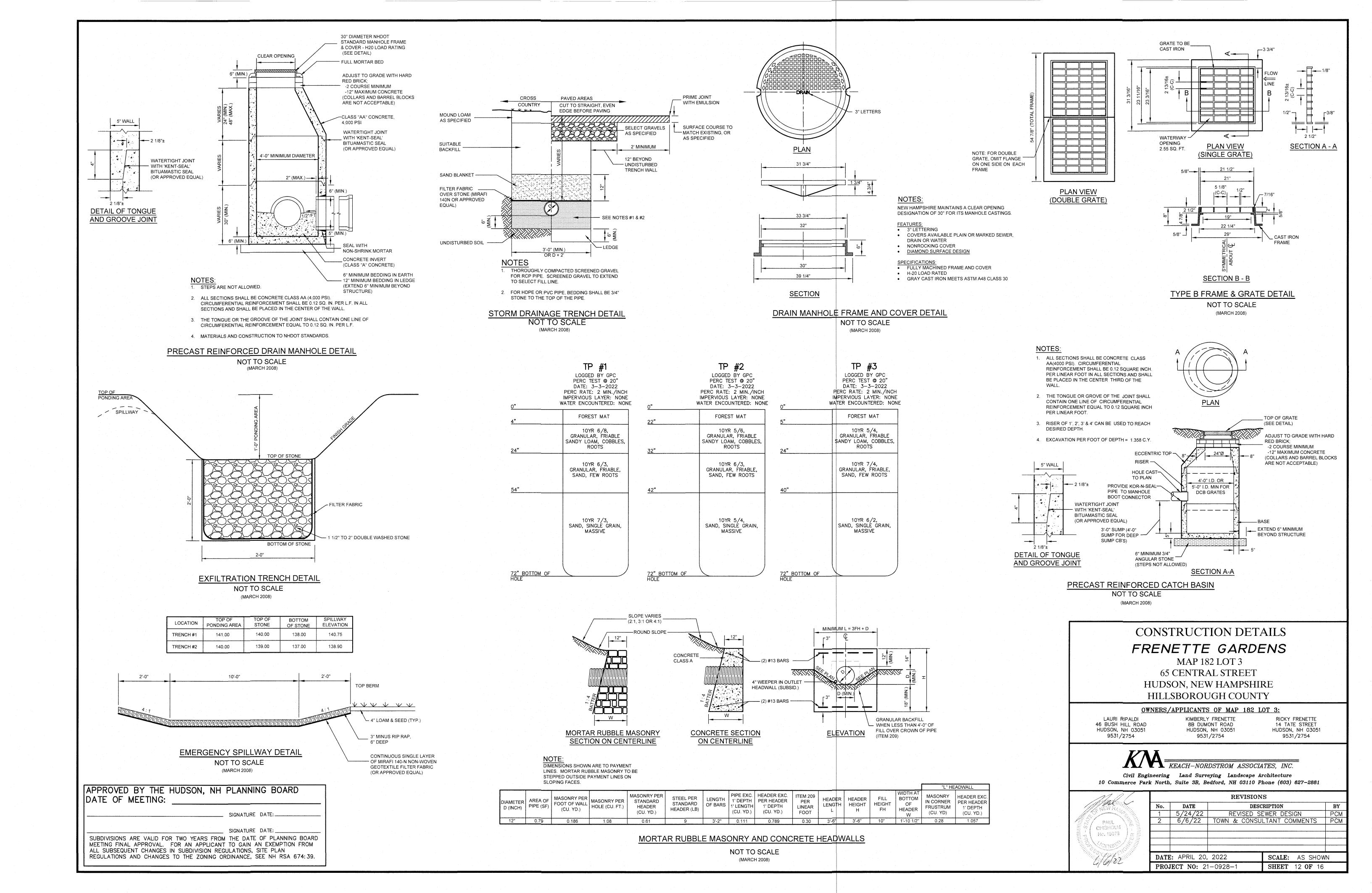
10 Commerce Park North, Suite 3B, Bedford, NH 03110 Phone (603) 627-2881

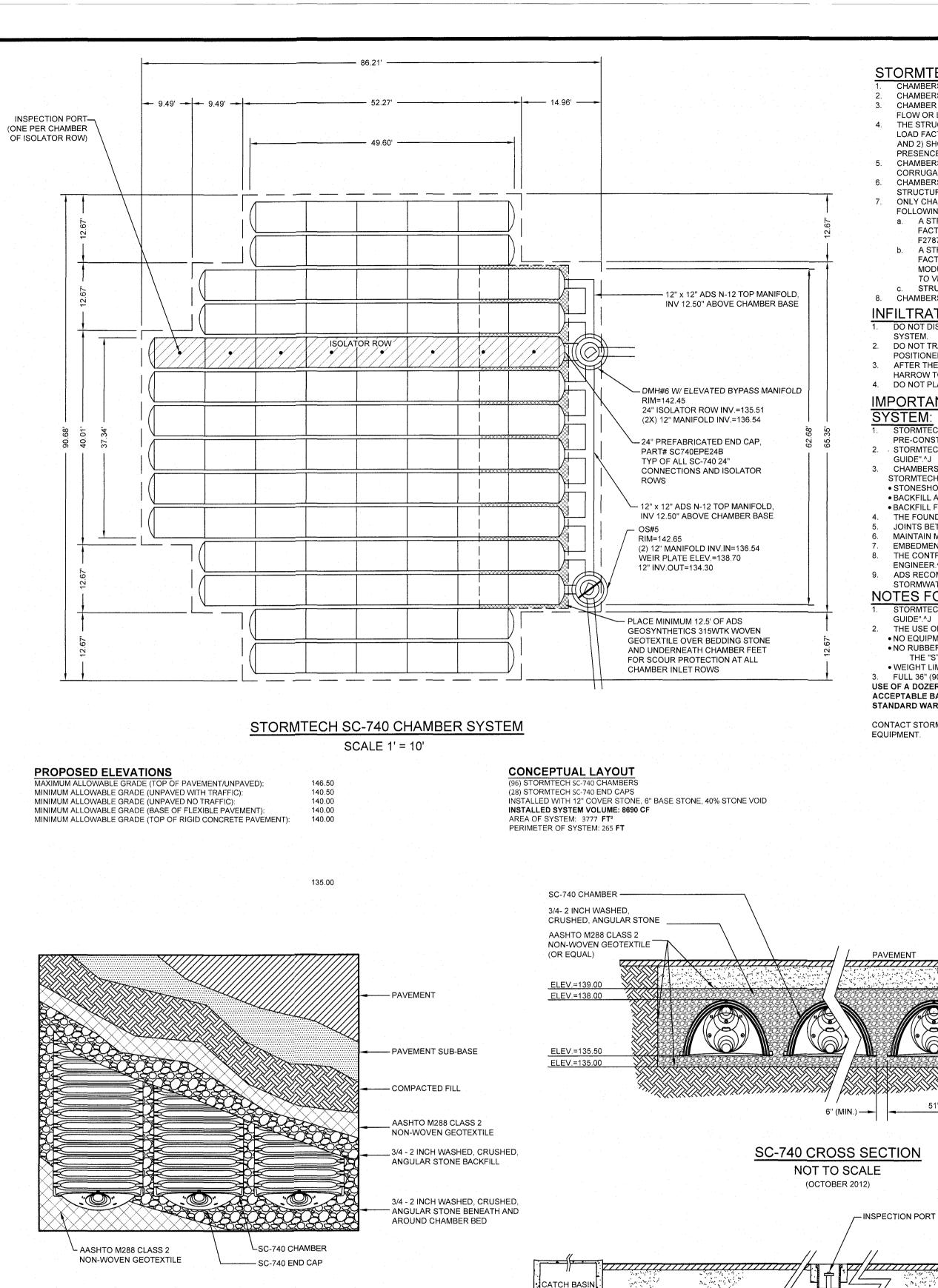


	REVISIONS				
No.	DATE	DES	CRIPTION	BY	
1	5/24/22	REVISED S	EWER DESIGN	PCM	
2	6/6/22	TOWN & CONSU	LTANT COMMENTS	PCM	
DATI	E: APRIL 20,	2022	SCALE: 1" = 30'		
PRO.	JECT NO: 2	1-0928-1	SHEET 10 OF 16		

SUBDIVISIONS ARE VALID FOR TWO YEARS FROM THE DATE OF PLANNING BOARD MEETING FINAL APPROVAL. FOR AN APPLICANT TO GAIN AN EXEMPTION FROM ALL SUBSEQUENT CHANGES IN SUBDIVISION REGULATIONS, SITE PLAN REGULATIONS AND CHANGES TO THE ZONING ORDINANCE, SEE NH RSA 674:39.







MANHOLE

AASHTO M288 CLASS 1 WOVEN

(5'-0" TO 6'-0" WIDE STRIP)

GEOTEXTILE OR EQUAL, BETWEEN

FOUNDATION STONE AND CHAMBERS

SC-740 ISOLATOR ROW PROFILE

NOT TO SCALE

(OCTOBER 2012)

SC-740 CHAMBER SYSTEM PLAN VIEW DETAIL

NOT TO SCALE (OCTOBER 2012)

APPROVED BY THE HUDSON, NH PLANNING BOARD DATE OF MEETING: SIGNATURE DATE: ____ SIGNATURE DATE: SUBDIVISIONS ARE VALID FOR TWO YEARS FROM THE DATE OF PLANNING BOARD MEETING FINAL APPROVAL. FOR AN APPLICANT TO GAIN AN EXEMPTION FROM ALL SUBSEQUENT CHANGES IN SUBDIVISION REGULATIONS, SITE PLAN REGULATIONS AND CHANGES TO THE ZONING ORDINANCE, SEE NH RSA 674: 39.

STORMTECH CHAMBER SPECIFICATIONS:

CHAMBERS SHALL BE MANUFACTURED FROM VIRGIN POLYPROPYLENE OR POLYETHYLENE RESINS.^J CHAMBER ROWS SHALL PROVIDE CONTINUOUS, UNOBSTRUCTED INTERNAL SPACE WITH NO INTERNAL SUPPORT PANELS THAT WOULD IMPEDE

FLOW OR LIMIT ACCESS FOR INSPECTION. THE STRUCTURAL DESIGN OF THE CHAMBERS, THE STRUCTURAL BACKFILL, AND THE INSTALLATION REQUIREMENTS SHALL ENSURE THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET FOR: 1) LONG-DURATION DEAD LOADS AND 2) SHORT-DURATION LIVE LOADS, BASED ON THE AASHTO DESIGN TRUCK WITH CONSIDERATION FOR IMPACT AND MULTIPLE VEHICLE

5. CHAMBERS SHALL MEET ASTM F2922 (POLYETHYLENE) OR ASTM F2418 (POLYPROPYLENE), "STANDARD SPECIFICATION FOR THERMOPLASTIC

A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE SAFETY

CORRUGATED WALL STORMWATER COLLECTION CHAMBERS".^J 6. CHAMBERS SHALL BE DESIGNED AND ALLOWABLE LOADS DETERMINED IN ACCORDANCE WITH ASTM F2787. "STANDARD PRACTICE FOR

STRUCTURAL DESIGN OF THERMOPLASTIC CORRUGATED WALL STORMWATER COLLECTION CHAMBERS". ONLY CHAMBERS THAT ARE APPROVED BY THE SITE DESIGN ENGINEER WILL BE ALLOWED. THE CHAMBER MANUFACTURER SHALL SUBMIT THE FOLLOWING UPON REQUEST TO THE SITE DESIGN ENGINEER FOR APPROVAL BEFORE DELIVERING CHAMBERS TO THE PROJECT SITE:

FACTORS ARE GREATER THAN OR EQUAL TO 1.95 FOR DEAD LOAD AND 1.75 FOR LIVE LOAD, THE MINIMUM REQUIRED BY ASTM F2787 AND BY AASHTO FOR THERMOPLASTIC PIPE. A STRUCTURAL EVALUATION SEALED BY A REGISTERED PROFESSIONAL ENGINEER THAT DEMONSTRATES THAT THE LOAD FACTORS SPECIFIED IN THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, SECTION 12.12, ARE MET. THE 50 YEAR CREEP MODULUS DATA SPECIFIED IN ASTM F2418 OR ASTM F2922 MUST BE USED AS PART OF THE AASHTO STRUCTURAL EVALUATION

TO VERIFY LONG-TERM PERFORMANCE. STRUCTURAL CROSS SECTION DETAIL ON WHICH THE STRUCTURAL EVALUATION IS BASED.

8. CHAMBERS AND END CAPS SHALL BE PRODUCED AT AN ISO 9001 CERTIFIED MANUFACTURING FACILITY. INFILTRATION SYSTEM NOTES:

DO NOT DISCHARGE SEDIMENT-LADEN WATERS FROM CONSTRUCTION ACTIVITIES (RUNOFF, WATER FROM EXCAVATIONS) TO THE INFILTRATION

2. DO NOT TRAFFIC EXPOSED SOIL SURFACE WITH CONSTRUCTION EQUIPMENT. IF FEASIBLE, PERFORM EXCAVATIONS WITH EQUIPMENT

POSITIONED OUTSIDE THE LIMITS OF THE INFILTRATION SYSTEM. AFTER THE AREA IS EXCAVATED TO THE FINAL DESIGN ELEVATION, THE FLOOR SHOULD BE DEEPLY TILLED WITH A ROTARY TILLER OR DISC

HARROW TO RESTORE INFILTRATION RATES, FOLLOWED BY A PASS WITH A LEVELING DRAG. 4. DO NOT PLACE INFILTRATION SYSTEMS INTO SERVICE UNTIL THE CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED

IMPORTANT - NOTES FOR THE BIDDING AND INSTALLATION OF THE SC-310/SC-740

. STORMTECH SC-310 & SC-740 CHAMBERS SHALL NOT BE INSTALLED UNTIL THE MANUFACTURER'S REPRESENTATIVE HAS COMPLETED A PRE-CONSTRUCTION MEETING WITH THE INSTALLERS.^J

STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/SC-780 CONSTRUCTION

3. CHAMBERS ARE NOT TO BE BACKFILLED WITH A DOZER OR AN EXCAVATOR SITUATED OVER THE CHAMBERS. STORMTECH RECOMMENDS 3 BACKFILL METHODS: • STONESHOOTER LOCATED OFF THE CHAMBER BED.

• BACKFILL AS ROWS ARE BUILT USING AN EXCAVATOR ON THE FOUNDATION STONE OR SUBGRADE.

• BACKFILL FROM OUTSIDE THE EXCAVATION USING A LONG BOOM HOE OR EXCAVATOR.^J THE FOUNDATION STONE SHALL BE LEVELED AND COMPACTED PRIOR TO PLACING CHAMBERS.^J

JOINTS BETWEEN CHAMBERS SHALL BE PROPERLY SEATED PRIOR TO PLACING STONE.^J

MAINTAIN MINIMUM - 6" (150 mm) SPACING BETWEEN THE CHAMBER ROWS.^J EMBEDMENT STONE SURROUNDING CHAMBERS MUST BE A CLEAN, CRUSHED, ANGULAR STONE 3/4-2" (20-50 mm).^J

> GRANULAR WELL GRADED SOIL/AGGREGATE MIXTURES, <35% FINES (COMPACT IN 6" LIFTS

TO 95% PROCTOR DENSITY)

- SC-740 END CAP

FOR UNPAVED INSTALLATION WHERE

RUTTING FROM VEHICLES MAY OCCUR,

INCREASE COVER TO 24 INCHES

THE CONTRACTOR MUST REPORT ANY DISCREPANCIES WITH CHAMBER FOUNDATION MATERIALS BEARING CAPACITIES TO THE SITE DESIGN

ADS RECOMMENDS THE USE OF "FLEXSTORM CATCH IT" INSERTS DURING CONSTRUCTION FOR ALL INLETS T ϕ PROTECT THE SUBSURFACE STORMWATER MANAGEMENT SYSTEM FROM CONSTRUCTION SITE RUNOFF.

NOTES FOR CONSTRUCTION EQUIPMENT: 1. STORMTECH SC-310 & SC-740 CHAMBERS SHALL BE INSTALLED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION

THE USE OF CONSTRUCTION EQUIPMENT OVER SC-310 & SC-740 CHAMBERS IS LIMITED:

• NO EQUIPMENT IS ALLOWED ON BARE CHAMBERS. • NO RUBBER TIRED LOADERS, DUMP TRUCKS, OR EXCAVATORS ARE ALLOWED UNTIL PROPER FILL DEPTHS ARE REACHED IN ACCORDANCE WITH THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE".

 WEIGHT LIMITS FOR CONSTRUCTION EQUIPMENT CAN BE FOUND IN THE "STORMTECH SC-310/SC-740/DC-780 CONSTRUCTION GUIDE". A FULL 36" (900 mm) OF STABILIZED COVER MATERIALS OVER THE CHAMBERS IS REQUIRED FOR DUMP TRUCK TRAVEL OR DUMPING. USE OF A DOZER TO PUSH EMBEDMENT STONE BETWEEN THE ROWS OF CHAMBERS MAY CAUSE DAMAGE TO THE CHAMBERS AND IS NOT AN ACCEPTABLE BACKFILL METHOD. ANY CHAMBERS DAMAGED BY THE "DUMP AND PUSH" METHOD ARE NOT COVERED UNDER THE STORMTECH

COVER ENTIRE ROW WITH AASHTO

AASHTO M288 CLASS 2

- NON-WOVEN GEOTEXTILE

(OR EQUAL)

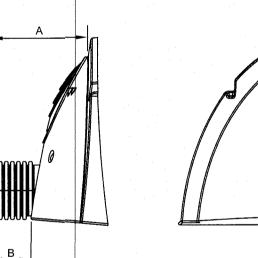
- M288 CLASS 2 NON-WOVEN

GEOTEXTILE OR EQUAL

(8'-0" WIDE STRIP)

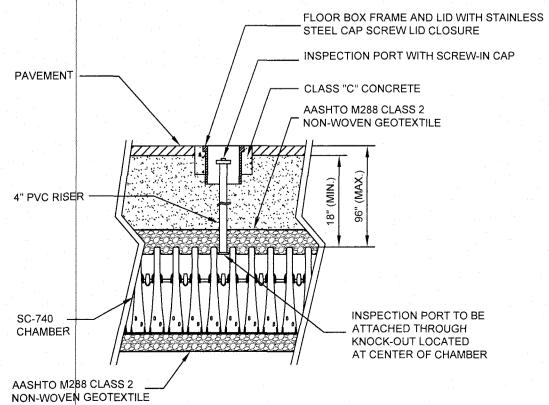
-SC-740 ENDCAP

CONTACT STORMTECH AT 1-888-892-2694 WITH ANY QUESTIONS ON INSTALLATION REQUIREMENTS OR WEIGHT LIMITS FOR CONSTRUCTION

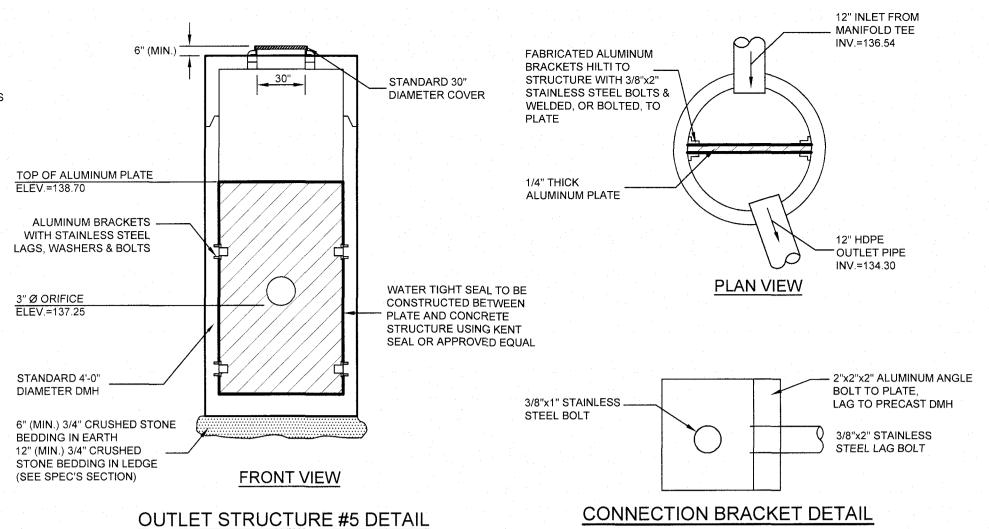




(OCTOBER 2012)					
SIZE	Α	В	С		
nm)	18.20" (462 mm)	9.20" (234 mm)	1.30" (33 mm)		
	20.10"	11.00"	4.000		



SC-740 INSPECTION PORT DETAIL

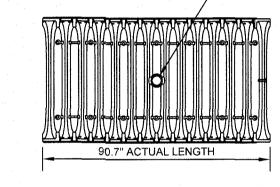


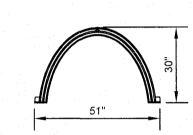
NOT TO SCALE (MARCH 2008)

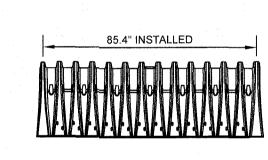
> ACCEPTS 4" PVC RISER FOR INSPECTION PORT

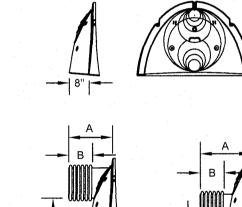
NOT TO SCALE

(MARCH 2008)









OMINAL CHAMBER SPECIFICATIONS SIZE $(W \times H \times INSTALLED LENGTH)$ CHAMBER STORAGE MINIMUM INSTALLED STORAGE

51.0" x 30.0" x 85.4" 45.9 CUBIC FEET 74.9 CUBIC FEET 75 LBS.

<u> </u>				
PIPE SIZE	Α	В	С	D
12 in (300 mm)	14.70 in (373 mm)	7.70 in (196 mm)	12.50 in (318 mm)	N/A
12 in (300 mm)	14.70 in (373 mm)	7.70 in (196 mm)	N/A	1.20 in (30 mm)
24 in (600 mm)	18.50 in (470 mm)	9.45 in (240 mm)	N/A	0.10 in (3 mm)

SC-740 TECHNICAL SPECIFICATIONS NOT TO SCALE (OCTOBER 2012)

CONSTRUCTION DETAILS FRENETTE GARDENS

MAP 182 LOT 3

65 CENTRAL STREET HUDSON, NEW HAMPSHIRE HILLSBOROUGH COUNTY

OWNERS/APPLICANTS OF MAP 182 LOT 3:

LAURI RIPALDI 46 BUSH HILL ROAD HUDSON, NH 03051 9531/2754

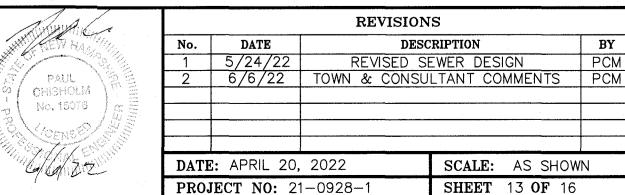
KIMBERLY FRENETTE 8B DUMONT ROAD HUDSON, NH 03051 9531/2754

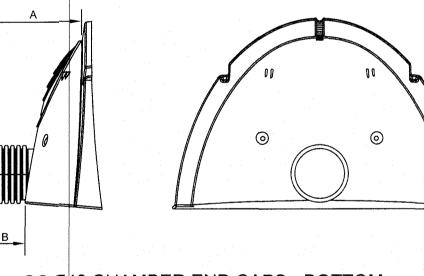
RICKY FRENETTE 14 TATE STREET HUDSON, NH 03051 9531/2754



■ KEACH-NORDSTROM ASSOCIATES. INC.

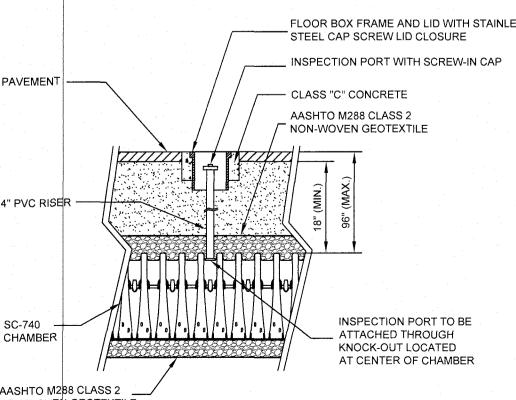
Civil Engineering Land Surveying Landscape Architecture 10 Commerce Park North, Suite 3B, Bedford. NH 03110 Phone (603) 627-2881



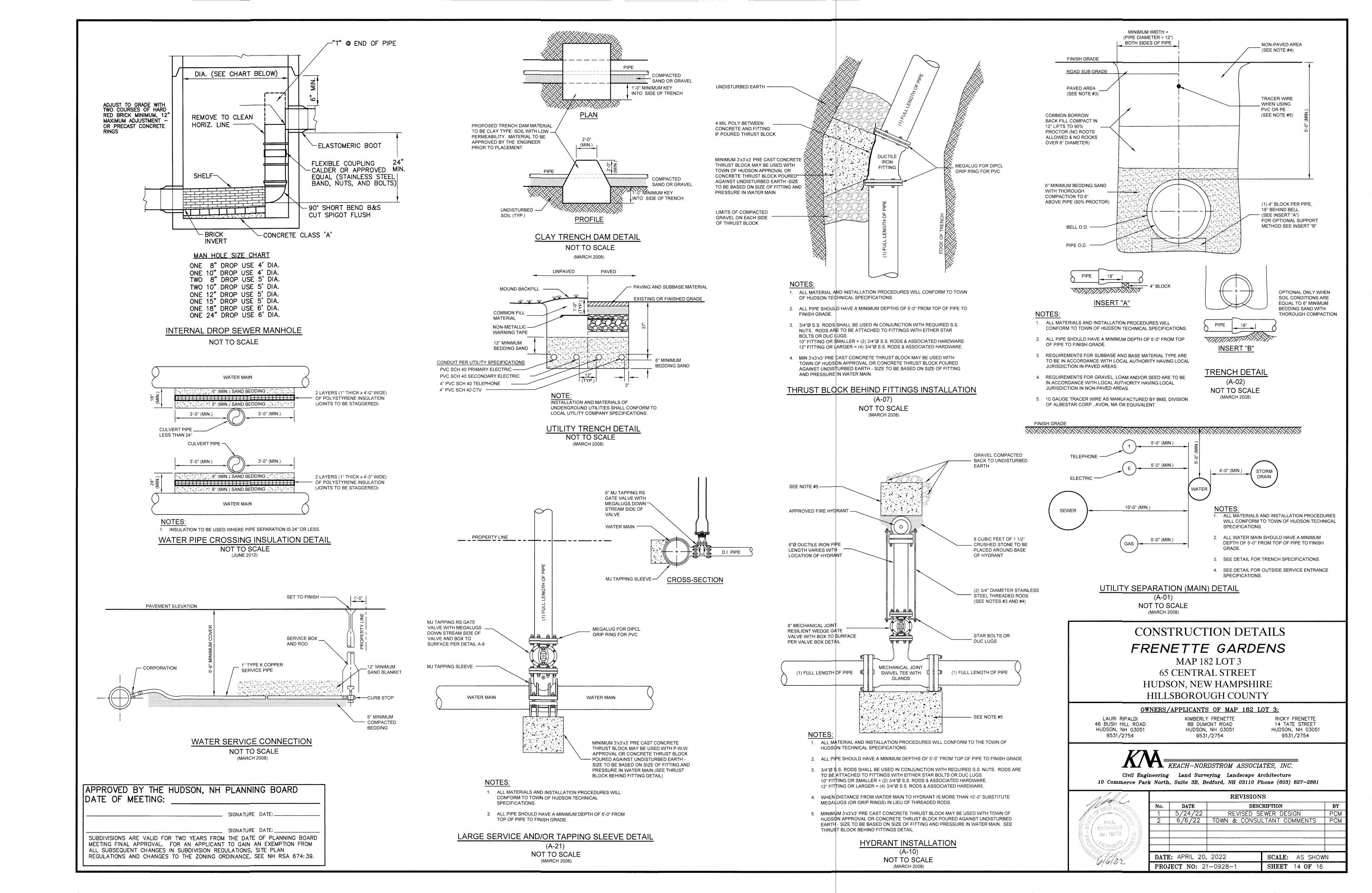


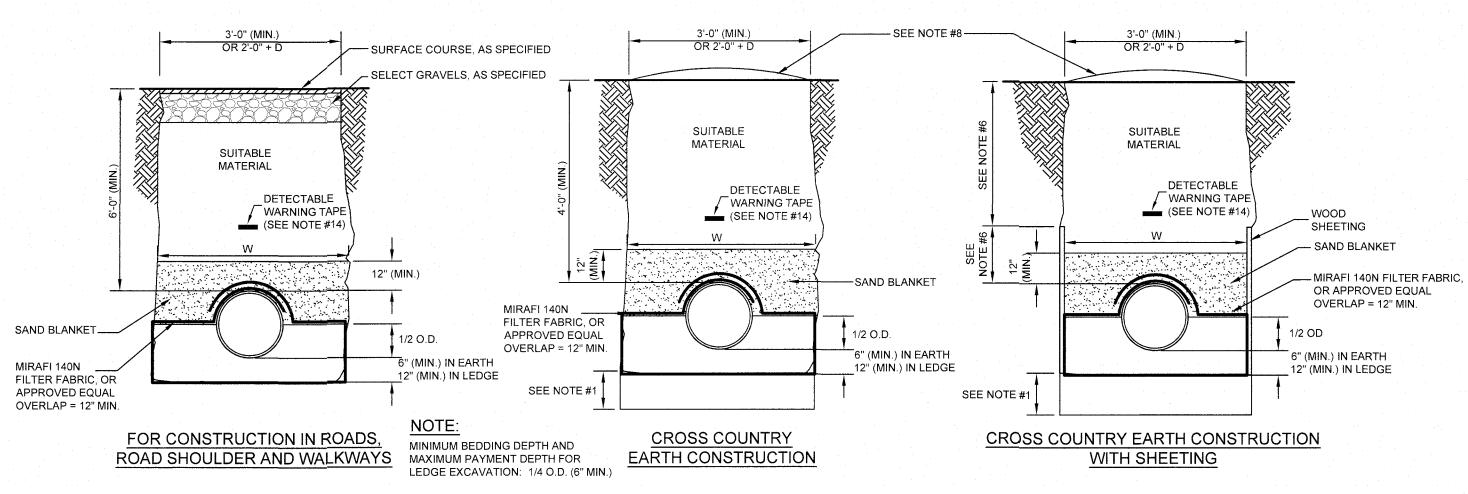
NOT TO SCALE

(300 mi 20.10" | 11.00" (511 mm) | (279 mm) (450 mm)



NOT TO SCALE (OCTOBER 2012)





SANITARY SEWER TRENCH DETAIL NOT TO SCALE

(NOVEMBER 2016)

1. ORDERED EXCAVATION OF UNSUITABLE MATERIAL BELOW GRADE. REFILL WITH BEDDING MATERIAL, ALSO SEE NOTE #7. BEDDING: CRUSHED STONE FREE FROM CLAY, LOAM, ORGANIC

- MATTER AND MEETING ASTM C33/C33M STONE SIZE NO. 67. 100% PASSING 1 INCH SCREEN 90 - 100% PASSING 3/4 INCH SCREEN 20 - 55% PASSING 3/8 INCH SCREEN 0 - 10% PASSING # 4 SIEVE
- 0 5% PASSING # 8 SIEVE WHERE ORDERED BY THE ENGINEER TO STABILIZE THE TRENCH BASE, GRADED CRUSHED STONE 1/2 INCH TO 1-1/2 INCHES SHALL BE USED. 2. SAND BLANKET: GRADED CLEAN SAND FREE FROM ORGANIC MATTER, SO THAT 100% PASSES A 1/2 INCH SIEVE AND NOT MORE THAN 15% WILL PASS A # 200 SIEVE. BLANKET MAY BE OMITTED FOR CAST IRON, DUCTILE IRON AND
- REINFORCED CONCRETE PIPE PROVIDED, HOWEVER, THAT NO STONE LARGER THAN 2 INCHES IS IN CONTACT WITH THE PIPE. 3. MIRAFI 140 N FILTER FABRIC, OR APPROVED EQUAL, SHALL BE INSTALLED
- 4. SUITABLE MATERIAL: IN ROADS, ROAD SHOULDERS, WALKWAYS AND RAVELED WAYS SUITABLE MATERIAL FOR TRENCH BACKFILL SHALL BE THE NATURAL MATERIAL EXCAVATED DURING THE COURSE OF CONSTRUCTION, BUT SHALL EXCLUDE DEBRIS, PIECES OF PAVEMENT, ORGANIC MATTER, TOP SOIL, ALL WET OR SOFT MUCK, PEAT OR CLAY, ALL EXCAVATED LEDGE MATERIAL AND ALL ROCKS OVER 6 INCHES IN LARGEST DIMENSION, OR ANY MATERIAL WHICH, AS DETERMINED BY THE ENGINEER, WILL NOT PROVIDE SUFFICIENT SUPPORT OR MAINTAIN THE COMPLETED CONSTRUCTION IN A STABLE CONDITION.

IN CROSS COUNTRY CONSTRUCTION, SUITABLE MATERIAL SHALL BE AS DESCRIBED ABOVE, EXCEPT THAT THE ENGINEER MAY PERMIT THE USE OF TOP SOIL, LOAM, MUCK OR PEAT IF HE/SHE IS SATISFIED THAT THE COMPLETED CONSTRUCTION WILL BE ENTIRELY STABLE AND PROVIDED THAT EASY ACCESS TO THE SEWER WILL BE PRESERVED FOR MAINTENANCE AND POSSIBLY RECONSTRUCTION, WHEN NECESSARY.

- 5. BASE COURSE, IF ORDERED BY THE ENGINEER, SHALL MEET THE REQUIREMENTS OF DIVISION 300 OF THE LATEST EDITION OF THE "STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION OF THE STATE OF NEW HAMPSHIRE, DEPARTMENT OF PUBLIC WORKS AND HIGHWAYS."
- WOOD SHEETING, IF REQUIRED, WHERE PLACED ALONGSIDE THE PIPE AND EXTENDING BELOW MID-DIAMETER, SHALL BE CUT OFF AND LEFT IN PLACE TO AN ELEVATION NOT LESS THAN 1 FOOT ABOVE THE TOP OF THE PIPE. WHERE SHEETING IS ORDERED BY THE ENGINEER TO BE LEFT IN PLACE. IT SHALL BE CUT OFF AT LEAST 3 FEET BELOW FINISHED GRADE, BUT NOT LESS THAN 1 FOOT ABOVE THE TOP OF THE PIPE.
- W = MAXIMUM ALLOWABLE TRENCH WIDTH TO A PLANE 12 INCHES ABOVE THE PIPE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, W SHALL BE NO MORE THAN 36 INCHES. FOR PIPES GREATER THAN 15 INCHES NOMINAL DIAMETER. W SHALL BE 24 INCHES PLUS PIPE O.D. W SHALL ALSO BE THE PAYMENT WIDTH FOR LEDGE EXCAVATION AND FOR ORDERED EXCAVATION BELOW GRADE.
- 8. FOR CROSS COUNTRY CONSTRUCTION, BACKFILL OR FILL SHALL BE MOUNDED TO A HEIGHT OF 6 INCHES ABOVE THE ORIGINAL GROUND
- NEW HAMPSHIRE DEPARTMENT OF ENVIRONMENTAL SERVICES DESIGN STANDARDS REQUIRE 10 FEET OF SEPARATION BETWEEN WATER AND SEWER. HOWEVER, SHOULD CONSTRUCTION REVEAL OR EXPOSE A WATERLINE (MAIN OR SERVICE) RUNNING APPROXIMATELY PARALLEL AND LESS THAN 10 FEET HORIZONTALLY FROM THE PROPOSED SEWER INSTALLATION AND WHERE IT IS NOT PRACTICAL TO RELOCATE THE SEWER, A DEVIATION MAY BE GRANTED PROVIDED THAT THE SEWER IS CONSTRUCTED IN ACCORDANCE WITH THE FORCE MAIN CONSTRUCTION REQUIREMENT A. FORCE MAINS SHALL BE CONSTRUCTED FROM DUCTILE IRON, HIGH
 - DENSITY POLYETHYLENE, OR PVC PER ENV-WQ 704.06(a). PVC SHALL CONFORM TO ASTM D2241-05 OR ASTM D1785-05 HDPE SHALL CONFORM TO ASTM D3035-03a D.I. SHALL BE CORROSION PROTECTED IN CORROSIVE ENVIRONMENTS

8 INCHES

2. PIPE AND JOINT MATERIALS

ADAPTERS SHALL BE USED.

OBSERVATION TEE AND PLUG

SEWER CLEAN-OUT AT TIME

OF SERVICE CONNECTION

TO BE REPLACED WITH

WYE (SEE

NOTES #4 & 5)

STREET SEWER -

WATER WORKS ASSOCIATION (AWWA):

DUCTILE IRON CASTINGS

MOLDS, FOR WATER OR OTHER LIQUIDS;

D2414-02 DURING MANUFACTURING; AND

DAMAGED PIPE SHALL BE REJECTED AND REMOVED FROM THE JOB SITE.

ASTM D3034-04A - PVC, SOLID WALL

- 10. WHERE WATER LINES AND SEWER LINES CROSS, THEY SHOULD CROSS AS PERPENDICULAR AS POSSIBLE AND THE WATER MAIN SHALL CROSS AT LEAST 18" INCHES ABOVE THE SEWER. FURTHER, THE SEWER JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLY FROM THE WATER MAIN
- 11. ALL SEWERS AT 8 PERCENT SLOPE, OR GREATER, SHALL HAVE IMPERVIOUS TRENCH DAMS CONSTRUCTED EVERY 300 FEET.
- 12. UNLESS OTHERWISE NOTED, ALL GRANULAR MATERIAL SHALL BE PLACED IN 12" LIFTS AND COMPACTED TO 95% OF THE MODIFIED PROCTOR TEST 13. WHERE WATER MAINS CROSS UNDER SEWER MAINS, BOTH THE SEWER AND WATER MAINS SHALL BE PRESSURE RATED PIPE PER ENV-WQ 704.06 AND TESTED PER AWWA C600-05 AT 1.5 TIMES DESIGN PRESSURE OR 100 PSI, WHICHEVER IS GREATER. WITH NO JOINTS WITHIN 9 FEET OF THE CROSSING
- POINT AND 18" MINIMUM VERTICAL SEPARATION. 14. ALL SEWERS SHALL BE MARKED USING METAL IMPREGNATED MARKING TAPE OR TRACER WIRE THAT CAN BE LOCATED USING METAL DETECTION EQUIPMENT.
- 15. GRAVITY PIPE SEWER TESTING A. ALL NEW GRAVITY SEWERS SHALL BE TESTED FOR WATER TIGHTNESS BY THE USE OF LOW-PRESSURE AIR TESTS.
- B. LOW-PRESSURE AIR TESTING SHALL BE IN CONFORMANCE WITH: 1. ASTM F1417-92(2005) "STANDARD TEST METHOD FOR INSTALLATION ACCEPTANCE OF PLASTIC GRAVITY SEWER LINES USING LOW-PRESSURE
- 2. UNI-BELL PVC PIPE ASSOCIATION UNI-B-6, "LOW-PRESSURE AIR TESTING OF INSTALLED SEWER PIPE" (1998) C. ALL NEW GRAVITY SEWERS SHALL BE CLEANED AND VISUALLY INSPECTED
- USING A LAMP TEST AND BY INTRODUCING WATER TO DETERMINE THAT THERE IS NO STANDING WATER IN THE SEWER AND SHALL BE TRUE TO LINE AND GRADE FOLLOWING INSTALLATION AND PRIOR TO USE
- D. ALL PLASTIC SEWER PIPE SHALL BE DEFLECTION TESTED NOT LESS THAN 30 DAYS NOR MORE THAN 90 DAYS FOLLOWING INSTALLATION.
- E. THE MAXIMUM ALLOWABLE DEFLECTION OF FLEXIBLE SEWER PIPE SHALL BE 5 PERCENT OF AVERAGE INSIDE DIAMETER. A RIGID BALL OR MANDREL WITH A DIAMETER OF AT LEAST 95 PERCENT OF THE AVERAGE INSIDE PIPE DIAMETER SHALL BE USED FOR TESTING PIPE DEFLECTION. THE DEFLECTION TEST SHALL BE CONDUCTED WITHOUT MECHANICAL PULLING DEVICES.

MINIMUM SIZE PIPE FOR HOUSE SERVICE SHALL BE 4 INCHES. MINIMUM SIZE FOR STREET SEWER LINES SHALL BE

1. AWWA C151/A21.51-02 - FOR DUCTILE IRON PIPE, CENTRIFUGALLY CAST IN METAL OR SAND-LINED

2. AWWA C150/A21.50-02 - FOR THICKNESS DESIGN OF DUCTILE IRON PIPE AND WITH ASTM A536-84 (2004)

2. AT LEAST 46 PSI AT 5% PIPE DIAMETER DEFLECTION, AS MEASURED IN ACCORDANCE WITH ASTM

MATERIAL CONFORMING TO ASTM D3212-96A(2003)E1 AND SHALL BE PUSH-ON OR BELL-AND-SPIGOT

THIS PORTION OF HOUSE

SEWER BY OTHERS

- BUILDING

CLEAN OUT

~ BASEMENT

✓ FLOOR

NOTE: HOUSE SEWER MAY ALSO BE LOCATED BELOW BASEMENT FLOOR

WHEN REQUIRED

3. JOINT SEALS FOR PVC PIPE SHALL BE OIL RESISTANT COMPRESSION RINGS OF ELASTOMERIC

JOINTS SHALL BE DEPENDENT UPON PROPER MATERIALS (SEE NOTE #2) FOR WATER TIGHTNESS, AND ALL JOINTS SHALL BE PROPERLY MATCHED WITH THE PIPE MATERIALS USED. WHERE DIFFERING MATERIALS ARE TO BE

CONNECTED, AS AT THE STREET SEWER WYE OR AT THE FOUNDATION WALL, APPROPRIATE MANUFACTURED

JOINT

- 8" PVC WITHIN R.O.W.

APPROVED BACKFLOW PREVENTER TO BE

HOUSE SEWER: 4" (OR 6") PVC SDR 35.

INSTALLED WERE DIRECTED.

DETECTABLE

WARNING TAPE

MINIMUM SLOPE 1/8" PER FOOT

(SEE NOTE #4) \

SELECTED BACKFILL

COMPACTED

TO BE THOROUGHLY

GRANULAR MATERIAL

MAXIMUM SIZE 1"

MIRAFI 140N FILTER

A. DUCTILE IRON PIPE AND FITTINGS SHALL CONFORM TO THE FOLLOWING STANDARDS OF THE AMERICAN

B. PLASTIC GRAVITY SEWER PIPE AND FITTINGS SHALL COMPLY WITH THE FOLLOWING STANDARDS:

B. JOINTS SHALL BE MECHANICAL, PUSH-ON OR BALL-AND-SOCKET TYPE.

CLEAR OPENING 30" ADJUST TO GRADE WITH BRICK FRAME TO BE SET IN (2 COURSE MINIMUM BED OF MORTAR 5 COURSE MAXIMUM) - ECCENTRIC CONE BITUMINOUS COATING 48" MINIMUM DOUBLE ROLL APPROVED PREFORMED BITUMA\$TIC SEALANT **BITUMASTIC** 6" BEDDING IN EARTH 12" IN LEDGE (SEE NOTE #5) TYPICAL SECTION` MAY BE OMITTED WHEN MANHOLE IS CAST IN PLACE STAINLESS STEEL -CLAMP MANHOLE " (MIN.) FILL WITH ----MORTAR (6" MINIMUM ALUMINUM ANODIZED. **MAXIMUM PROJECTION** INTERNAL OF PIPE INTO MANHOLE CLAMP - NEOPRENE-LIKE KOR-N-SEAL KOR-N-SEAL JOINT SLEEVE (OR EQUAL) BASE THICKNESS TO BE FULL WALL THICKNESS AND **BRICK MASONRY** SECTION A-A MONOLITHIC TO A POINT 6" ABOVE THE PIPE CROWN. 12" MINIMUM EACH SIDE TOP OF SHELF SHALL BE 1" ABOVE CROWN OF HIGHEST PIPE CARE SHALL BE TAKEN TO INSURE THAT THE BRICK INVERT TEST IS A SMOOTH CONTINUATION OF THE SEWER INVERT. INVERT **SECTION B-B** BRICKS SHALL BE LAID ON EDGE.

SANITARY SEWER MANHOLE NOT TO SCALE

PROTECT AGAINST PIPE PENETRATION OR FAILURE AT THE FITTING BY THE USE OF BELL-ON-BELL CONNECTIONS. FOR EXISTING SEWER WHERE FITTINGS CANNOT BE INSTALLED, SADDLE CONNECTIONS SHALL BE USED. PRESSURE SEWERAGE SHALL HAVE AN ISOLATION VALVE OR CURB STOP VALVE INSTALLED AT THE PROPERTY LINE. IF A CHECK VALVE IS USED AT THE PROPERTY LINE. THE VALVE

B. PIPES SHALL BE CAREFULLY BEDDED ON A 4 INCH LAYER OF CRUSHED STONE AND/OR GRAVEL. . BEDDING AND RE-FILL, FOR A DEPTH OF 12 INCHES ABOVE THE TOP OF THE PIPE, SHALL BE CAREFULLY AND THOROUGHLY TAMPED BY HAND OR WITH THE APPROPRIATE MECHANICAL

D. THE PIPE SHALL BE LAID AT A CONTINUOUS AND CONSTANT GRADE FROM THE STREET SEWER

PIPE JOINTS MUST BE MADE UNDER DRY CONDITIONS. IF WATER IS PRESENT, ALL NECESSARY

OLLOWING MANNERS: (PRIOR TO BACKFILLING) A. AN OBSERVATION TEE SHALL BE INSTALLED AS SHOWN AND WHEN READY FOR TESTING, AN

AS POSSIBLE, WET TRENCH CONDITIONS OR, IF THE TRENCH IS WET, THE GROUND WATER SHALL BE PERMITTED TO RISE IN THE TRENCH OVER THE PIPE. INSPECTIONS FOR LEAKS SHALL BE MADE.

IS DRY, THE PIPE SHALL BE LIBERALLY HOSED WITH WATER, OR IF THE TRENCH IS WET. GROUND WATER SHALL BE PERMITTED TO RISE IN THE TRENCH OVER THE PIPE. OBSERVATION FOR LEAKS SHALL BE MADE IN THE FIRST DOWNSTREAM MANHOLE.

THE PIPE SHALL BE DUG-UP, IF NECESSARY, AND RE-LAID SO AS TO ASSURE WATER-TIGHTNESS. ILLEGAL CONNECTIONS: NOTHING BUT SANITARY WASTE FLOW FROM TOILETS, SINKS, LAUNDRY, ETC. SHALL BE PERMITTED. ROOF LEADERS, FOOTING DRAINS, SUMP PUMPS OR ANY OTHER SIMILAR CONNECTION CARRYING RAIN WATER, DRAINAGE OR GROUND WATER, SHALL NOT BE PERMITTED.

9. WATER SERVICE SHALL NOT BE LAID IN THE SAME TRENCH AS THE SEWER SERVICE, UNLESS NECESSARY AND APPROVED BY THE AHJ. WHEN NECESSARY, THE WATER SERVICE SHALL BE PLACED ABOVE AND TO ONE SIDE OF THE SEWER SERVICE, AS SHOWN.

ADDITION, A FERROUS MATERIAL, ROD OR PIPE SHALL BE PLACED OVER THE WYE TO AID IN LOCATING THE BURIED PIPE WITH A DIP NEEDLE OR PIPE FINDER.

11. CHIMNEY CONNECTIONS ARE ONLY PERMITTED IF ALLOWED BY THE AHJ. ANY VERTICAL RISE GREATER THAN 4 FEET SHALL BE PROVIDED WITH ADDED SUPPORT BY ENCASING THE FITTING AND RISER IN A HOUSE WATER PRECAST CONCRETE CHIMNEY. UP TO 12 FEET OF VERTICAL RISE CAN ALSO BE SECURED BY PROPER MEANS AS LONG AS IT CONSISTS OF A BELL-ON-BELL CONNECTION PROPERLY PROTECTED AGAINST PIPE PENETRATION AND IF IT IS ALLOWED BY THE AHJ.

COMPACTED TO 95% OF THE MODIFIED PROCTOR TEST DENSITY.

5. SERVICE CONNECTIONS SHALL USE SANITARY TEE OR WYE FITTINGS FOR ALL NEW CONSTRUCTION. THE CENTERLINE OF ALL BUILDING CONNECTIONS SHALL ENTER THE TOP HALF OF THE SEWER. ANY SERVICE CONNECTION WITH A VERTICAL RISE UP TO 4 FEET MAY HAVE THE SEWER FITTING SET VERTICALLY. ANY SERVICE CONNECTION WITH A VERTICAL RISE UP TO 12 FEET SHALL EMPLOY NON-ENCASED RISERS THAT SHALL BE INSTALLED WITHIN A VAULT TO FACILITATE MAINTENANCE. ROOF DOWNSPOUTS, EXTERIOR OR INTERIOR FOUNDATION DRAINS, SUMP PUMPS OR OTHER SOURCE OF SURFACE WATER RUN-OFF OR GROUND WATER SHALL NOT BE DIRECTLY OR INDIRECTLY CONNECTED TO A PUBLIC SEWER.

PIPE INSTALLATION: A. THE PIPE SHALL BE HANDLED, PLACED AND JOINTED IN ACCORDANCE WITH INSTALLATION GUIDES

OF THE APPROPRIATE MANUFACTURER.

CONNECTION TO THE HOUSE FOUNDATION AT A GRADE OF NOT LESS THAN 1/8 INCH PER FOOT.

STEPS SHALL BE TAKEN TO DEWATER THE TRENCH. STING: THE COMPLETED HOUSE SEWER SHALL BE SUBJECTED TO A LEAKAGE TEST IN ANY OF THE

INFLATABLE BLADDER OR PLUG SHALL BE INSERTED JUST UPSTREAM FROM THE OPENING IN THE TEE. AFTER INFLATION, WATER SHALL BE INTRODUCED INTO THE SYSTEM ABOVE THE PLUG TO A HEIGHT OF 5 FEET ABOVE THE LEVEL OF THE PLUG. B. THE PIPE SHALL BE LEFT EXPOSED AND LIBERALLY HOSED WITH WATER TO SIMULATE, AS NEARLY

THROUGH THE CLEAN OUT WITH A FLASHLIGHT. C. DRY FLUORESCENCE DYE SHALL BE SPRINKLED INTO THE TRENCH OVER THE PIPE. IF THE TRENCH

D. LEAKAGE OBSERVED IN ANY OF THE ABOVE TESTS SHALL BE CAUSE FOR NON-ACCEPTANCE AND

LOCATION: THE LOCATION OF THE WYE SHALL BE RECORDED AND FILED IN THE MUNICIPAL RECORDS. IN

12. UNLESS OTHERWISE NOTED, ALL GRANULAR MATERIAL SHALL BE PLACED IN 12" MAXIMUM LIFTS AND

MAXIMUM DISTANCE TO FLEXIBLE JOINT INVERT AND SHELF TO BE PLACED AFTER LEAKAGE

- NHDOT FRAME AND COVER,

(MARCH 2011)

17. MANHOLE STEPS ARE NOT PERMITTED BY THE TOWN.

18. MANHOLE TESTING: A. MANHOLES SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST. B. THE MANHOLE VACUUM TEST SHALL CONFORM TO THE FOLLOWING: 1. THE INITIAL VACUUM GAUGE TEST PRESSURE SHALL BE 10 INCHES Hg: AND

1. ALL COMPONENT PARTS OF MANHOLE STRUCTURES SHALL HAVE THE STRENGTH, LEAK RESISTANCE AND

3. MANHOLE STRUCTURES SHALL BE DESIGNED TO WITHSTAND HS-20 LOADING AND SHALL NOT LEAK IN EXCESS

BARRELS, CONE SECTIONS, AND CONCRETE GRADE RINGS SHALL BE CONSTRUCTED OF PRECAST REINFORCED

BASE SECTIONS SHALL BE OF MONOLITHIC CONSTRUCTION TO A POINT AT LEAST 6 INCHES ABOVE THE CROWN

HORIZONTAL JOINTS BETWEEN SECTIONS OF PRECAST CONCRETE BARRELS SHALL BE OF AN OVERLAPPING

TYPE, SEALED FOR WATER-TIGHTNESS USING A DOUBLE ROW OF AN ELASTOMERIC OR MASTIC-LIKE SEALANT.

C. ELASTOMERIC SEALING RING CAST IN THE MANHOLE OPENING WITH SEAL FORMED ON THE

10. ALL PRECAST SECTIONS AND BASES SHALL HAVE THE DATE OF MANUFACTURE AND THE NAME OR TRADEMARK

12. MANHOLES THAT ARE NOT REPLACING EXISTING MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT

CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW. AT CHANGES IN DIRECTION, THE INVERTS SHALL

BE LAID OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LINE OF THE SEWER

PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE HIGHEST PIPE CROWN AND SLOPED TO

13. REPLACEMENT MANHOLES WHERE THERE IS AN ESTABLISHED LINE AND GRADE THROUGH WHICH THE SEWER

14. WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED IN LIEU OF

A. CONCRETE FOR CAST-IN-PLACE BASES OR COMPLETE MANHOLES SHALL CONFORM TO THE

REQUIREMENTS FOR CLASS AS CONCRETE IN THE NEW HAMPSHIRE DEPARTMENT OF

D. THE MANHOLE FRAME AND COVER SHALL PROVIDE A 30-INCH DIAMETER CLEAR OPENING;

TRANSPORTATION'S "STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION";

E. THE MANHOLE COVER SHALL HAVE THE WORD "SEWER" IN 3-INCH LETTERS CAST INTO THE TOP

F. THE CASTINGS SHALL BE OF EVEN-GRAINED CAST IRON, SMOOTH AND FREE FROM SCALE, LUMPS,

G. CONTACT SURFACES OF COVERS AND FRAMES SHALL BE MACHINED AT THE FOUNDRY TO PREVENT

I. BRICK MASONRY FOR SHELF, INVERT AND GRADE ADJUSTMENT SHALL COMPLY WITH ASTM C32-05,

M. HYDRATED LIME SHALL BE TYPE S CONFORMING TO THE ASTM C207-06 "STANDARD SPECIFICATIONS

N. SAND SHALL CONSIST OF INERT NATURAL SAND CONFORMING TO THE ASTM C33-03 "STANDARD

J. MORTAR SHALL BE COMPOSED OF PORTLAND CEMENT AND SAND WITH OR WITHOUT HYDRATED

2. 4.5 PARTS SAND, ONE PART CEMENT AND 0.5 PARTS HYDRATED LIME;

O. CONCRETE FOR DROP SUPPORTS SHALL CONFORM TO THE REQUIREMENT FOR CLASS AAA

CONCRETE OF THE NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION'S "STANDARD

P. SUBJECT TO (Q) BELOW, A FLEXIBLE PIPE JOINT SHALL BE PROVIDED WITHIN THE FOLLOWING

Q. NO FLEXIBLE JOINT SHALL BE REQUIRED FOR DI PIPE OR FOR PVC PIPE UP THROUGH 15-INCH

R. WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED IN LIEU OF A CONE SECTION, PROVIDED THE SLAB HAS AN ECCENTRIC ENTRANCE OPENING

WITHIN 48-INCHES FOR REINFORCED CONCRETE (RC) PIPE; AND

2. WITHIN 60-INCHES FOR PVC PIPE LARGER THAN 15-INCH DIAMETER;

CONFORM TO THE REQUIREMENTS OF THE NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION'S

PRECAST CONCRETE BARREL SECTIONS, CONES AND BASES SHALL CONFORM TO ASTM C478-06;

B. REINFORCING FOR CAST-IN-PLACE CONCRETE SHALL BE STEEL OR STRUCTURAL FIBERS THAT

CROWN AND SLOPED TO DRAIN TOWARD THE FLOWING THROUGH CHANNEL

"STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION":

H. CASTINGS SHALL BE EQUAL TO CLASS 30, CONFORMING TO ASTM A48/48M-03;

... CEMENT SHALL BE TYPE II PORTLAND CEMENT CONFORMING TO ASTM C150-05;

A CONE SECTION, PROVIDED THE SLAB HAS AN ECCENTRIC ENTRANCE OPENING AND BE CAPABLE OF

DRAIN TOWARD THE FLOWING THROUGH CHANNEL. UNDERLAYMENT OF INVERT AND SHELF SHALL CONSIST OF

A. A BRICK PAVED SHELF AND INVERT CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW

B. A PRECAST CONCRETE SHELF AND INVERT WITH THE SHELF CONSTRUCTED TO THE ELEVATION OF THE HIGHEST PIPE CROWN AND SLOPED TO DRAIN TOWARD THE FLOWING THROUGH CHANNEL; OR

C. A FIBERGLASS INSERT WITH THE SHELF CONSTRUCTED TO THE ELEVATION OF THE HIGHEST PIPE

A. ELASTOMERIC, RUBBER SLEEVE WITH WATERTIGHT JOINTS AT THE MANHOLE OPENING AND PIPE

D. NON-SHRINK GROUTED JOINTS WHERE WATERTIGHT BONDING TO THE MANHOLE AND PIPE CAN BE

MANHOLE STRUCTURES SHALL HAVE A LIFE EXPECTANCY OF AT LEAST 25 YEARS.

OF ONE GPD PER VERTICAL FOOT OF MANHOLE FOR THE LIFE OF THE STRUCTURE.

B. CAST INTO THE WALL OR SECURED WITH STAINLESS STEEL CLAMPS;

SURFACE OF THE PIPE BY COMPRESSION OF THE RING; AND

OF THE MANUFACTURER IMPRESSED OR INDELIBLY MARKED ON THE INSIDE WALL.

BRICK MASONRY. INVERTS AND SHELVES SHALL BE PLACED AFTER TESTING.

15. THE MINIMUM INTERNAL DIAMETER OF MANHOLES SHALL BE 48 INCHES

16. MATERIALS OF CONSTRUCTION FOR MANHOLES SHALL BE AS FOLLOWS.

BLISTERS, SAND HOLES AND DEFECTS;

ROCKING OF COVERS IN ANY ORIENTATION:

CLAY OR SHALE, FOR GRADE SS HARD BRICK;

FOR HYDRATED LIME FOR MASONRY PURPOSES"

DISTANCES FROM ANY MANHOLE CONNECTION:

AND IS CAPABLE OF SUPPORTING H-20 LOADS.

K. PROPORTIONS IN MORTAR OF PARTS BY VOLUMES SHALL BE:

SPECIFICATIONS FOR CONCRETE, FINE AGGREGATES";

SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION";

4.5 PARTS SAND AND 1.5 PARTS CEMENT; OR

11. ALL PRECAST SECTIONS AND BASES SHALL BE COATED ON THE EXTERIOR WITH A BITUMINOUS

SPACE NECESSARY FOR THE INTENDED SERVICE.

7. PIPE TO MANHOLE JOINTS SHALL BE AS FOLLOWS:

9. MANHOLE CONE SECTIONS SHALL BE ECCENTRIC IN SHAPE.

ENTERS AND EXITS THE MANHOLE SHALL HAVE:

AS REQUIRED IN (12) ABOVE.

SURFACES:

OBTAINED.

DAMP-PROOFING COATING.

SUPPORTING HS-20 LOADS.

SURFACE

LIME ADDITION:

CONCRETE

OF THE INCOMING PIPE.

2. THE MINIMUM ACCEPTABLE TEST HOLD TIME FOR A 1-INCH Hg PRESSURE DROP TO 9 INCH Hg SHALL BE a. NOT LESS THAN 2 MINUTES FOR MANHOLES LESS THAN 10 FEET DEEP IN DEPTH;

b. NOT LESS THAN 2.5 MINUTES FOR MANHOLES 10 TO 15 FEET DEEP; AND c. NOT LESS THAN 3 MINUTES FOR MANHOLES MORE THAN 15 FEET DEEP. THE MANHOLE SHALL BE REPAIRED AND RETESTED IF THE TEST HOLD TIMES FAIL TO ACHIEVE THE

ACCEPTANCE LIMITS SPECIFIED IN (B) ABOVE D. FOLLOWING COMPLETION OF THE LEAKAGE TEST, THE FRAME AND COVER SHALL BE PLACED ON THE TOP OF THE MANHOLE OR SOME OTHER MEANS USED TO PREVENT ACCIDENTAL ENTRY BY UNAUTHORIZED PERSONS, CHILDREN OR ANIMALS UNTIL THE CONTRACTOR IS READY TO MAKE FINAL ADJUSTMENTS TO GRADE.

CONSTRUCTION DETAILS FRENETTE GARDENS

MAP 182 LOT 3 65 CENTRAL STREET HUDSON, NEW HAMPSHIRE HILLSBOROUGH COUNTY

OWNERS/APPLICANTS OF MAP 182 LOT 3:

LAURI RIPALDI 46 BUSH HILL ROAD HUDSON, NH 03051 9531/2754

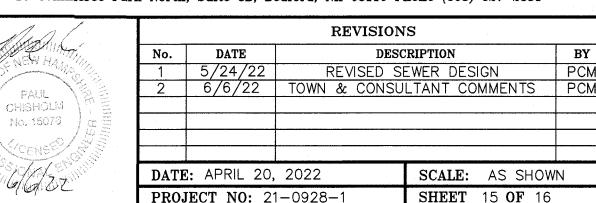
KIMBERLY FRENETTE 8B DUMONT ROAD HUDSON, NH 03051 9531/2754

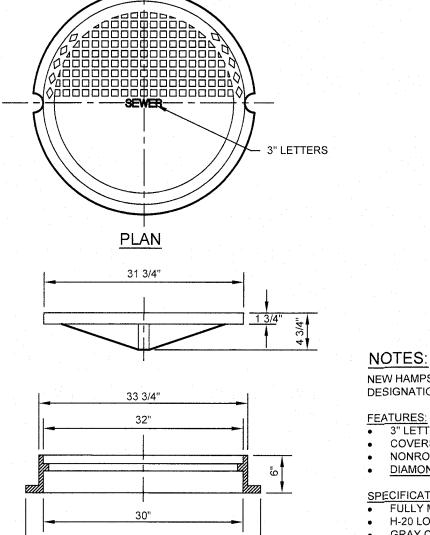
RICKY FRENETTE 14 TATE STREET HUDSON, NH 03051 9531/2754



■ KEACH-NORDSTROM ASSOCIATES, INC.

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NEW HAMPSHIRE MAINTAINS A CLEAR OPENING DESIGNATION OF 30" FOR ITS MANHOLE CASTINGS.

FEATURES:

• 3" LETTERING

 COVERS MARKED SEWER NONROCKING COVER

DIAMOND SURFACE DESIGN

FULLY MACHINED FRAME AND COVER H-20 LOAD RATED

• GRAY CAST IRON MEETS ASTM A48 CLASS 30

SECTION

SEWER MANHOLE FRAME AND COVER DETAIL

(MARCH 2008)

APPROVED BY THE HUDSON, NH PLANNING BOARD DATE OF MEETING: SIGNATURE DATE:_ SIGNATURE DATE: _ SUBDIVISIONS ARE VALID FOR TWO YEARS FROM THE DATE OF PLANNING BOARD MEETING FINAL APPROVAL. FOR AN APPLICANT TO GAIN AN EXEMPTION FROM ALL SUBSEQUENT CHANGES IN SUBDIVISION REGULATIONS, SITE PLAN

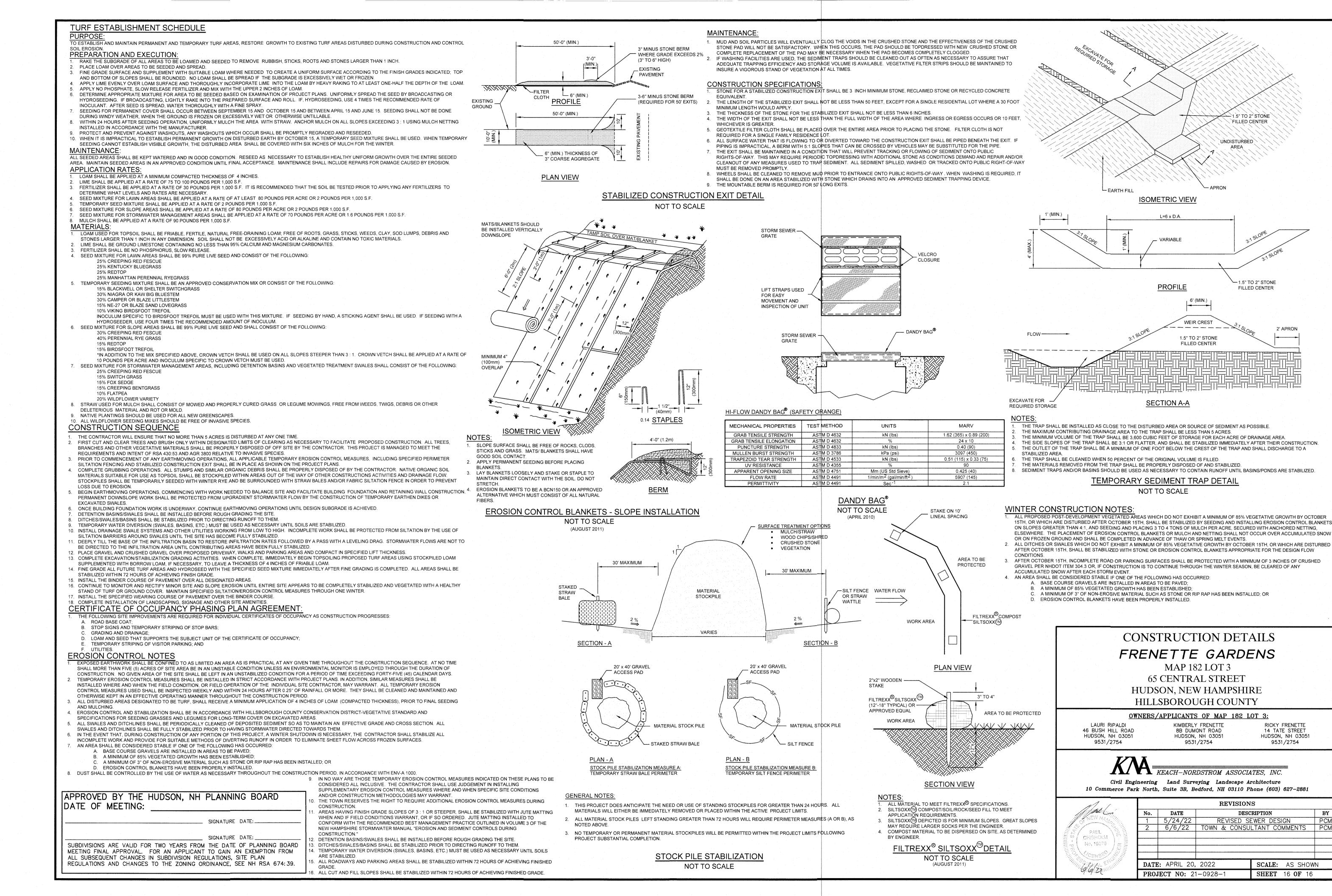
REGULATIONS AND CHANGES TO THE ZONING ORDINANCE, SEE NH RSA 674:39.

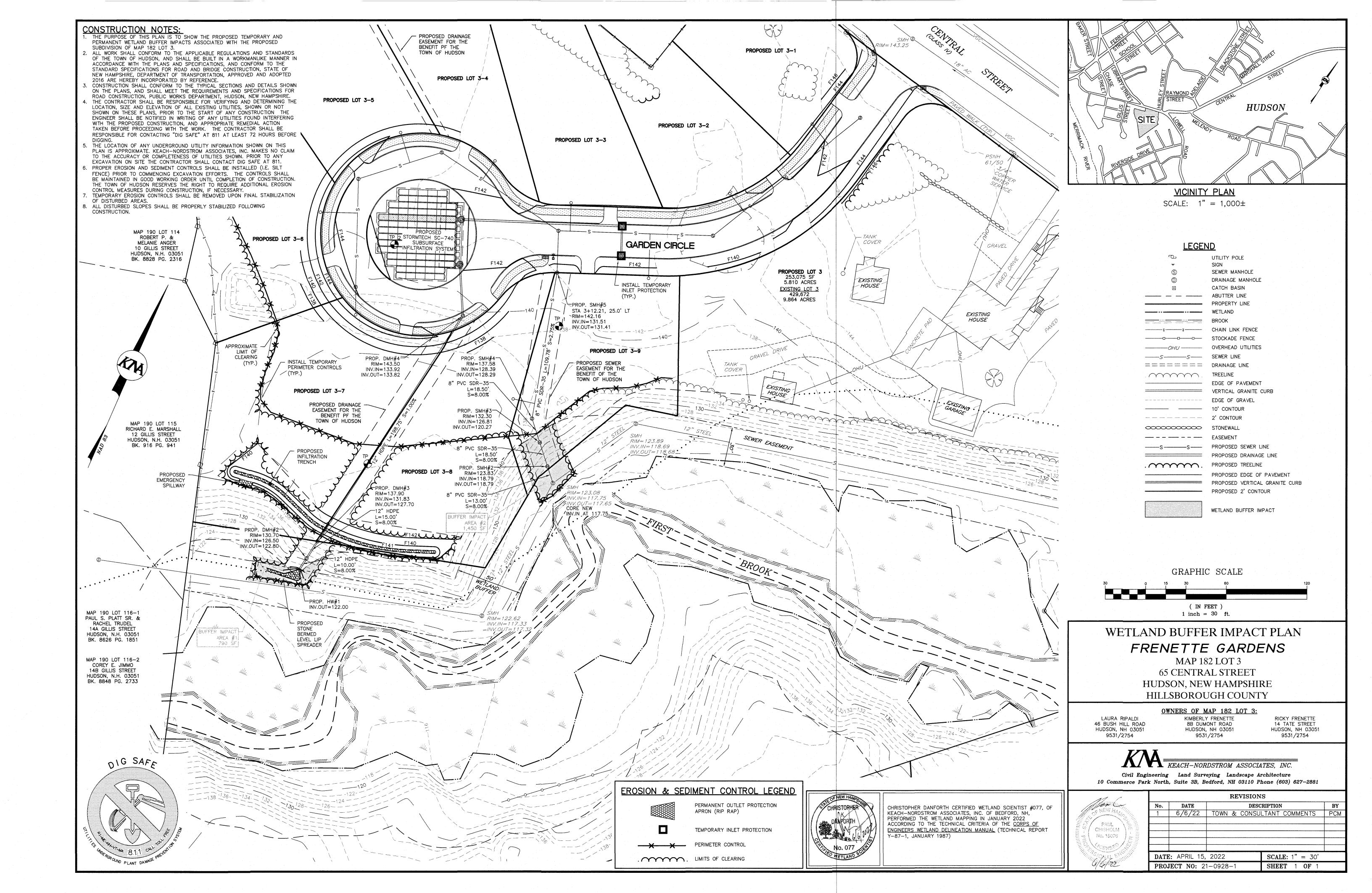
39 1/4"

NOT TO SCALE

SANITARY SEWER SERVICE DETAIL NOT TO SCALE

FABRIC, OR APPROVED EQUAL BEDDING TO BE SEWER THOROUGHLY COMPACTED (SEE NOTE #12) -6" (MIN.) IN EARTH WATER AND SEWER 12" (MIN.) IN LEDGE IN SAME TRENCH TRENCH CROSS-SECTION





Stormwater Management Report

Frenette Gardens

Map 182; Lot 3 **65 Central Street Hudson, New Hampshire**

April 20, 2022

Revised: June 6, 2022

KNA Project No. 21-0928-1

Prepared For:

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OPERATION AND MAINTENANCE MANUAL PRE-DEVELOPMENT DRAINAGE AREAS PLAN POST-DEVELOPMENT DRAINAGE AREAS PLAN

I. INTRODUCTION

A. Project Description

The project proposes to subdivide the existing parcel, located at 65 Central Street, into ten (10) new residential lots and construct approximately 700 feet of new roadway, culminating in a cul-de-sac. Roadway construction also entails the installation of public utilities, including water, sewer, drainage, gas, underground electric, and telecommunications services. The proposed stormwater management system includes a subsurface infiltration system, consisting of Stormtech SC-740 chambers, and two stone bottomed infiltration trenches as well as a closed drainage system which directs runoff into said subsurface infiltration system.

B. Existing Site Conditions

The subject property, prior to the subdivision, is approximately 9.88 acres in total area, and is located at 65 Central Street in Hudson's Town Residential (TR) Zoning District. The lot is currently developed with a single-family house in the northeast corner. It is bisected by First Brook to the south of the existing house. The parcel is bordered by Central Street to the north and several single-family houses to the east, south, and west. The lot currently has access from Central Street.

According to the Natural Resources Conservation Service (NRCS) web soil survey, the predominant soil types onsite are Windsor-Urban Land Complex with slopes ranging from 3-15% and Windsor Loamy Sand, with slopes ranging from 15-35%. Both soils are classified as Hydrologic Soil Group (HSG) 'A'.

II. STORM DRAINAGE ANALYSIS & DESIGN

A. Methodology

In accordance with the provisions of the Town of Hudson, and generally accepted engineering practice, the 2-year, 10-year, 25-year, and 50-year frequency storms have each been used in the various aspects of analysis and design of stormwater management considerations for the subject site. All proposed stormwater measures have been designed to not overtop in the 50-year frequency storm.

KNA utilizes HydroCAD version 10.0 to analyze both pre and post-development watershed characteristics. This computer software system is based largely on hydrology techniques (TR-20) developed by the Soil Conservation Service (now the Natural Resources Conservation Service). In addition, the software derives Time of Concentration values using the methodology contained within USDA-S.C.S. publication <u>Urban Hydrology for Small Watersheds Technical Release No. 55 (TR 55)</u>.

All design and analysis calculations performed using the referenced methodologies are attached to this report. The minimum time of concentrations used for the analysis is 6 minutes. These calculations document each catchment area, a breakdown of surface type, time of concentration, rainfall intensity, peak discharge volume, Manning's "n" value, peak velocity, and other descriptive design data for each watershed and pipe segment evaluated. In addition, the "Pre/Post Development Drainage Area Plans" graphically define and illustrate the extent of each watershed or catchment area investigated.

B. Pre-Development Drainage Conditions

In the pre-development scenario, three (3) point of analysis (POA) have been identified as the appropriate points to compare pre vs. post development rates of stormwater discharge. These points of analysis reflect the main discharge point of the site and were analyzed to show the impact from the proposed improvements.

The pre-development drainage model's POA's are further described as follows:

Link ALink BCentral StreetFirst Brook Tributary

➤ Link C First Brook

In general, the site slopes from a central high point in the existing field downward to the three points of analysis. Runoff from a small portion of the front of the lot along Central Street and half the roof of the existing house flows to the roadway and is collected in the existing drainage network (Link A). Runoff from the western portion of the lot flows over the property line and into a small brook on the abutting lots (Link B), which eventually feeds into First Brook. Finally, runoff from most of the site is conveyed to First Brook (Link C) by overland flow. There are two existing depressions on site, which are currently used as gardens by the property owner. These depressions are included in the drainage analysis. For a more visual description of the information presented in this section, please refer to the attached "Pre-Development Drainage Areas Plan" attached in the appendix of this report.

C. Post-Development Drainage Conditions:

The same POA's that were identified in the pre-development scenario have been analyzed in the post-development scenario.

The proposed stormwater management system utilizes both open and closed practices for the collection, detention, treatment, and recharge of runoff. Stormwater runoff generated from the proposed roadway and most of the developed lots, will be collected by two catch basins and piped to a subsurface infiltration system located under the grass panel at the center of the cul-de-sac. This BMP was selected for the site as part of a pilot program proposed by the Town of Hudson to move away from open detention basins and shift towards less intrusive subsurface stormwater solutions. It is designed to mitigate peak rates and provide the required treatment and recharge volumes per town regulations. Outfall from the system will be piped to the toe of slope along the embankment leading down to the brook, where it will be diffused by a stone bermed level lip spreader before discharging to the wetland. The bottom of this system will lie below the frost line and ensure that this BMP will continue to operate as intended during frozen ground conditions.

It is important to note that a typical 2,000 square foot lot development envelope of impervious area was assumed for the drainage calculations, to properly size the stormwater BMP's. This approximate area was determined by assuming each lot will be developed with a 1,500-sf house and a 500-sf driveway. This means that the nine proposed lots contribute an additional 18,000-sf of impervious area. The subsurface infiltration system was designed with the intent of having 14,000-sf of impervious lot area (and the roadway) drain to the BMP based on assumed lot grading. The 4,000-sf of remaining impervious lot area (back half of roofs) is accounted for by the construction of two proposed infiltration trenches to be located along the rear property lines of Lots 3-4, 3-5, 3-6, 3-7, and 3-8. These trenches include two feet of washed, crushed stone wrapped in fabric and one foot ponding area with a ten-foot overflow spillway in the berm. Outfall from these trenches will flow overland to First Brook and its tributary. Additionally, both trenches have been designed to not overtop in the 50-

year storm event under frozen ground conditions by removing infiltration from the drainage analysis.

The peak stormwater runoff rate and the channel protection requirements for the specific storm frequencies are presented and analyzed in the subsequent summary section of this report (Tables 1 & 2). For a more visual description of the information presented in this section, please refer to the attached "Post-Development Drainage Areas Plan" attached in the appendix of this report.

D. Summary:

The subject site complies with the Town of Hudson regulations regarding stormwater treatment and groundwater recharge volume. Proposed stormwater best management practices (BMP) are designed in accordance with the <u>New Hampshire Stormwater Manual Volume 2: Post-Construction Best Management Practices Selection and Design and BMP worksheets provided by the New Hampshire Department of Environmental Services. In addition, stormwater discharges, in terms of peak rate of runoff and total volume, are consistent with the Town of Hudson Stormwater Regulations. The results are reported below in Table 1 and 2.</u>

Table 1: Peak Flow Discharge Rate

S	ite Pre-D)evelopm	ent vs. P	ost-Deve	lopment	(cfs)		
Description	2-Y	'ear	10-`	Year	25-`	Year	50-	/ear
24-hr Rainfall	2.95	in/hr	4.45	in/hr	5.62	in/hr	6.72	in/hr
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Α	0.20	0.20	0.30	0.30	0.38	0.38	0.52	0.50
В	0.22	0.21	0.33	0.33	0.43	0.42	0.71	0.55
С	0.89	0.88	1.36	1.35	1.77	1.74	2.49	2.48

Table 2: Stormwater Runoff Volume

Site Pre-Development vs. F	Post Development (Storr	n Volume in Acre-Feet)
Description	2-Y	ear
24-hr Rainfall	2.95	in/hr
	Pre	Post
Α	0.02	0.02
В	0.02	0.02
С	0.11	0.11

III. EROSION & SEDIMENTATION CONTROL PROVISIONS

A. Temporary Erosion Control Measures

As an integral part of the engineering design of this site, an erosion and sedimentation control plan has been developed with the intent of limiting the potential for soil loss and associated receiving water quality degradation, both during and after the construction period. As the project plans indicate, traditional temporary erosion and sedimentation control devices and practices, such as siltation fencing and temporary block and sediment barriers at. In preparation of these provisions, reference was made to the New Hampshire Stormwater Manual; Volume 3: Erosion and Sediment Temporary Controls During Construction. Construction details for each temporary erosion control measure and practice specified have been added to the project plans. These plans also contain a number of

erosion control notes, which are offered to the selected contractor in order to supplement the specified measures and practices to the extent practical.

B. Construction Sequence

A site-specific construction sequence sensitive to limiting soil loss due to erosion and associated water quality degradation was prepared specifically for this project and is shown on the project plans. As pointed out in the erosion control notes, it is important for the contractor to recognize that proper judgment in the implementation of work will be essential if erosion is to be limited and protection of completed work is to be realized. Moreover, any specific changes in sequence and/or field conditions affecting the ability of specific erosion control measures to adequately serve their intended purpose should be reported to this office by the contractor. Further, the contractor is encouraged to supplement specified erosion control measures during the construction period where and when in his/ her best judgment additional protection is warranted.

C. Permanent Erosion Control Measures

In the design of this site, consideration was given to limiting the potential for long-term erosion of completed improvements. As a result, several permanent erosion control measures were incorporated into the site design. These provisions include:

- 1) Specification of a turf establishment schedule and seed mixture, utilizing materials and workmanship recognized as appropriate for the site conditions at hand; and
- 2) The design has provided catch basins with sumps to capture runoff and reduce the overland flow, thereby reducing erosion.
- 3) Multiple infiltration practices were designed to reduce runoff and volume.

FIGURES AND SPREADSHEETS

FIGURE NO. 1 – AERIAL IMAGE

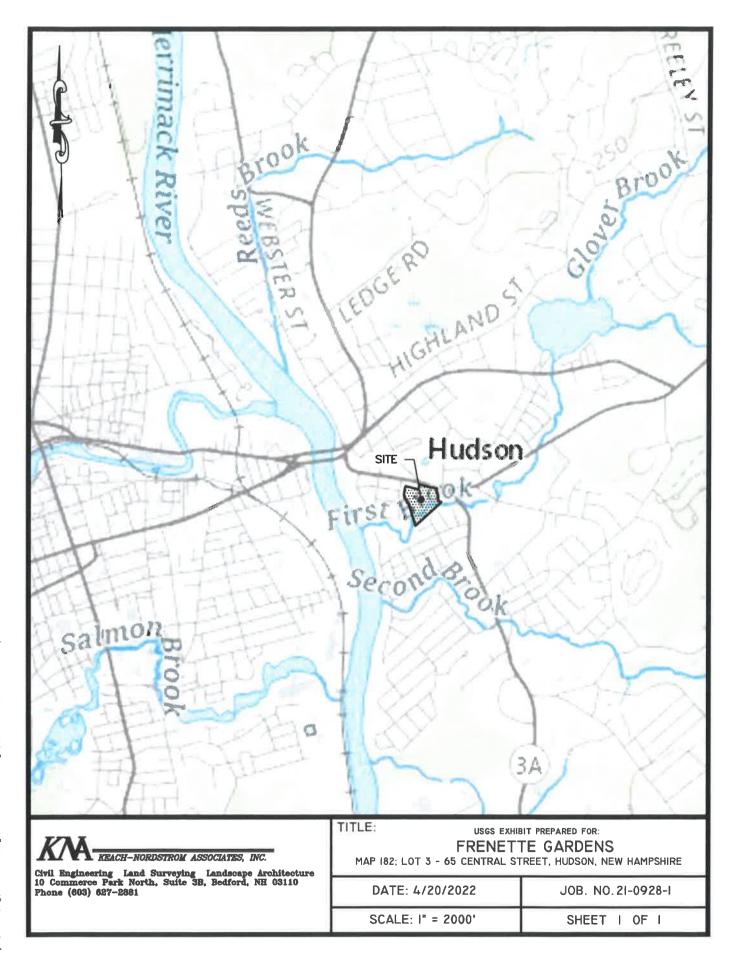
FIGURE NO. 2 – USGS IMAGE

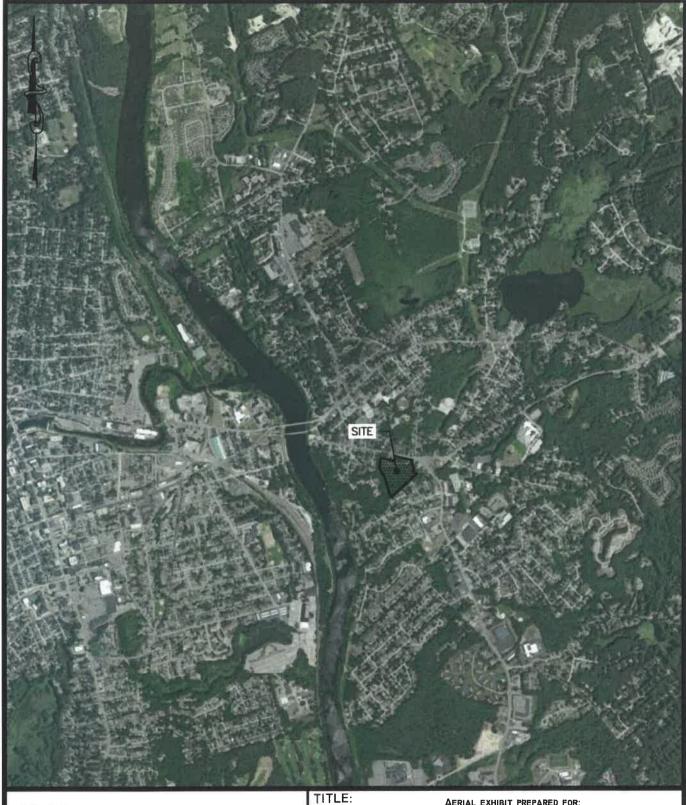
FIGURE NO. 3 - SCS SOILS MAP

FIGURE NO. 4 - EXTREME PRECIPITATION TABLES

FIGURE NO. 5 - GROUNDWATER RECHARGE VOLUME CALCULATION

FIGURE NO. 6 - BMP WORKSHEETS







KEACH-NORDSTROM ASSOCIATES, INC.

Civil Engineering Land Surveying Landscape Architecture 10 Commerce Park North, Suite 3B, Bedford, NH 03110 Phone (603) 627–2881

AERIAL EXHIBIT PREPARED FOR:

FRENETTE GARDENS
MAP 182; LOT 3 - 65 CENTRAL STREET, HUDSON, NEW HAMPSHIRE

DATE: 4/20/2022	JOB. NO.2I-0928-i
SCALE: I" = 2000'	SHEET OF



Natural Resources
Conservation Service

Web Soil Survey National Cooperative Soil Survey

2/14/2022 Page 1 of 4

MAP INFORMATION

MAP LEGEND

The soil surveys that comprise your AOI were mapped at

contrasting soils that could have been shown at a more detailed line placement. The maps do not show the small areas of misunderstanding of the detail of mapping and accuracy of soil Enlargement of maps beyond the scale of mapping can cause

Please rely on the bar scale on each map sheet for map

Source of Map: Natural Resources Conservation Service

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator accurate calculations of distance or area are required. Albers equal-area conic projection, should be used if more projection, which preserves direction and shape but distorts

This product is generated from the USDA-NRCS certified data as

Hillsborough County, New Hampshire, Eastern

Soil map units are labeled (as space allows) for map scales

Date(s) aerial images were photographed: Jun 19, 2020—Aug 6,

shifting of map unit boundaries may be evident. imagery displayed on these maps. As a result, some minor The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background

Hydrologic Soil Group

		Percent of AOI
WdD Windsor loamy sand, 15 to 35 percent slopes	7.2	39.4%
WnC Windsor-Urban land complex, 3 to 15 percent slopes	11.1	60.6%

Description

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

Rating Options

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified

Tie-break Rule: Higher

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing Yes

State New Hampshire

Location

Longitude 71.434 degrees West 42.761 degrees North

Elevation 0 feet

Date/Time Mon, 14 Feb 2022 16:02:56 -0500

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.27	0.42	0.52	0.68	0.85	1.07	1yr	0.74	1.01	1.24	1.56	1.96	2.48	2.72	1yr	2.19	2.61	3.04	3.73	4.34	1yr
2yr	0.33	0.51	0.64	0.84	1.05	1.32	2yr	0.91	1.21	1.53	1.91	2.37	2.95	3.28	2yr	2.61	3.15	3.66	4.38	4.98	2yr
5yr	0.39	0.61	0.77	1.03	1.32	1.67	5yr	1.14	1.52	1.93	2.42	3.00	3.73	4.17	5yr	3.30	4.01	4.64	5.51	6.22	5yr
10yr	0.44	0.70	0.88	1.20	1.56	1.99	10yr	1.34	1.80	2.32	2.90	3.60	4.45	5.00	10yr	3.94	4.81	5.55	6.54	7.37	10yr
25yr	0.53	0.83	1.06	1.46	1.94	2.51	25yr	1.68	2.25	2.93	3.67	4.56	5.62	6.37	25yr	4.97	6.13	7.05	8.22	9.21	25yr
50yr	0.59	0.95	1.21	1.70	2.30	3.00	50yr	1.99	2.66	3.51	4.42	5.48	6.72	7.66	50yr	5.94	7.36	8.45	9.78	10.92	50yr
100yr	0.68	1.10	1.42	2.01	2.73	3.58	100yr	2.36	3.16	4.20	5.28	6.55	8.03	9.20	100yr	7.10	8.85	10.13	11.63	12.94	100yr
200yr	0.77	1.26	1.63	2.35	3.24	4.28	200yr	2.80	3.75	5.03	6.34	7.85	9.60	11.06	200yr	8.49	10.64	12.14	13.84	15.34	200yr
500yr	0.93	1.53	2.00	2.90	4.07	5.41	500yr	3.51	4.70	6.38	8.05	9.96	12.17	14.13	500yr	10.77	13.58	15.44	17.43	19.22	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.22	0.35	0.42	0.57	0.70	0.80	1yr	0.60	0.78	1.06	1.32	1.67	2.28	2.56	1yr	2.01	2.46	2.71	3.01	3.71	1yr
2yr	0.32	0.49	0.60	0.81	1.00	1.20	2yr	0.86	1.17	1.37	1.79	2.30	2.89	3.20	2yr	2.56	3.08	3.57	4.27	4.87	2yr
5yr	0.36	0.55	0.69	0.94	1.20	1.42	5yr	1.04	1.39	1.63	2.11	2.69	3.50	3.88	5yr	3.10	3.73	4.27	5.14	5.81	5yr
10yr	0.39	0.61	0.75	1.05	1.36	1.60	10yr	1.17	1.57	1.82	2.39	3.04	4.04	4.49	10yr	3.58	4.32	4.91	5.88	6.64	10yr
25yr	0.45	0.68	0.85	1.21	1.59	1.88	25yr	1.38	1.83	2.13	2.81	3.54	4.88	5.48	25yr	4.32	5.27	5.89	7.04	7.89	25yr
50yr	0.49	0.74	0.92	1.33	1.79	2.13	50yr	1.54	2.08	2.41	3.20	3.99	5.66	6.38	50yr	5.01	6.13	6.78	8.07	9.00	50yr
100yr	0.53	0.81	1.01	1.46	2.00	2.40	100yr	1.73	2.35	2.73	3.50	4.49	6.47	7.45	100yr	5.72	7.17	7.81	9.27	10.22	100yr
200yr	0.59	0.88	1.12	1.62	2.26	2.73	200yr	1.95	2.66	3.07	3.95	5.09	7.48	8.73	200yr	6.62	8.39	9.00	10.64	11.65	200yr
500yr	0.67	0.99	1.27	1.85	2.63	3.23	500yr	2.27	3.16	3.61	4.66	6.02	9.10	10.81	500yr	8.05	10.39	10.85	12.78	13.84	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.31	0.48	0.58	0.78	0.96	1.12	1yr	0.83	1.10	1.27	1.66	2.10	2.63	2.87	1yr	2.33	2.76	3.44	4.23	4.78	1yr
2yr	0.35	0.54	0.67	0.91	1.12	1.31	2yr	0.97	1.28	1.49	1.93	2.47	3.05	3.39	2yr	2.70	3.26	3.78	4.50	5.14	2yr
5yr	0.44	0.67	0.83	1.14	1.46	1.67	5yr	1.26	1.63	1.90	2.43	3.05	4.02	4.53	5yr	3.55	4.36	5.00	5.92	6.64	5yr
10yr	0.52	0.81	1.00	1.40	1.80	2.04	10yr	1.56	1.99	2.31	2.91	3.62	4.97	5.64	10yr	4.40	5.42	6.21	7.27	8.11	10yr
25yr	0.68	1.03	1.28	1.83	2.41	2.65	25yr	2.08	2.59	2.98	3.68	4.51	6.59	7.54	25yr	5.83	7.25	8.27	9.56	10.59	25yr
50yr	0.82	1.25	1.55	2.23	3.00	3.23	50yr	2.59	3.16	3.63	4.41	5.34	8.17	9.39	50yr	7.23	9.03	10.26	11.76	12.96	50yr
100yr	1.00	1.51	1.89	2.73	3.75	3.94	100yr	3.23	3.85	4.42	5.45	6.32	10.24	11.67	100yr	9.06	11.22	12.75	14.49	15.88	100yr
200yr	1.21	1.83	2.32	3.35	4.68	4.81	200yr	4.04	4.70	5.36	6.55	7.49	12.71	14.51	200yr	11.25	13.95	15.83	17.86	19.47	200yr
500yr	1.58	2.36	3.03	4.41	6.27	6.24	500yr	5.41	6.10	6.96	8.37	9.37	16.91	19.30	500yr	14.96	18.56	21.09	23.54	25.50	500yr





GROUNDWATER RECHARGE VOLULME (GRV) CALCULATION (Env-Wq 1507.04)

0.87	ac	Area of HSG A soil that was replaced by impervious cover	0.40"
	ac	Area of HSG B soil that was replaced by impervious cover	0.25"
	ac	Area of HSG C soil that was replaced by impervious cover	0.10"
	ac	Area of HSG D soil or impervious cover that was replaced by impervious cover	0.0"
0.40	inches	Rd = Weighted groundwater recharge depth	
0.3472	ac-in	GRV = AI * Rd	
1,260	cf	GRV conversion (ac-in x 43,560 sf/ac x 1ft/12")	

Provide calculations below showing that the project meets the groundwater recharge requirements (Env-Wq 1507.04):
Subsurface Infiltration System provides 5,676 cf of recharge volume where 1,260 cf is required



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: Stormtech SC-740 System (1P)

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

Yes	Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
2.74 ac	A = Area draining to the practice	
0.79 ac	A _I = Impervious area draining to the practice	
0.29 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.31 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.85 ac-in	WQV= 1" x Rv x A	
3,079 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
770 cf	25% x WQV (check calc for sediment forebay volume)	
Isolator Row	Method of pretreatment? (not required for clean or roof runoff)	
N/A cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
5,676 cf	V = Volume ¹ (attach a stage-storage table)	≥ WQV
3,777 sf	A _{SA} = Surface area of the bottom of the pond	_
3.00 iph	Ksat _{DESIGN} = Design infiltration rate ²	
3.3 hours	I _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	< 72-hrs
135.00 feet	E _{BTM} = Elevation of the bottom of the basin	
- feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	oit)
- feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	t pit)
135.00 feet	D _{SHWT} = Separation from SHWT	≥* ³
135.0 feet	D _{ROCK} = Separation from bedrock	≥ * ³
N/A ft	D _{amend} = Depth of amended soil, if applicable due high infiltation rate	> 24"
N/A ft	D _T = Depth of trench, if trench proposed	4 - 10 ft
Yes Yes/No	If a trench or underground system is proposed, has observation well been provide	led? ←yes
N/A	If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements.	' ← yes
N/A Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
N/A :1	If a basin is proposed, pond side slopes.	≥3:1
136.78 ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
138.77 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
139.00 ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES	10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES	If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes

- 1. Volume below the lowest invert of the outlet structure and excludes forebay volume
- 2. Ksat_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
- 3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
- 4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
- 5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

Designer's Notes:	 		



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: Infiltration Trench #1

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

		-
Yes	Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.54 ac	A = Area draining to the practice	
0.07 ac	A _I = Impervious area draining to the practice	
0.13 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.16 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.09 ac-in	WQV= 1" x Rv x A	
323 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
81 cf	25% x WQV (check calc for sediment forebay volume)	
N/A	Method of pretreatment? (not required for clean or roof runoff)	
N/A cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
929 cf	V = Volume ¹ (attach a stage-storage table)	_ ≥ WQV
384 sf	A _{SA} = Surface area of the bottom of the pond	_
3.00 iph	Ksat _{DESiGN} = Design infiltration rate ²	
3.4 hours	I _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	< 72-hrs
138.00 feet	E _{BTM} = Elevation of the bottom of the basin	
- feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test	pit)
- feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the tes	t pit)
138.00 feet	D _{SHWT} = Separation from SHWT	≥ * ³
138.0 feet	D _{ROCK} = Separation from bedrock	≥ * ³
N/A ft	D _{amend} = Depth of amended soil, if applicable due high infiltation rate	> 24"
2.00 ft	D _T = Depth of trench, if trench proposed	4 - 10 ft
No Yes/No	If a trench or underground system is proposed, has observation well been provide	led? ←yes
Yes	If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements.	¹ ← yes
N/A Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
N/A :1	If a basin is proposed, pond side slopes.	≥3:1
140.10 ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
140.60 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
141.00 ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES	10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES	If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes
		

- 1. Volume below the lowest invert of the outlet structure and excludes forebay volume
- 2. Ksat_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
- 3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
- 4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
- 5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

Designer's Notes:				



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: Infiltration Trench #2

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

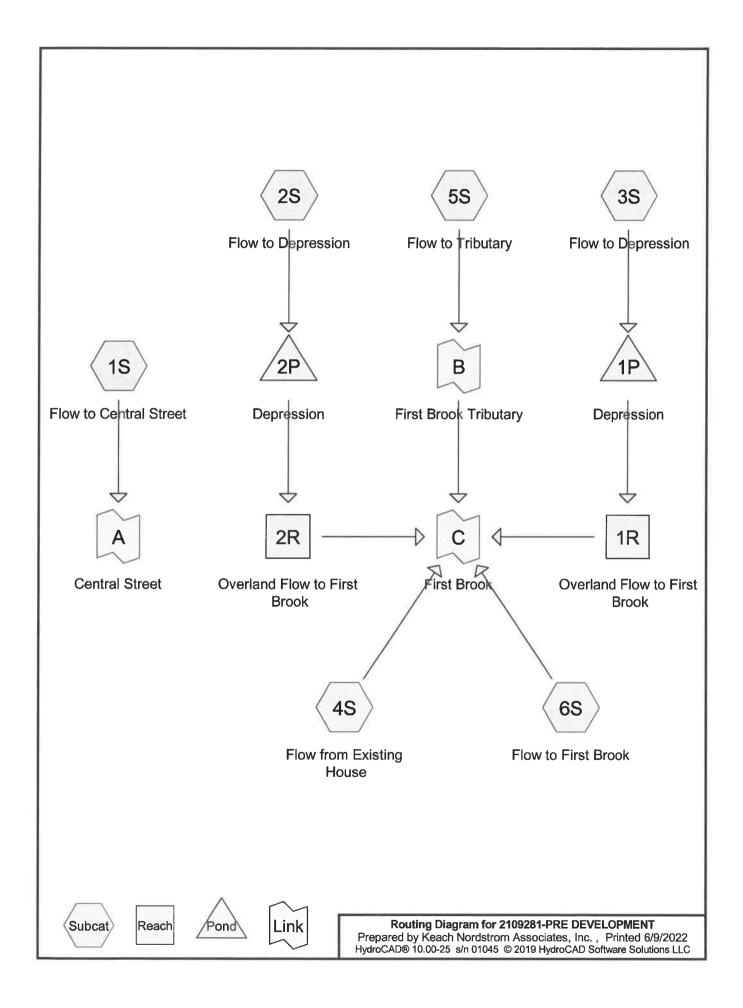
Yes	Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.39 ac	A = Area draining to the practice	-
0.02 ac	A _I = Impervious area draining to the practice	
0.06 decimal	I = Percent impervious area draining to the practice, in decimal form	
0.10 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.04 ac-in	WQV= 1" x Rv x A	
145 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
36 cf	25% x WQV (check calc for sediment forebay volume)	
N/A	Method of pretreatment? (not required for clean or roof runoff)	
N/A cf	V_{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
986 cf	V = Volume ¹ (attach a stage-storage table)	≥ WQV
333 sf	A _{SA} = Surface area of the bottom of the pond	
3.00 iph	Ksat _{DESIGN} = Design infiltration rate ²	
1.7 hours	$I_{DRAIN} = Drain time = V / (A_{SA} + I_{DESIGN})$	< 72-hrs
137.00 feet	E _{BTM} = Elevation of the bottom of the basin	
- feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
- feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
137.00 feet	D _{SHWT} = Separation from SHWT	≥ * ³
137.0 feet	D _{ROCK} = Separation from bedrock	≥ * ³
N/A ft	D _{amend} = Depth of amended soil, if applicable due high infiltation rate	≥ 24 "
2.00 ft	D _T = Depth of trench, if trench proposed	4 - 10 ft
No Yes/No	If a trench or underground system is proposed, has observation well been provid	ed? ←yes
Yes	If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements. 4	← yes
N/A Yes/No	If a basin is proposed, Is the perimeter curvilinear, and basin floor flat?	← yes
N/A :1	If a basin is proposed, pond side slopes.	<u>></u> 3:1
137.52 ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
138.91 ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
140.00 ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES	10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES	If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes

- 1. Volume below the lowest invert of the outlet structure and excludes forebay volume
- 2. Ksat_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
- 3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
- 4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
- 5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

Designer's Notes:		 		

HYDROCAD DRAINAGE ANALYSIS

- I. 2-YR, PRE-DEVELOPMENT
- II. 10-YR, PRE-DEVELOPMENT
- III. 25-YR, PRE-DEVELOPMENT
- IV. 50-YR, PRE-DEVELOPMENT
- V. 2-YR, POST-DEVELOPMENT
- VI. 10-YR, POST-DEVELOPMENT
- VII. 25-YR, POST-DEVELOPMENT
- VIII. 50-YR, POST-DEVELOPMENT
- IX. FROZEN GROUND CONDITIONS POND NODES



Page 2

Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method

Subcatchment 1S: Flow to Central Stree	Runoff Area=21,075 sf 15.46% Impervious Runoff Depth>0.49" Flow Length=125' Tc=13.9 min CN=WQ Runoff=0.20 cfs 0.02 af
Subcatchment 2S: Flow to Depression	Runoff Area=43,218 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=144' Tc=13.9 min CN=WQ Runoff=0.00 cfs 0.00 af
Subcatchment 3S: Flow to Depression	Runoff Area=37,017 sf 1.72% Impervious Runoff Depth>0.05" Flow Length=163' Tc=19.0 min CN=WQ Runoff=0.03 cfs 0.00 af
Subcatchment 4S: Flow from Existing	Runoff Area=84,645 sf 16.53% Impervious Runoff Depth>0.52" Flow Length=162' Tc=23.8 min CN=WQ Runoff=0.68 cfs 0.08 af
Subcatchment 5S: Flow to Tributary	Runoff Area=98,684 sf 4.88% Impervious Runoff Depth>0.13" Flow Length=747' Tc=19.9 min CN=WQ Runoff=0.22 cfs 0.02 af
Subcatchment 6S: Flow to First Brook	Runoff Area=73,668 sf 0.00% Impervious Runoff Depth>0.00" Flow Length=247' Tc=15.1 min CN=WQ Runoff=0.00 cfs 0.00 af
	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af =150.0' S=0.1520 '/' Capacity=282.79 cfs Outflow=0.00 cfs 0.00 af
	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af =170.0' S=0.1194 '/' Capacity=250.65 cfs Outflow=0.00 cfs 0.00 af
Pond 1P: Depression	Peak Elev=140.07' Storage=144 cf Inflow=0.03 cfs 0.00 af Outflow=0.00 cfs 0.00 af
Pond 2P: Depression	Peak Elev=135.00' Storage=0 cf Inflow=0.00 cfs 0.00 af Outflow=0.00 cfs 0.00 af
Link A: Central Street	Inflow=0.20 cfs 0.02 af Primary=0.20 cfs 0.02 af
Link B: First Brook Tributary	Inflow=0.22 cfs 0.02 af Primary=0.22 cfs 0.02 af
Link C: First Brook	Inflow=0.89 cfs 0.11 af Primary=0.89 cfs 0.11 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.13 af Average Runoff Depth = 0.19" 93.66% Pervious = 7.704 ac 6.34% Impervious = 0.521 ac

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Summary for Subcatchment 1S: Flow to Central Street

Runoff = 0.20 cfs @ 12.18 hrs, Volume=

0.02 af. Depth> 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

A	rea (sf)	CN	Description	n					
	1,998	98.0	Paved pa	Paved parking, HSG A					
	1,260	98.0	Roofs, HS	Roofs, HSG A					
	1,466	30.0	Woods, G	Good, HSG	A				
	15,781	39.0	>75% Gra	iss cover, (Good, HSG A				
	570	96.0	Gravel su	rface, HSG	6 A				
	21,075		Weighted	Weighted Average					
	17,817	40.1	84.54% P	84.54% Pervious Area					
	3,258	98.0	15.46% In	npervious A	Area				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
12.8	50	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.95"				
1.1	75	0.0285	1.18		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
13.9	125	Total							

Summary for Subcatchment 2S: Flow to Depression

Runoff = 0.00 cfs @ 0.00 hrs, Volume=

0.00 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	A	rea (sf)	CN	Description	n						
		22,970	30.0	0 Woods, Good, HSG A							
		20,248	39.0	>75% Gra	ass cover, (Good, HSG A					
		43,218		Weighted	Average						
		43,218	34.2	100.00%	Pervious A	rea					
	Тс	Length	Slope	Velocity	Capacity	Description					
<u></u>	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	12.8	50	0.0200	0.06		Sheet Flow,					
						Woods: Light underbrush n= 0.400 P2= 2.95"					
	1.0	94	0.0957	1.55		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	13.9	144	Total								

Summary for Subcatchment 3S: Flow to Depression

Runoff = 0.03 cfs @ 12.25 hrs, Volume= 0.00

0.00 af, Depth> 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	Α	rea (sf)	CN	Description	n					
		18,978	30.0	Woods, G	Woods, Good, HSG A					
		17,402	39.0	>75% Gra	ass cover, (Good, HSG A				
		637	98.0	Roofs, HS	SG A					
		37,017		Weighted	Weighted Average					
		36,380	34.3	98.28% P	ervious Are	ea				
		637	98.0	1.72% lm	pervious Ai	rea				
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	16.9	50	0.0100	0.05		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.95"				
	2.0	113	0.0354	0.94		Shallow Concentrated Flow,				
-						Woodland Kv= 5.0 fps				
_	19.0	163	Total			31				

Summary for Subcatchment 4S: Flow from Existing House

Runoff = 0.68 cfs @ 12.31 hrs, Volume=

0.08 af, Depth> 0.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

12	Α	rea (sf)	CN	Description	n	
		8,242	98.0	Paved pa	rking, HSG	A
		5,752	98.0	Roofs, HS	G A	
		28,838	30.0	Woods, G	lood, HSG	A
		39,430	39.0	>75% Gra	ss cover, (Good, HSG A
		2,383	96.0	Gravel su	rface, HSG	6 A
		84,645		Weighted	Average	
	70,651 37.2 83.47% Pervious A					ea
		13,994	98.0	16.53% lr	npervious A	Area
	Tc	Length	Slope	Velocity	Capacity	Description
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	22.4	50	0.0050	0.04		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	23.8	162	Total			

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Summary for Subcatchment 5S: Flow to Tributary

Runoff = 0.22 cfs @ 12.26 hrs, Volume=

0.02 af, Depth> 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	A	rea (sf)	CN	Description	on						
		1,636	98.0	Roofs, HS	Roofs, HSG A						
		46,962	30.0	Woods, G	Good, HSG	A					
		46,908	39.0	>75% Gra	ass cover, (Good, HSG A					
٠.		3,178	98.0	Paved pa	rking, HSG	A					
		98,684		Weighted	Average						
		93,870	34.5	95.12% P	ervious Are	ea					
		4,814	98.0	4.88% lm	4.88% Impervious Area						
	_				_						
	Tc	Length	Slope	Velocity	Capacity	Description					
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	16.9	50	0.0100	0.05		Sheet Flow,					
						Woods: Light underbrush n= 0.400 P2= 2.95"					
	0.9	72	0.0694	1.32		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,					
						Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'					
-						n= 0.025 Earth, clean & winding					
	19.9	747	Total								

Summary for Subcatchment 6S: Flow to First Brook

Runoff = 0.00 cfs @ 12.20 hrs, Volume= 0.00 af, Depth> 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

Area (sf)	CN	Description				
65,603	30.0	Woods, Good, HSG A				
7,986	39.0	>75% Grass cover, Good, HSG A				
79	96.0	Gravel surface, HSG A				
73,668		Weighted Average				
73,668	31.0	100.00% Pervious Area				

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.8	50	0.0200	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.95"
1.4	90	0.0444	1.05		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	57	0.0614	1.73		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.3	50	0.3200	2.83		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
15.1	2/7	Total			

15.1 247 Total

Summary for Reach 1R: Overland Flow to First Brook

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth = 0.00" for 2-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf, Capacity= 282.79 cfs

5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior

Side Slope Z-value= 3.0 '/' Top Width= 11.00'

Length= 150.0' Slope= 0.1520 '/'

Inlet Invert= 141.80', Outlet Invert= 119.00'



Summary for Reach 2R: Overland Flow to First Brook

Inflow Area = 0.992 ac, 0.00% Impervious, Inflow Depth = 0.00" for 2-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf, Capacity= 250.65 cfs

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5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior Side Slope Z-value= 3.0 '/' Top Width= 11.00' Length= 170.0' Slope= 0.1194 '/' Inlet Invert= 137.80', Outlet Invert= 117.50'



Summary for Pond 1P: Depression

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth > 0.05" for 2-YEAR event

Inflow = 0.03 cfs @ 12.25 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.07' @ 24.00 hrs Surf.Area= 2,060 sf Storage= 144 cf Flood Elev= 142.00' Surf.Area= 3,991 sf Storage= 5,980 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inv	ert Avail.Sto	orage Storage I	Description	
#1	140.	00' 5,9	80 cf Custom	Stage Data (Pri	ismatic) Listed below (Recalc)
Elevatio	01.5	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
140.0	00	1,989	0	0	
142.0	00	3,991	5,980	5,980	
Device	Routing	Invert	Outlet Devices	,	
#1	Primary	141.80'	Head (feet) 0. 2.50 3.00 3.5	20 0.40 0.60 (0) 2.54 2.61 2.6	0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=140.00' TW=141.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 2P: Depression

Inflow Area = 0.992 ac, 0.00% Impervious, Inflow Depth = 0.00" for 2-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 135.00' @ 0.00 hrs Surf.Area= 250 sf Storage= 0 cf Flood Elev= 139.00' Surf.Area= 6.715 sf Storage= 15.895 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no inflow)

Volume	Invert	Avail.Storage	Storage Description
#1	135.00'	15.895 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
135.00	250	0	0
136.00	2,787	1,519	1,519
138.00	5,488	8,275	9,794
139.00	6,715	6,102	15,895

Device Routing Invert Outlet Devices

#1 Primary 137.90' 5.0' long x 2.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

2.50 3.00 3.50

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88

2.85 3.07 3.20 3.32

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=137.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link A: Central Street

Inflow Area = 0.484 ac, 15.46% Impervious, Inflow Depth > 0.49" for 2-YEAR event

Inflow = 0.20 cfs @ 12.18 hrs, Volume= 0.02 af

Primary = 0.20 cfs @ 12.18 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 2.265 ac, 4.88% Impervious, Inflow Depth > 0.13" for 2-YEAR event

Inflow = 0.22 cfs @ 12.26 hrs, Volume= 0.02 af

Primary = 0.22 cfs @ 12.26 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 2-YEAR Rainfall=2.95"

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Summary for Link C: First Brook

Inflow Area = 7.742 ac, 5.77% Impervious, Inflow Depth > 0.17" for 2-YEAR event

Inflow = 0.89 cfs @ 12.30 hrs, Volume= 0.11 af

Primary = 0.89 cfs @ 12.30 hrs, Volume= 0.11 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method

	unoff Area=21,075 sf 15.46% Impervious Runoff Depth>0.83" Length=125' Tc=13.9 min CN=WQ Runoff=0.30 cfs 0.03 af
	Runoff Area=43,218 sf 0.00% Impervious Runoff Depth>0.05" Length=144' Tc=13.9 min CN=WQ Runoff=0.01 cfs 0.00 af
	Runoff Area=37,017 sf 1.72% Impervious Runoff Depth>0.12" Length=163' Tc=19.0 min CN=WQ Runoff=0.04 cfs 0.01 af
	unoff Area=84,645 sf 16.53% Impervious Runoff Depth>0.85" Length=162' Tc=23.8 min CN=WQ Runoff=1.03 cfs 0.14 af
	Runoff Area=98,684 sf 4.88% Impervious Runoff Depth>0.25" Length=747' Tc=19.9 min CN=WQ Runoff=0.33 cfs 0.05 af
	Runoff Area=73,668 sf 0.00% Impervious Runoff Depth>0.02" Length=247' Tc=15.1 min CN=WQ Runoff=0.01 cfs 0.00 af
Reach 1R: Overland Flow to First Brook Avg n=0.013 L=150.0	g. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af 'S=0.1520'/' Capacity=282.79 cfs Outflow=0.00 cfs 0.00 af
Reach 2R: Overland Flow to First Brook Avg n=0.013 L=170.0	g. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af 'S=0.1194 '/' Capacity=250.65 cfs Outflow=0.00 cfs 0.00 af
Pond 1P: Depression	Peak Elev=140.18' Storage=370 cf Inflow=0.04 cfs 0.01 af Outflow=0.00 cfs 0.00 af
Pond 2P: Depression	Peak Elev=135.28' Storage=172 cf Inflow=0.01 cfs 0.00 af Outflow=0.00 cfs 0.00 af
Link A: Central Street	Inflow=0.30 cfs 0.03 af Primary=0.30 cfs 0.03 af
Link B: First Brook Tributary	Inflow=0.33 cfs 0.05 af Primary=0.33 cfs 0.05 af
Link C: First Brook	Inflow=1.36 cfs 0.19 af Primary=1.36 cfs 0.19 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.23 af Average Runoff Depth = 0.34" 93.66% Pervious = 7.704 ac 6.34% Impervious = 0.521 ac HydroCAD® 10.00-25 s/n 01045 © 2019 HydroCAD Software Solutions LLC

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Summary for Subcatchment 1S: Flow to Central Street

Runoff = 0.30 cfs @ 12.18 hrs, Volume=

0.03 af, Depth> 0.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	Α	rea (sf)	CN	Description	n				
		1,998	98.0	Paved parking, HSG A					
		1,260	98.0	Roofs, HS	G A				
		1,466	30.0	Woods, G	ood, HSG	A			
		15,781	39.0	>75% Gra	iss cover, (Good, HSG A			
		570	96.0	Gravel su	rface, HSG	G A			
21,075 Weighted Average									
	17,817 40.1 84.54% Pervious				ervious Are	ea			
		3,258	98.0	15.46% In	npervious A	Area			
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	12.8	50	0.0200	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.95"			
	1.1	75	0.0285	1.18		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	13.9	125	Total						

Summary for Subcatchment 2S: Flow to Depression

Runoff = 0.01 cfs @ 14.90 hrs, Volume=

0.00 af, Depth> 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	A	rea (sf)	CN	Description	n				
		22,970	30.0	Woods, Good, HSG A					
		20,248	39.0	>75% Gra	ass cover, (Good, HSG A			
		43,218		Weighted	Average				
43,218 34.2 100.00% Pervious Area					Pervious A	rea			
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	12.8	50	0.0200	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.95"			
	1.0	94	0.0957	1.55		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	13.9	144	Total						

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Summary for Subcatchment 3S: Flow to Depression

Runoff = 0.04 cfs @ 12.25 hrs, Volume= 0.01 af, Depth> 0.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	A	rea (sf)	CN	Description	n					
-		18,978	30.0	Woods, G	Good, HSG	A				
		17,402	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
		637	98.0	Roofs, HS	SG A					
87.		37,017		Weighted	Average					
36,380 34.3 98.28% Pervious Area					_	ea				
		637	98.0	1.72% Im	pervious Ar	rea				
					•					
	Tc	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
	16.9	50	0.0100	0.05		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.95"				
	2.0	113	0.0354	0.94		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	19.0	163	Total							

Summary for Subcatchment 4S: Flow from Existing House

Runoff = 1.03 cfs @ 12.31 hrs, Volume= 0.14 af, Depth> 0.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	Α	rea (sf)	CN	Description	n	
		8,242	98.0	Paved par	rking, HSG	A
		5,752	98.0	Roofs, HS		
		28,838	30.0	Woods, G	ood, HSG	A
		39,430	39.0	>75% Gra	ss cover, (Good, HSG A
		2,383	96.0	Gravel su	rface, HSG	i A
		84,645		Weighted	Average	
70,651 37.2 83.47% Pervious Area					ea	
		13,994	98.0	16.53% In	npervious A	Area .
	Тс	Length	Slope		Capacity	Description
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	22.4	50	0.0050	0.04		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,
- 1						Woodland Kv= 5.0 fps
	23.8	162	Total			

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Summary for Subcatchment 5S: Flow to Tributary

Runoff = 0.33 cfs @ 12.26 hrs, Volume=

0.05 af, Depth> 0.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	Α	rea (sf)	CN	Description	n				
		1,636	98.0	Roofs, HSG A					
		46,962	30.0	Woods, G	Good, HSG	A			
		46,908	39.0	>75% Gra	ass cover, (Good, HSG A			
		3,178	98.0	Paved pa	rking, HSG	A			
		98,684		Weighted	Average				
		93,870	34.5	95.12% P	ervious Are	ea			
		4,814	98.0	4.88% lm	pervious Ai	rea			
	_				_				
	Тс	Length	Slope	Velocity	Capacity	Description			
2	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	16.9	50	0.0100	0.05		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.95"			
	0.9	72	0.0694	1.32		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,			
						Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'			
_						n= 0.025 Earth, clean & winding			
	19.9	747	Total						

Summary for Subcatchment 6S: Flow to First Brook

Runoff = 0.01 cfs @ 12.20 hrs, Volume=

0.00 af, Depth> 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

 Area (sf)	CN	Description
65,603	30.0	Woods, Good, HSG A
7,986	39.0	>75% Grass cover, Good, HSG A
 79	96.0	Gravel surface, HSG A
73,668		Weighted Average
73,668	31.0	100.00% Pervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	12.8	50	0.0200	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.4	90	0.0444	1.05		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.5	57	0.0614	1.73		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.3	50	0.3200	2.83		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	15.1	247	Total			

Summary for Reach 1R: Overland Flow to First Brook

0.850 ac. 1.72% Impervious, Inflow Depth = 0.00" for 10-YEAR event Inflow Area =

Inflow 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

0.00 hrs, Volume= Outflow 0.00 cfs @ 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps. Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf, Capacity= 282.79 cfs

5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior

Side Slope Z-value= 3.0 '/' Top Width= 11.00'

Length= 150.0' Slope= 0.1520 '/'

Inlet Invert= 141.80', Outlet Invert= 119.00'



Summary for Reach 2R: Overland Flow to First Brook

0.992 ac, 0.00% Impervious, Inflow Depth = 0.00" for 10-YEAR event Inflow Area =

Inflow 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps. Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf. Capacity= 250.65 cfs

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5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior Side Slope Z-value= 3.0 '/' Top Width= 11.00' Length= 170.0' Slope= 0.1194 '/' Inlet Invert= 137.80', Outlet Invert= 117.50'



Summary for Pond 1P: Depression

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth > 0.12" for 10-YEAR event

Inflow 0.04 cfs @ 12.25 hrs, Volume= 0.01 af

0.00 hrs, Volume= 0.00 hrs, Volume= Outflow = 0.00 cfs @ 0.00 af, Atten= 100%, Lag= 0.0 min

Primary 0.00 cfs @ 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.18' @ 24.00 hrs Surf.Area= 2,167 sf Storage= 370 cf

Flood Elev= 142.00' Surf.Area= 3,991 sf Storage= 5,980 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inv	<u>ert Avail.Sto</u>	orage Storage	Description	
#1	140.	00' 5,9	80 cf Custom	Stage Data (Pri	ismatic) Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
140.0	00	1,989	0	0	
142.0	00	3,991	5,980	5,980	
Device	Routing	Invert	Outlet Device	s	
#1	Primary	141.80'	Head (feet) 0 2.50 3.00 3.5	0.20 0.40 0.60 (50 n) 2.54 2.61 2.6	0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=140.00' TW=141.80' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 2P: Depression

Inflow Area = 0.992 ac, 0.00% Impervious, Inflow Depth > 0.05" for 10-YEAR event

Inflow = 0.01 cfs @ 14.90 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 135.28' @ 24.00 hrs Surf.Area= 966 sf Storage= 172 cf

Flood Elev= 139.00' Surf.Area= 6,715 sf Storage= 15,895 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Taxaada Oodlad Daadaaa

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	135.00'	15,895 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
135.00	250	0	0
136.00	2,787	1,519	1,519
138.00	5,488	8,275	9,794
139.00	6,715	6,102	15,895
	(feet) 135.00 136.00 138.00	(feet) (sq-ft) 135.00 250 136.00 2,787 138.00 5,488	(feet) (sq-ft) (cubic-feet) 135.00 250 0 136.00 2,787 1,519 138.00 5,488 8,275

Device	Routing	Invert	Outlet Devices
#1	Primary	137.90'	5.0' long x 2.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50
			Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=137.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link A: Central Street

Inflow Area = 0.484 ac, 15.46% Impervious, Inflow Depth > 0.83" for 10-YEAR event

Inflow = 0.30 cfs @ 12.18 hrs, Volume= 0.03 af

Primary = 0.30 cfs @ 12.18 hrs, Volume= 0.03 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 2.265 ac, 4.88% Impervious, Inflow Depth > 0.25" for 10-YEAR event

Inflow = 0.33 cfs @ 12.26 hrs, Volume= 0.05 af

Primary = 0.33 cfs @ 12.26 hrs, Volume= 0.05 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 10-YEAR Rainfall=4.45"

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Summary for Link C: First Brook

7.742 ac, 5.77% Impervious, Inflow Depth > 0.29" for 10-YEAR event 1.36 cfs @ 12.29 hrs, Volume= 0.19 af Inflow Area =

Inflow

Primary 1.36 cfs @ 12.29 hrs, Volume= 0.19 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method

	unoff Area=21,075 sf 15.46% Impervious Runoff Depth>1.23" Length=125' Tc=13.9 min CN=WQ Runoff=0.38 cfs 0.05 af
	Runoff Area=43,218 sf 0.00% Impervious Runoff Depth>0.18" Length=144' Tc=13.9 min CN=WQ Runoff=0.05 cfs 0.01 af
	Runoff Area=37,017 sf 1.72% Impervious Runoff Depth>0.27" Length=163' Tc=19.0 min CN=WQ Runoff=0.07 cfs 0.02 af
Subcatchment 4S: Flow from Existing Flow	unoff Area=84,645 sf 16.53% Impervious Runoff Depth>1.20" Length=162' Tc=23.8 min CN=WQ Runoff=1.33 cfs 0.19 af
	Runoff Area=98,684 sf 4.88% Impervious Runoff Depth>0.44" Length=747' Tc=19.9 min CN=WQ Runoff=0.43 cfs 0.08 af
	Runoff Area=73,668 sf 0.00% Impervious Runoff Depth>0.07" Length=247' Tc=15.1 min CN=WQ Runoff=0.02 cfs 0.01 af
	g. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af 0' S=0.1520 '/' Capacity=282.79 cfs Outflow=0.00 cfs 0.00 af
	g. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af 0' S=0.1194 '/' Capacity=250.65 cfs Outflow=0.00 cfs 0.00 af
Pond 1P: Depression	Peak Elev=140.38' Storage=834 cf Inflow=0.07 cfs 0.02 af Outflow=0.00 cfs 0.00 af
Pond 2P: Depression	Peak Elev=135.62' Storage=643 cf Inflow=0.05 cfs 0.01 af Outflow=0.00 cfs 0.00 af
Link A: Central Street	Inflow=0.38 cfs 0.05 af Primary=0.38 cfs 0.05 af
Link B: First Brook Tributary	Inflow=0.43 cfs 0.08 af Primary=0.43 cfs 0.08 af
Link C: First Brook	Inflow=1.77 cfs 0.29 af Primary=1.77 cfs 0.29 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.37 af Average Runoff Depth = 0.54" 93.66% Pervious = 7.704 ac 6.34% Impervious = 0.521 ac

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Summary for Subcatchment 1S: Flow to Central Street

Runoff =

0.38 cfs @ 12.19 hrs, Volume=

0.05 af, Depth> 1.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	A	rea (sf)	CN	Description	n		
		1,998	98.0	Paved pa	rking, HSG	A	
		1,260	98.0	Roofs, HS	SG A		
		1,466	30.0	Woods, G	Good, HSG	A	
		15,781	39.0	>75% Gra	>75% Grass cover, Good, HSG A		
		570	96.0	Gravel su	rface, HSG	6 A	
_	21,075			Weighted	Average		
		17,817	40.1	84.54% P	ervious Are	ea	
		3,258	98.0	15.46% In	npervious A	Area	
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	12.8	50	0.0200	0.06		Sheet Flow,	
						Woods: Light underbrush n= 0.400 P2= 2.95"	
	1.1	75	0.0285	1.18		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
-	13.9	125	Total				

Summary for Subcatchment 2S: Flow to Depression

Runoff =

0.05 cfs @ 12.51 hrs, Volume=

0.01 af, Depth> 0.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	A	rea (sf)	CN	Description	n	
22,970 30.0 Woods, Good, HSG			Woods, G	ood, HSG	A	
		20,248	39.0	>75% Gra	iss cover, (Good, HSG A
43,218 Weighted Average			Weighted	Average		
		43,218	34.2	100.00%	Pervious A	rea
	_					—
	Tc	Length	Slope		Capacity	Description
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	12.8	50	0.0200	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.0	94	0.0957	1.55		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	13.9	144	Total			

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Summary for Subcatchment 3S: Flow to Depression

Runoff

=

0.07 cfs @ 12.47 hrs, Volume=

0.02 af, Depth> 0.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	A	rea (sf)	CN	Description	n		
		18,978	30.0	Woods, G	lood, HSG	A	
		17,402	39.0	>75% Gra	iss cover, (Good, HSG A	
		637	98.0	Roofs, HSG A			
-		37,017		Weighted	Weighted Average		
		36,380	34.3	98.28% P	ervious Are	ea	
		637	98.0	1.72% lm	pervious Ai	rea	
	Tc	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	16.9	50	0.0100	0.05		Sheet Flow,	
						Woods: Light underbrush n= 0.400 P2= 2.95"	
	2.0	113	0.0354	0.94		Shallow Concentrated Flow,	
						Woodland Kv= 5.0 fps	
	19.0	163	Total				

Summary for Subcatchment 4S: Flow from Existing House

Runoff

=

1.33 cfs @ 12.32 hrs, Volume=

0.19 af, Depth> 1.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

-	Α	rea (sf)	CN	Description	n			
		8,242	98.0	Paved par	rking, HSG	A		
		5,752	98.0	Roofs, HS	G A			
		28,838	30.0	Woods, Good, HSG A				
		39,430	39.0	>75% Gra	>75% Grass cover, Good, HSG A			
		2,383	96.0	Gravel su	rface, HSG	6 A		
		84,645		Weighted	Average			
		70,651	37.2	83.47% P	ervious Are	ea		
		13,994	98.0	16.53% In	npervious A	Area		
	Tc	Length	Slope	Velocity	Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	22.4	50	0.0050	0.04		Sheet Flow,		
						Woods: Light underbrush n= 0.400 P2= 2.95"		
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,		
			_			Woodland Kv= 5.0 fps		
-	23.8	162	Total					

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Summary for Subcatchment 5S: Flow to Tributary

Runoff = 0.43 cfs @ 12.28 hrs, Volume= 0.08 af, Depth> 0.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	Α	rea (sf)	CN	Description	n	
		1,636	98.0	Roofs, HS	SG A	
		46,962	30.0	Woods, G	Good, HSG	A
		46,908	39.0	>75% Gra	ass cover, (Good, HSG A
		3,178	98.0	Paved pa	rking, HSG	Α
		98,684		Weighted	Average	
	93,870 34.5		34.5	95.12% P	ervious Are	ea
		4,814	98.0	4.88% lm	pervious Ai	rea
	Tc	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	16.9	50	0.0100	0.05		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	0.9	72	0.0694	1.32		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,
						Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'
_						n= 0.025 Earth, clean & winding
	19.9	747	Total			

Summary for Subcatchment 6S: Flow to First Brook

Runoff = 0.02 cfs @ 12.50 hrs, Volume= 0.01 af, Depth> 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	Area (sf)	CN	Description	
65,603 30.0 Wood			Woods, Good, HSG A	
7,986 39.0			>75% Grass cover, Good, HSG A	
	79	96.0	Gravel surface, HSG A	
73,668			Weighted Average	
			100.00% Pervious Area	

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
12.8	50	0.0200	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.95"
1.4	90	0.0444	1.05		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
0.5	57	0.0614	1.73		Shallow Concentrated Flow,
					Short Grass Pasture Kv= 7.0 fps
0.3	50	0.3200	2.83		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
15.1	2/17	Total			

15.1 247 Total

Summary for Reach 1R: Overland Flow to First Brook

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth = 0.00" for 25-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf, Capacity= 282.79 cfs

5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior

Side Slope Z-value= 3.0 '/' Top Width= 11.00'

Length= 150.0' Slope= 0.1520 '/'

Inlet Invert= 141.80', Outlet Invert= 119.00'



Summary for Reach 2R: Overland Flow to First Brook

Inflow Area = 0.992 ac. 0.00% Impervious, Inflow Depth = 0.00" for 25-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min

Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf. Capacity= 250.65 cfs

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5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior Side Slope Z-value= 3.0 '/' Top Width= 11.00' Length= 170.0' Slope= 0.1194 '/' Inlet Invert= 137.80', Outlet Invert= 117.50'



Summary for Pond 1P: Depression

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth > 0.27" for 25-YEAR event

Inflow = 0.07 cfs @ 12.47 hrs, Volume= 0.02 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.38' @ 24.00 hrs Surf.Area= 2,372 sf Storage= 834 cf

Flood Elev= 142.00' Surf.Area= 3,991 sf Storage= 5,980 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Avail Storage Storage Description

Center-of-Mass det. time= (not calculated: no outflow)

Invert

Volume

volume	IIIV	ert Avaii.Sit	nage Storage i	Jescription	
#1	140.	00' 5,9	80 cf Custom	Stage Data (Pr	ismatic) Listed below (Recalc)
Elevatio (fee	t)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
140.0 142.0		1,989 3,991	0 5,980	5,980	
Device	Routing	Invert	Outlet Devices	.	
#1	Primary	141.80'	Head (feet) 0. 2.50 3.00 3.5	20 0.40 0.60 (0) 2.54 2.61 2.(Pad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=140.00' TW=141.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 2P: Depression

Inflow Area = 0.992 ac, 0.00% Impervious, Inflow Depth > 0.18" for 25-YEAR event

Inflow = 0.05 cfs @ 12.51 hrs, Volume= 0.01 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 135.62' @ 24.00 hrs Surf.Area= 1,824 sf Storage= 643 cf

Flood Elev= 139.00' Surf.Area= 6,715 sf Storage= 15,895 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description	_	
#1	135.00'	15,895 cf	Custom Stage Data (Prismatic) Listed below (Recalc)		
Flevation	Surf A	rea Inc	oc Store Cum Store		

Elevation	Suri.Area	inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
135.00	250	0	0
136.00	2,787	1,519	1,519
138.00	5,488	8,275	9,794
139.00	6,715	6,102	15,895

Device	Routing	Invert	Outlet Devices
#1	Primary 137.90'		5.0' long x 2.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50
			Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88
			2.85 3.07 3.20 3.32

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=137.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link A: Central Street

Inflow Area = 0.484 ac, 15.46% Impervious, Inflow Depth > 1.23" for 25-YEAR event

Inflow = 0.38 cfs @ 12.19 hrs. Volume= 0.05 af

Primary = 0.38 cfs @ 12.19 hrs, Volume= 0.05 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 2.265 ac, 4.88% Impervious, Inflow Depth > 0.44" for 25-YEAR event

Inflow = 0.43 cfs @ 12.28 hrs, Volume= 0.08 af

Primary = 0.43 cfs @ 12.28 hrs, Volume= 0.08 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Link C: First Brook

7.742 ac, 5.77% Impervious, Inflow Depth > 0.45" for 25-YEAR event 1.77 cfs @ 12.31 hrs, Volume= 0.29 af Inflow Area =

Inflow

Primary 1.77 cfs @ 12.31 hrs, Volume= 0.29 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points Runoff by SCS TR-20 method, UH=SCS, Weighted-Q Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Flow to Central Stree	t Runoff Area=21,075 sf 15.46% Impervious Runoff Depth>1.68" Flow Length=125' Tc=13.9 min CN=WQ Runoff=0.52 cfs 0.07 af
Subcatchment 2S: Flow to Depression	Runoff Area=43,218 sf 0.00% Impervious Runoff Depth>0.40" Flow Length=144' Tc=13.9 min CN=WQ Runoff=0.14 cfs 0.03 af
Subcatchment 3S: Flow to Depression	Runoff Area=37,017 sf 1.72% Impervious Runoff Depth>0.51" Flow Length=163' Tc=19.0 min CN=WQ Runoff=0.16 cfs 0.04 af
Subcatchment 4S: Flow from Existing	Runoff Area=84,645 sf 16.53% Impervious Runoff Depth>1.61" Flow Length=162' Tc=23.8 min CN=WQ Runoff=1.72 cfs 0.26 af
Subcatchment 5S: Flow to Tributary	Runoff Area=98,684 sf 4.88% Impervious Runoff Depth>0.71" Flow Length=747' Tc=19.9 min CN=WQ Runoff=0.71 cfs 0.13 af
Subcatchment 6S: Flow to First Brook	Runoff Area=73,668 sf 0.00% Impervious Runoff Depth>0.23" Flow Length=247' Tc=15.1 min CN=WQ Runoff=0.06 cfs 0.03 af
	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af =150.0' S=0.1520 '/' Capacity=282.79 cfs Outflow=0.00 cfs 0.00 af
	Avg. Flow Depth=0.00' Max Vel=0.00 fps Inflow=0.00 cfs 0.00 af =170.0' S=0.1194 '/' Capacity=250.65 cfs Outflow=0.00 cfs 0.00 af
Pond 1P: Depression	Peak Elev=140.67' Storage=1,566 cf Inflow=0.16 cfs 0.04 af Outflow=0.00 cfs 0.00 af
Pond 2P: Depression	Peak Elev=135.97' Storage=1,439 cf Inflow=0.14 cfs 0.03 af Outflow=0.00 cfs 0.00 af
Link A: Central Street	Inflow=0.52 cfs 0.07 af Primary=0.52 cfs 0.07 af
Link B: First Brook Tributary	Inflow=0.71 cfs 0.13 af Primary=0.71 cfs 0.13 af
Link C: First Brook	Inflow=2.49 cfs 0.43 af Primary=2.49 cfs 0.43 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.56 af Average Runoff Depth = 0.82" 93.66% Pervious = 7.704 ac 6.34% Impervious = 0.521 ac

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Summary for Subcatchment 1S: Flow to Central Street

Runoff =

0.52 cfs @ 12.20 hrs, Volume=

0.07 af, Depth> 1.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

		rea (sf)	CN	Description	nn	
		1,998	98.0	Paved pa	A	
		1,260	98.0	Roofs, HS		
		1,466	30.0	Woods, G	Α	
		15,781	39.0	>75% Gra	Good, HSG A	
-		570	96.0	Gravel su	rface, HSG	B A
		21,075		Weighted	Average	
		17,817	40.1	84.54% P	ervious Are	ea
		3,258	98.0	15.46% In	npervious A	Area
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	12.8	50	0.0200	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.1	75	0.0285	1.18		Shallow Concentrated Flow,
2						Short Grass Pasture Kv= 7.0 fps
	13.9	125	Total			

Summary for Subcatchment 2S: Flow to Depression

Runoff =

0.14 cfs @ 12.40 hrs, Volume=

0.03 af, Depth> 0.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

100	Α	rea (sf)	CN	Description	n				
22,970 30.0 Woods, Good, HSG A						A			
02		20,248	39.0	>75% Grass cover, Good, HSG A					
43,218 Weighted Average									
43,218 34.2			34.2	100.00%	Pervious A	rea			
	Τ.	1 11.	01	N J - 1 20	0 11	Describette			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	12.8	50	0.0200	0.06	(0.0)	Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.95"			
	1.0	94	0.0957	1.55		Shallow Concentrated Flow,			
2						Woodland Kv= 5.0 fps			
	13.9	144	Total						

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Summary for Subcatchment 3S: Flow to Depression

Runoff = 0.16 cfs @ 12.39 hrs, Volume= 0.04 af, Depth> 0.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

Α	rea (sf)	CN	Description	n				
	18,978	30.0	Woods, G	Woods, Good, HSG A				
	17,402	39.0	>75% Gra	>75% Grass cover, Good, HSG A				
	637	98.0	Roofs, HS	SG A				
	37,017		Weighted	Weighted Average				
	36,380	34.3	98.28% P	ervious Are	ea			
	637	98.0	1.72% lm	pervious Ar	rea			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
16.9	50	0.0100	0.05		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.95"			
2.0	113	0.0354	0.94		Shallow Concentrated Flow,			
					Woodland Kv= 5.0 fps			
19.0	163	Total						

Summary for Subcatchment 4S: Flow from Existing House

Runoff = 1.72 cfs @ 12.33 hrs, Volume= 0.26 af, Depth> 1.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

ΑΑ	rea (sf)	CN	Description	n			
	8,242	98.0	Paved parking, HSG A				
	5,752	98.0	Roofs, HSG A				
	28,838	30.0	Woods, Good, HSG A				
	39,430	39.0	>75% Gra	iss cover, (Good, HSG A		
	2,383	96.0	Gravel su	rface, HSG	A		
	84,645		Weighted	Average			
	70,651	37.2	83.47% P	83.47% Pervious Area			
	13,994	98.0	16.53% Impervious Area				
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
22.4	50	0.0050	0.04		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.95"		
1.4	112	0.0714	1.34		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
23.8	162	Total					

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Summary for Subcatchment 5S: Flow to Tributary

Runoff = 0.71 cfs @ 12.33 hrs, Volume=

0.13 af, Depth> 0.71"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

A	rea (sf)	CN	Description	n			
	1,636	98.0	Roofs, HS	Roofs, HSG A			
	46,962	30.0	Woods, G	Good, HSG	A		
	46,908	39.0	>75% Gra	ass cover, (Good, HSG A		
19	3,178	98.0	Paved pa	rking, HSG	Α		
	98,684		Weighted	Average			
	93,870	34.5	95.12% P	ervious Are	ea		
	4,814	98.0	4.88% Im	pervious A	rea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)			
16.9	50	0.0100	0.05		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.95"		
0.9	72	0.0694	1.32		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,		
					Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'		
					n= 0.025 Earth, clean & winding		
19.9	747	Total					

Summary for Subcatchment 6S: Flow to First Brook

Runoff = 0.06 cfs @ 12.40 hrs, Volume=

0.03 af, Depth> 0.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

Area (sf)	CN	Description
65,603	30.0	Woods, Good, HSG A
7,986	39.0	>75% Grass cover, Good, HSG A
79	96.0	Gravel surface, HSG A
73,668		Weighted Average
73,668	31.0	100.00% Pervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	12.8	50	0.0200	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.95"
	1.4	90	0.0444	1.05		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
	0.5	57	0.0614	1.73		Shallow Concentrated Flow,
						Short Grass Pasture Kv= 7.0 fps
	0.3	50	0.3200	2.83		Shallow Concentrated Flow,
						Woodland Kv= 5.0 fps
_	15.1	247	Total			

Summary for Reach 1R: Overland Flow to First Brook

Inflow Area = 0.850 ac, 1.72% Impervious, Inflow Depth = 0.00" for 50-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf. Capacity= 282.79 cfs

5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior

Side Slope Z-value= 3.0 '/' Top Width= 11.00'

Length= 150.0' Slope= 0.1520 '/'

Inlet Invert= 141.80', Outlet Invert= 119.00'



Summary for Reach 2R: Overland Flow to First Brook

Inflow Area = 0.992 ac, 0.00% Impervious, Inflow Depth = 0.00" for 50-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Max. Velocity= 0.00 fps, Min. Travel Time= 0.0 min Avg. Velocity = 0.00 fps, Avg. Travel Time= 0.0 min

Peak Storage= 0 cf @ 0.00 hrs

Average Depth at Peak Storage= 0.00'

Bank-Full Depth= 1.00' Flow Area= 8.0 sf, Capacity= 250.65 cfs

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5.00' x 1.00' deep channel, n= 0.013 Corrugated PE, smooth interior Side Slope Z-value= 3.0 '/' Top Width= 11.00'

Length= 170.0' Slope= 0.1194 '/'

Inlet Invert= 137.80', Outlet Invert= 117.50'



Summary for Pond 1P: Depression

Inflow Area = 0.850 ac. 1.72% Impervious, Inflow Depth > 0.51" for 50-YEAR event

Inflow 0.16 cfs @ 12.39 hrs, Volume= 0.04 af

0.00 hrs, Volume= Outflow 0.00 af, Atten= 100%, Lag= 0.0 min = 0.00 cfs @

0.00 cfs @ 0.00 hrs, Volume= 0.00 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.67' @ 24.00 hrs Surf.Area= 2,663 sf Storage= 1,566 cf

Flood Elev= 142.00' Surf.Area= 3,991 sf Storage= 5,980 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Inv	ert Avail.Sto	orage Storage	Description	
#1	140.	00' 5,9	80 cf Custom	Stage Data (Pri	smatic) Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
140.0	0	1,989	0	0	
142.0	00	3,991	5,980	5,980	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	141.80'	Head (feet) (2.50 3.00 3.	0.20 0.40 0.60 (50 h) 2.54 2.61 2.6	ad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 1.80 2.00 61 2.60 2.66 2.70 2.77 2.89 2.88

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=140.00' TW=141.80' (Dynamic Tailwater) -1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Device Routing

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Summary for Pond 2P: Depression

Inflow Area = 0.00% Impervious, Inflow Depth > 0.40" for 50-YEAR event 0.992 ac.

0.14 cfs @ 12.40 hrs, Volume= 0.03 af Inflow

0.00 hrs, Volume= Outflow = 0.00 cfs @ 0.00 af, Atten= 100%, Lag= 0.0 min

0.00 cfs @ 0.00 hrs, Volume= 0.00 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 135.97' @ 24.00 hrs Surf.Area= 2,714 sf Storage= 1,439 cf

Flood Elev= 139.00' Surf.Area= 6,715 sf Storage= 15,895 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Invert Outlet Devices

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	135.00'	15,895 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
135.00	250	0	0
136.00	2,787	1,519	1,519
138.00	5,488	8,275	9,794
139.00	6,715	6,102	15,895

DCVIOC	rtouting	IIIIVOIT	Cattot Borioco
#1	Primary	137.90'	5.0' long x 2.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=137.80' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link A: Central Street

0.484 ac, 15.46% Impervious, Inflow Depth > 1.68" for 50-YEAR event Inflow Area =

Inflow 0.52 cfs @ 12.20 hrs, Volume= 0.07 af

0.52 cfs @ 12.20 hrs, Volume= 0.07 af. Atten= 0%, Lag= 0.0 min Primary

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

2.265 ac. 4.88% Impervious, Inflow Depth > 0.71" for 50-YEAR event Inflow Area =

Inflow 0.71 cfs @ 12.33 hrs, Volume= 0.13 af

0.13 af, Atten= 0%, Lag= 0.0 min Primary 0.71 cfs @ 12.33 hrs, Volume=

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 50-YEAR Rainfall=6.72"

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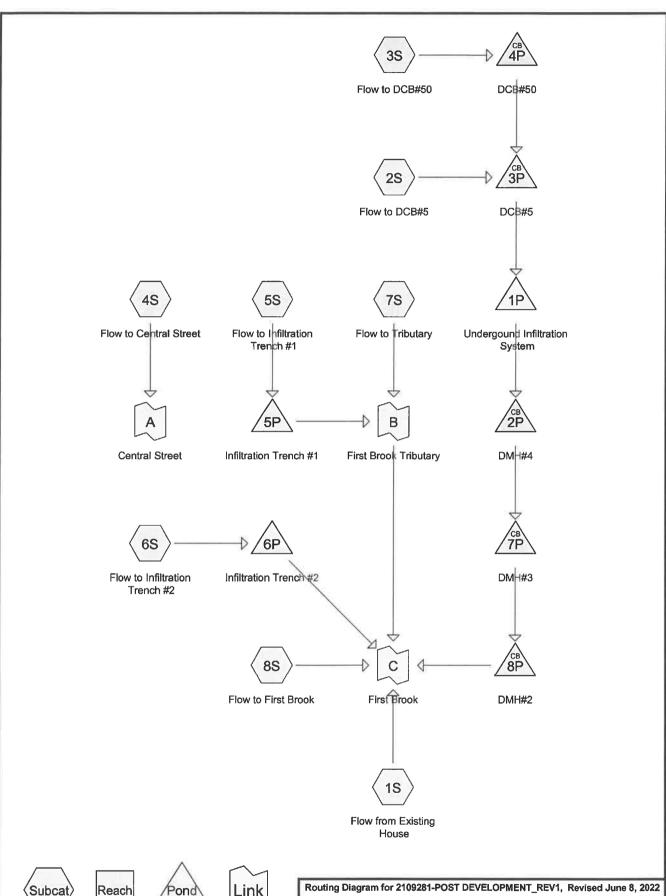
Summary for Link C: First Brook

Inflow Area = 7.742 ac, 5.77% Impervious, Inflow Depth > 0.66" for 50-YEAR event

Inflow = 2.49 cfs @ 12.33 hrs, Volume= 0.43 af

Primary = 2.49 cfs @ 12.33 hrs, Volume= 0.43 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs











Type III 24-hr 2-YEAR Rainfall=2.95"

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ns LLC Page 2

Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Reach routing by Dyn-Stor-	Ind method - Pond routing by Dyn-Stor-Ind method
Subcatchment 1S: Flow from Existing	Runoff Area=86,036 sf 16.27% Impervious Runoff Depth>0.51" Flow Length=162' Tc=24.2 min CN=WQ Runoff=0.67 cfs 0.08 af
Subcatchment 2S: Flow to DCB#5	Runoff Area=75,925 sf 24.53% Impervious Runoff Depth>0.67" Tc=6.0 min CN=WQ Runoff=1.21 cfs 0.10 af
Subcatchment 3S: Flow to DCB#50	Runoff Area=43,243 sf 36.54% Impervious Runoff Depth>0.99" Tc=6.0 min CN=WQ Runoff=1.03 cfs 0.08 af
Subcatchment 4S: Flow to Central Street	et Runoff Area=15,941 sf 20.44% Impervious Runoff Depth>0.64" Flow Length=125' Tc=13.7 min CN=WQ Runoff=0.20 cfs 0.02 af
Subcatchment 5S: Flow to Infiltration	Runoff Area=23,530 sf 12.75% Impervious Runoff Depth>0.35" Flow Length=269' Tc=16.8 min CN=WQ Runoff=0.14 cfs 0.02 af
Subcatchment 6S: Flow to Infiltration	Runoff Area=16,816 sf 5.95% Impervious Runoff Depth>0.16" Tc=6.0 min CN=WQ Runoff=0.07 cfs 0.01 af
Subcatchment 7S: Flow to Tributary	Runoff Area=58,458 sf 8.23% Impervious Runoff Depth>0.22" Flow Length=747' Tc=20.2 min CN=WQ Runoff=0.21 cfs 0.02 af
Subcatchment 8S: Flow to First Brook	Runoff Area=38,360 sf 0.00% Impervious Runoff Depth>0.01" Flow Length=200' Tc=14.3 min CN=WQ Runoff=0.00 cfs 0.00 af
Pond 1P: Undergound Infiltration Syste Discarded=	Peak Elev=136.05' Storage=2,415 cf Inflow=2.24 cfs 0.18 af 0.26 cfs 0.18 af Primary=0.00 cfs 0.00 af Outflow=0.26 cfs 0.18 af
Pond 2P: DMH#4 12.0" Roo	Peak Elev=133.82' Inflow=0.00 cfs 0.00 af und Culvert n=0.013 L=198.7' S=0.0100 '/' Outflow=0.00 cfs 0.00 af
Pond 3P: DCB#5	Peak Elev=137.06' Inflow=2.24 cfs 0.18 af und Culvert n=0.013 L=119.6' S=0.0050 '/' Outflow=2.24 cfs 0.18 af
Pond 4P: DCB#50	Peak Elev=137.35' Inflow=1.03 cfs 0.08 af ound Culvert n=0.013 L=22.0' S=0.0200 '/' Outflow=1.03 cfs 0.08 af
Pond 5P: Infiltration Trench #1 Discarded=	Peak Elev=139.25' Storage=192 cf Inflow=0.14 cfs 0.02 af e0.03 cfs 0.02 af Primary=0.00 cfs 0.00 af Outflow=0.03 cfs 0.02 af
Pond 6P: Infiltration Trench #2 Discarded=	Peak Elev=137.21' Storage=28 cf Inflow=0.07 cfs 0.01 af -0.02 cfs 0.01 af Primary=0.00 cfs 0.00 af Outflow=0.02 cfs 0.01 af
D 1 7D - DAI 1490	Dook Flour-197 701 Inflour-9 00 efc 0 00 ef

Pond 7P: DMH#3 Peak Elev=127.70' Inflow=0.00 cfs 0.00 af 12.0" Round Culvert n=0.013 L=15.0' S=0.0800 '/' Outflow=0.00 cfs 0.00 af

Pond 8P: DMH#2 Peak Elev=122.80' Inflow=0.00 cfs 0.00 af 12.0" Round Culvert n=0.013 L=10.0' S=0.0800 '/' Outflow=0.00 cfs 0.00 af

Type III 24-hr 2-YEAR Rainfall=2.95"

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Link A: Central Street Inflow=0.20 cfs 0.02 af

Primary=0.20 cfs 0.02 af

Link B: First Brook Tributary Inflow=0.21 cfs 0.02 af

Primary=0.21 cfs 0.02 af

Link C: First Brook Inflow=0.88 cfs 0.11 af

Primary=0.88 cfs 0.11 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.33 af Average Runoff Depth = 0.48" 83.12% Pervious = 6.837 ac 16.88% Impervious = 1.389 ac

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Summary for Subcatchment 1S: Flow from Existing House

Runoff = 0.67 cfs @ 12.32 hrs, Volume=

0.08 af, Depth> 0.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

ΑΑ	rea (sf)	CN	Descriptio	n					
	8,242	98.0	Paved par	Paved parking, HSG A					
	5,752	98.0	Roofs, HS	G A					
	28,793	30.0	Woods, G	ood, HSG	A				
	40,866	39.0	>75% Gra	iss cover, (Good, HSG A				
12	2,383	96.0	Gravel su	rface, HSG	5 A				
	86,036		Weighted	Average					
	72,042	37.3	83.73% Pervious Area						
	13,994	98.0	16.27% In	npervious A	Area				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
22.8	50	0.0050	0.04		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.84"				
1.4	112	0.0714	1.34		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
24.2	162	Total							

Summary for Subcatchment 2S: Flow to DCB#5

Runoff = 1.21 cfs @ 12.08 hrs, Volume=

0.10 af, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	Area (sf)	CN	Description						
	8,986	98.0	Paved parking, HSG A						
	56,071	39.0	75% Grass cover, Good, HSG A						
	637	98.0	Roofs, HSG A						
	1,231	30.0	Voods, Good, HSG A						
*	9,000	98.0	Lots, HSG A						
	75,925		Weighted Average						
	57,302	38.8	75.47% Pervious Area						
	18,623	98.0	24.53% Impervious Area						
(n	Tc Length	Slope (ft/ft)	Velocity Capacity Description (ft/sec) (cfs)						
	6.0		Direct Entry						

6.0

Direct Entry,

Type III 24-hr 2-YEAR Rainfall=2.95" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 3S: Flow to DCB#50

Runoff = 1.03 cfs @ 12.08 hrs, Volume= 0.08 af, Depth> 0.99"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

_	Α	rea (sf)	CN	Description							
-		27,440	39.0	>75% Gra	>75% Grass cover, Good, HSG A						
		10,803	98.0	Paved parking, HSG A							
*		5,000	98.0	Lots, HSC	Lots, HSG A						
-		43,243		Weighted Average							
		27,440	39.0	63.46% Pervious Area							
		15,803	98.0	36.54% Impervious Area							
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	6.0					Direct Entry.					

Summary for Subcatchment 4S: Flow to Central Street

Runoff = 0.20 cfs @ 12.18 hrs, Volume= 0.02 af, Depth> 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

A	rea (sf)	CN	Description	n					
	11,163	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
	1,260	98.0	Roofs, HS	SG A					
	1,998	98.0	Paved pa	rking, HSG	A				
	570	96.0	Gravel su	rface, HSG	G A				
y	950	30.0	Woods, G	ood, HSG	Α				
	15,941 Weighted Average			Average					
	12,683	40.9	79.56% P	ervious Are	ea				
	3,258	98.0	20.44% Ir	npervious A	Area				
_	_			_					
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
11.0	40	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.84"				
1.6	10	0.0200	0.10		Sheet Flow,				
					Grass: Short n= 0.150 P2= 2.84"				
1.1	75	0.0285	1.18		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
13.7	125	Total							

Type III 24-hr 2-YEAR Rainfall=2.95" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 5S: Flow to Infiltration Trench #1

Runoff = 0.14 cfs @ 12.22 hrs, Volume= 0.02 af, Depth> 0.35"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	Α	rea (sf)	CN	Description	n				
*		3,000	98.0	Lots, HSC	θA				
		14,196	39.0	>75% Gra	ass cover, (Good, HSG A			
_		6,334	30.0	Woods, G	Woods, Good, HSG A				
		23,530		Weighted Average					
		20,530	36.2	87.25% P	87.25% Pervious Area				
		3,000	98.0	12.75% Ir	npervious A	Area			
	Tc	Length	Slope	Velocity	1 (7)	Description			
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	13.1	50	0.0200	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.84"			
	3.1	185	0.0200	0.99		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	0.0	12	0.3300	4.02		Shallow Concentrated Flow,			
_						Short Grass Pasture Kv= 7.0 fps			
	16.8	269	Total						

Summary for Subcatchment 6S: Flow to Infiltration Trench #2

Runoff = 0.07 cfs @ 12.08 hrs, Volume= 0.01 af, Depth> 0.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	Α	rea (sf)	CN	Description					
-		6,548	30.0	Woods, Good, HSG A					
		9,268	39.0	>75% Grass cover, Good, HSG A					
*		1,000	98.0	Lots, HSG A					
25		16,816		Weighted Average					
		15,816	35.3	94.05% Pervious Area					
		1,000	98.0	5.95% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity Capacity Description (ft/sec) (cfs)					
-	^ ^			DI LEA					

6.0 Direct Entry,

Type III 24-hr 2-YEAR Rainfall=2.95"

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Summary for Subcatchment 7S: Flow to Tributary

Runoff = 0.21 cfs @ 12.26 hrs, Volume=

0.02 af, Depth> 0.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

	Α	rea (sf)	CN	Description	n					
-		1,636	98.0	Roofs, HS	Roofs, HSG A					
		38,714	30.0	Woods, G	/oods, Good, HSG A					
		14,930	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
		3,178	98.0	Paved pa	Paved parking, HSG A					
		58,458		Weighted	Average					
	53,644 32.5			91.77% P	ervious Are	e a				
		4,814	98.0	8.23% Im	pervious A	rea				
	_									
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	17.3	50	0.0100	0.05		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.84"				
	0.9	72	0.0694	1.32		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,				
						Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'				
						n= 0.025 Earth, clean & winding				
	20.2	747	Total							

Summary for Subcatchment 8S: Flow to First Brook

Runoff = 0.00 cfs @ 12.19 hrs, Volume=

0.00 af, Depth> 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 2-YEAR Rainfall=2.95"

,	Area (sf)	CN	Description	n		
	32,083	30.0	Woods, G	Good, HSG	A	
	6,198	39.0	>75% Gra	ass cover, (Good, HSG A	
	79	96.0	Gravel su	rface, HSG	6 A	
	38,360		Weighted Average			
	38,360	31.6	100.00%	Pervious A	rea	
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
13.1	50	0.0200	0.06		Sheet Flow,	
					Woods: Light underbrush n= 0.400 P2= 2.84"	
1.2	150	0.1700	2.06		Shallow Concentrated Flow,	
					Woodland Kv= 5.0 fps	
14.3	200	Total				

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Summary for Pond 1P: Undergound Infiltration System

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 0.78" for 2-YEAR event

Inflow = 2.24 cfs @ 12.08 hrs, Volume= 0.18 af

Outflow = 0.26 cfs @ 11.73 hrs, Volume= 0.18 af, Atten= 88%, Lag= 0.0 min

Discarded = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 136.05' @ 12.68 hrs Surf.Area= 3,776 sf Storage= 2,415 cf Flood Elev= 139.00' Surf.Area= 3,776 sf Storage= 8,688 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 57.9 min (815.5 - 757.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	4,277 cf	32.13'W x 117.54'L x 4.00'H Field A
			15,103 cf Overall - 4,410 cf Embedded = 10,693 cf x 40.0% Voids
#2A	135.50'	4,410 cf	ADS_StormTech SC-740 +Cap x 96 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			96 Chambers in 6 Rows
		8 688 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	134.30'	12.0" Round Culvert
	•		L= 38.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 134.30' / 133.92' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Device 1	137.25'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	138.70'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	135.00	3,000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.26 cfs @ 11.73 hrs HW=135.05' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.26 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=133.82' (Dynamic Tailwater)

-1=Culvert (Passes 0.00 cfs of 1.54 cfs potential flow)
-2=Orifice/Grate (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: DMH#4

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 2-YEAR event Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min O.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dvn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 2-YEAR Rainfall=2.95"

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Peak Elev= 133.82' @ 0.00 hrs

Flood Elev= 143.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	133.82'	12.0" Round Culvert
			L= 198.7' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 133.82' / 131.83' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=133.82' TW=127.70' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 3P: DCB#5

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 0.78" for 2-YEAR event

Inflow = 2.24 cfs @ 12.08 hrs, Volume= 0.18 af

Outflow = 2.24 cfs @ 12.08 hrs, Volume= 0.18 af, Atten= 0%, Lag= 0.0 min

Primary = 2.24 cfs @ 12.08 hrs, Volume= 0.18 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.06' @ 12.08 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.20'	15.0" Round Culvert
			L= 119.6' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.20' / 135.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Primary OutFlow Max=2.22 cfs @ 12.08 hrs HW=137.05' TW=135.63' (Dynamic Tailwater) 1=Culvert (Barrel Controls 2.22 cfs @ 3.52 fps)

Summary for Pond 4P: DCB#50

Inflow Area = 0.993 ac, 36.54% Impervious, Inflow Depth > 0.99" for 2-YEAR event

Inflow = 1.03 cfs @ 12.08 hrs, Volume= 0.08 af

Outflow = 1.03 cfs @ 12.08 hrs, Volume= 0.08 af, Atten= 0%, Lag= 0.0 min

Primary = 1.03 cfs @ 12.08 hrs, Volume= 0.08 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.35' @ 12.10 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.74'	12.0" Round Culvert
	_		L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.74' / 136.30' S= 0.0200 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.97 cfs @ 12.08 hrs HW=137.34' TW=137.05' (Dynamic Tailwater)
1=Culvert (Outlet Controls 0.97 cfs @ 2.84 fps)

Type III 24-hr 2-YEAR Rainfall=2.95"

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Summary for Pond 5P: Infiltration Trench #1

Inflow Area = 0.540 ac, 12.75% Impervious, Inflow Depth > 0.35" for 2-YEAR event

Inflow = 0.14 cfs @ 12.22 hrs, Volume= 0.02 af

Outflow = 0.03 cfs @ 11.88 hrs, Volume= 0.02 af, Atten= 81%, Lag= 0.0 min

Discarded = 0.03 cfs @ 11.88 hrs, Volume= 0.02 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 139.25' @ 12.84 hrs Surf.Area= 384 sf Storage= 192 cf

Flood Elev= 141.00' Surf.Area= 1,572 sf Storage= 1,285 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 42.5 min (809.0 - 766.6)

Volume	Inve	rt Ava	il.Storage	Storage Description					
#1	138.00)'	1,285 c	Custom Stage	Data (Prismatic)	Listed below (Recalc)			
Elevation	on S	Surf.Area	Voids	Inc.Store	Cum.Store				
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)				
138.0	00	384	0.0	0	0				
140.0	00	384	40.0	307	307 307				
141.0	00	1,572	100.0	978	1,285				
Device	Routing	In	vert Ou	ıtlet Devices					
#1	Primary	140).75' 10	.0' long x 4.0' bre	eadth Broad-Cres	sted Rectangular Weir			
	•	,		ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00					
				,	0 3.00 3.50 4.00 4.50 5.00 5.50				
			Co	ef. (English) 2.38	3 2.54 2.69 2.68	3 2.67 2.67 2.65 2.66 2.66			
				38 2.72 2.73 2.7					
#2 Discarded 138.00' 3.000 in/hr Exfiltration over Surface area						area			

Discarded OutFlow Max=0.03 cfs @ 11.88 hrs HW=138.04' (Free Discharge) 2=Exfiltration (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=138.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Infiltration Trench #2

Inflow Area = 0.386 ac, 5.95% Impervious, Inflow Depth > 0.16" for 2-YEAR event
Inflow = 0.07 cfs @ 12.08 hrs, Volume= 0.01 af
Outflow = 0.02 cfs @ 12.03 hrs, Volume= 0.01 af, Atten= 65%, Lag= 0.0 min
Discarded = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs
Peak Elev= 137.21' @ 12.34 hrs Surf.Area= 333 sf Storage= 28 cf

Flood Elev= 140.00' Surf.Area= 1,369 sf Storage= 1,117 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Type III 24-hr 2-YEAR Rainfall=2.95"

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Center-of-Mass det. time= 4.9 min (762.6 - 757.6)

Volume	Inve	rt Ava	il.Storage	Storage Description					
#1	137.0	0'	1,117 cf	Custom Stage	Custom Stage Data (Prismatic) Listed below				
Elevatio	vation Surf.Area Voids (feet) (sq-ft) (%)			Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
		333	0.0	(Cubic-leet)					
			40.0	266	0 266				
140.0		1,369	100.0	851	1,117				
Device	Routing	In	vert Out	t Outlet Devices					
#1	Primary			10.0' long x 10.0' breadth Broad-Crested Rectangular Weir					
#2	Discarde	d 137	Coe	Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64 3.000 in/hr Exfiltration over Surface area					

Discarded OutFlow Max=0.02 cfs @ 12.03 hrs HW=137.04' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=137.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 7P: DMH#3

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 2-YEAR event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af
Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min
Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 127.70' @ 0.00 hrs

Flood Elev= 137.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	127.70'	12.0" Round Culvert
			L= 15.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 127.70' / 126.50' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=127.70' TW=122.80' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 8P: DMH#2

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 2-YEAR event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af
Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 2-YEAR Rainfall=2.95"

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Peak Elev= 122.80' @ 0.00 hrs

Flood Elev= 130.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	122.80'	12.0" Round Culvert
	_		L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 122.80' / 122.00' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=122.80' TW=0.00' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Link A: Central Street

Inflow Area = 0.366 ac, 20.44% Impervious, Inflow Depth > 0.64" for 2-YEAR event

Inflow = 0.20 cfs @ 12.18 hrs, Volume= 0.02 af

Primary = 0.20 cfs @ 12.18 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 1.882 ac, 9.53% Impervious, Inflow Depth > 0.16" for 2-YEAR event

Inflow = 0.21 cfs @ 12.26 hrs, Volume= 0.02 af

Primary = 0.21 cfs @ 12.26 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link C: First Brook

Inflow Area = 7.860 ac, 16.72% Impervious, Inflow Depth > 0.17" for 2-YEAR event

Inflow = 0.88 cfs @ 12.30 hrs, Volume= 0.11 af

Primary = 0.88 cfs @ 12.30 hrs, Volume= 0.11 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 10-YEAR Rainfall=4.45"

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

3 , ,	3 , ,
Subcatchment 1S: Flow from Existing	Runoff Area=86,036 sf 16.27% Impervious Runoff Depth>0.84" Flow Length=162' Tc=24.2 min CN=WQ Runoff=1.03 cfs 0.14 af
Subcatchment 2S: Flow to DCB#5	Runoff Area=75,925 sf 24.53% Impervious Runoff Depth>1.11" Tc=6.0 min CN=WQ Runoff=1.85 cfs 0.16 af
Subcatchment 3S: Flow to DCB#50	Runoff Area=43,243 sf 36.54% Impervious Runoff Depth>1.60" Tc=6.0 min CN=WQ Runoff=1.57 cfs 0.13 af
Subcatchment 4S: Flow to Central Street	et Runoff Area=15,941 sf 20.44% Impervious Runoff Depth>1.07" Flow Length=125' Tc=13.7 min CN=WQ Runoff=0.30 cfs 0.03 af
Subcatchment 5S: Flow to Infiltration	Runoff Area=23,530 sf 12.75% Impervious Runoff Depth>0.60" Flow Length=269' Tc=16.8 min CN=WQ Runoff=0.22 cfs 0.03 af
Subcatchment 6S: Flow to Infiltration	Runoff Area=16,816 sf 5.95% Impervious Runoff Depth>0.31" Tc=6.0 min CN=WQ Runoff=0.10 cfs 0.01 af
Subcatchment 7S: Flow to Tributary	Runoff Area=58,458 sf 8.23% Impervious Runoff Depth>0.37" Flow Length=747' Tc=20.2 min CN=WQ Runoff=0.33 cfs 0.04 af
Subcatchment 8S: Flow to First Brook	Runoff Area=38,360 sf 0.00% Impervious Runoff Depth>0.02" Flow Length=200' Tc=14.3 min CN=WQ Runoff=0.01 cfs 0.00 af
Pond 1P: Undergound Infiltration System Discarded=	m Peak Elev=136.78' Storage=4,459 cf Inflow=3.41 cfs 0.29 af 0.26 cfs 0.29 af Primary=0.00 cfs 0.00 af Outflow=0.26 cfs 0.29 af
Pond 2P: DMH#4 12.0" Rou	Peak Elev=133.82' Inflow=0.00 cfs 0.00 af and Culvert n=0.013 L=198.7' S=0.0100 '/' Outflow=0.00 cfs 0.00 af
Pond 3P: DCB#5 15.0" Rou	Peak Elev=137.32' Inflow=3.41 cfs 0.29 af and Culvert n=0.013 L=119.6' S=0.0050 '/' Outflow=3.41 cfs 0.29 af
Pond 4P: DCB#50	Peak Elev=137.59' Inflow=1.57 cfs 0.13 af bund Culvert n=0.013 L=22.0' S=0.0200'/' Outflow=1.57 cfs 0.13 af
Pond 5P: Infiltration Trench #1 Discarded=	Peak Elev=140.10' Storage=350 cf Inflow=0.22 cfs 0.03 af 0.03 cfs 0.03 af Primary=0.00 cfs 0.00 af Outflow=0.03 cfs 0.03 af
Pond 6P: Infiltration Trench #2 Discarded=	Peak Elev=137.52' Storage=70 cf Inflow=0.10 cfs 0.01 af 0.02 cfs 0.01 af Primary=0.00 cfs 0.00 af Outflow=0.02 cfs 0.01 af
Pond 7P: DMH#3	Peak Elev=127.70' Inflow=0.00 cfs 0.00 af bund Culvert n=0.013 L=15.0' S=0.0800'/' Outflow=0.00 cfs 0.00 af
Pond 8P: DMH#2	Peak Elev=122.80' Inflow=0.00 cfs 0.00 af

12.0" Round Culvert n=0.013 L=10.0' S=0.0800 '/' Outflow=0.00 cfs 0.00 af

Type III 24-hr 10-YEAR Rainfall=4.45"

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Link A: Central Street Inflow=0.30 cfs 0.03 af

Primary=0.30 cfs 0.03 af

Link B: First Brook Tributary Inflow=0.33 cfs 0.04 af

Primary=0.33 cfs 0.04 af

Link C: First Brook Inflow=1.35 cfs 0.18 af

Primary=1.35 cfs 0.18 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.55 af Average Runoff Depth = 0.80" 83.12% Pervious = 6.837 ac 16.88% Impervious = 1.389 ac

Type III 24-hr 10-YEAR Rainfall=4.45"

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Summary for Subcatchment 1S: Flow from Existing House

Runoff = 1.03 cfs @ 12.32 hrs, Volume=

0.14 af, Depth> 0.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	Α	rea (sf)	CN	Description					
		8,242	98.0	Paved pa	A				
		5,752	98.0	Roofs, HS	G A				
		28,793	30.0	Woods, G	lood, HSG	A			
40,866 39.0 >75% Grass cover, Good, HSG A									
		2,383	96.0	Gravel su	rface, HSG	6 A			
_		86,036		Weighted	Average				
		72,042	37.3	83.73% Pervious Area					
	13,994 98.0			16.27% Impervious Area					
	Tc	Length	Slope	Velocity	Capacity	Description			
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	22.8	50	0.0050	0.04		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.84"			
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	24.2	162	Total						

Summary for Subcatchment 2S: Flow to DCB#5

Runoff = 1.85 cfs @ 12.08 hrs, Volume=

0.16 af, Depth> 1.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	Α	rea (sf)	CN	Description							
		8,986	98.0	Paved parking, HSG A							
		56,071	39.0	75% Grass cover, Good, HSG A							
		637	98.0	Roofs, HSG A							
		1,231	30.0	/oods, Good, HSG A							
*	Lots, HSG A										
		75,925		Weighted Average							
		57,302	38.8	75.47% Pervious Area							
		18,623	98.0	24.53% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)								
	6.0			Direct Entry.							

Type III 24-hr 10-YEAR Rainfall=4.45" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 3S: Flow to DCB#50

Runoff = 1.57 cfs @ 12.08 hrs, Volume= 0.13 af, Depth> 1.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

-	Α	rea (sf)	_ CN_	Description								
		27,440	39.0	>75% Gra	>75% Grass cover, Good, HSG A							
		10,803	98.0	Paved par	B A							
*		5,000	98.0	Lots, HSC	Lots, HSG A							
-		43,243		Weighted	Weighted Average							
		27,440	39.0	63.46% Pervious Area								
		15,803	98.0	36.54% Impervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description						
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	6.0					Direct Entry,						

Summary for Subcatchment 4S: Flow to Central Street

Runoff = 0.30 cfs @ 12.18 hrs, Volume= 0.03 af, Depth> 1.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	A	rea (sf)	CN	Description	n							
		11,163	39.0	>75% Gra	75% Grass cover, Good, HSG A							
		1,260	98.0	Roofs, HS	Roofs, HSG A							
		1,998	98.0	Paved pa	Paved parking, HSG A							
		570	96.0	Gravel su	Gravel surface, HSG A							
10		950	30.0	Woods, G	Woods, Good, HSG A							
		15,941		Weighted	Weighted Average							
		12,683	40.9	79.56% P	ervious Are	ea						
		3,258	98.0	20.44% Ir	20.44% Impervious Area							
	Tc	Length	Slope	Velocity	Capacity	Description						
1	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	11.0	40	0.0200	0.06		Sheet Flow,						
						Woods: Light underbrush n= 0.400 P2= 2.84"						
	1.6	10	0.0200	0.10		Sheet Flow,						
						0 0 1 0 0 4 5 0 0 0 0 4 11						
						Grass: Short n= 0.150 P2= 2.84"						
	1.1	75	0.0285	1.18		Shallow Concentrated Flow,						
	1.1	75	0.0285	1.18								

Type III 24-hr 10-YEAR Rainfall=4.45"

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Summary for Subcatchment 5S: Flow to Infiltration Trench #1

Runoff 0.22 cfs @ 12.22 hrs, Volume= 0.03 af, Depth> 0.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

A	rea (sf)	CN	Description	n					
*	3,000	98.0	Lots, HSC	ots, HSG A					
	14,196	39.0	>75% Gra	ass cover, (Good, HSG A				
	6,334	30.0	Woods, G	Good, HSG	A				
	23,530		Weighted	Average					
	20,530	36.2	87.25% P	ervious Are	ea				
	3,000	98.0	12.75% Ir	npervious A	Area				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
13.1	50	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.84"				
3.1	185	0.0200	0.99		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
0.5	22	0.0200	0.71		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
0.0	12	0.3300	4.02		Shallow Concentrated Flow,				
					Short Grass Pasture Kv= 7.0 fps				
16.8	269	Total							

Summary for Subcatchment 6S: Flow to Infiltration Trench #2

Runoff 0.10 cfs @ 12.08 hrs, Volume= 0.01 af, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

	A	rea (sf)	CN	Description	n			
		6,548	30.0	Woods, G	ood, HSG	G A		
		9,268	39.0	>75% Gra	ass cover, (Good, HSG A		
*		1,000	98.0	Lots, HSC	6 A			
		16,816 Weighted Average			Average			
				94.05% P	94.05% Pervious Area			
		1,000 98.0 5.9		5.95% Impervious Area		Area		
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
	6.0					Direct Entry,		

Type III 24-hr 10-YEAR Rainfall=4.45" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 7S: Flow to Tributary

Runoff = 0.33 cfs @ 12.26 hrs, Volume=

0.04 af, Depth> 0.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

A	rea (sf)	CN	Descriptio	n		
	1,636	98.0	Roofs, HS	SG A		
	38,714 30.0 Woods, Good, HSG A			lood, HSG	A	
	14,930	39.0	>75% Gra	iss cover, (Good, HSG A	
	3,178	98.0	Paved par	rking, HSG	Α	
	58,458		Weighted	Average		
	53,644 32.5		91.77% Pervious Area			
	4,814	98.0	8.23% lm	pervious Ai	rea	
				_		
Tc	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
17.3	50	0.0100	0.05		Sheet Flow,	
					Woods: Light underbrush n= 0.400 P2= 2.84"	
0.9	72	0.0694	1.32		Shallow Concentrated Flow,	
					Woodland Kv= 5.0 fps	
2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,	
					Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'	
					n= 0.025 Earth, clean & winding	
20.2	747	Total				

Summary for Subcatchment 8S: Flow to First Brook

Runoff = 0.01 cfs @ 12.19 hrs, Volume=

0.00 af, Depth> 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 10-YEAR Rainfall=4.45"

A	rea (sf)	CN	Description	n	
	32,083	30.0	Woods, G	lood, HSG	A
	6,198	39.0	>75% Gra	iss cover, (Good, HSG A
	79	96.0	Gravel su	rface, HSG	i A
	38,360		Weighted	Average	
	38,360	31.6	100.00%	Pervious A	rea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
13.1	50	0.0200	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.84"
1.2	150	0.1700	2.06		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
14.3	200	Total	·	·	

Type III 24-hr 10-YEAR Rainfall=4.45"

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Summary for Pond 1P: Undergound Infiltration System

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 1.29" for 10-YEAR event Inflow = 0.29 af

Outflow = 0.26 cfs @ 11.46 hrs, Volume= 0.29 af, Atten= 92%, Lag= 0.0 min

Discarded = 0.26 cfs @ 11.46 hrs, Volume= 0.29 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 136.78' @ 13.27 hrs Surf.Area= 3,776 sf Storage= 4,459 cf

Flood Elev= 139.00' Surf.Area= 3,776 sf Storage= 8,688 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 127.1 min (893.8 - 766.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	4,277 cf	32.13'W x 117.54'L x 4.00'H Field A
			15,103 cf Overall - 4,410 cf Embedded = 10,693 cf x 40.0% Voids
#2A	135.50'	4,410 cf	ADS_StormTech SC-740 +Cap x 96 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			96 Chambers in 6 Rows
		8,688 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	134.30'	12.0" Round Culvert
	-		L= 38.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 134.30' / 133.92' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Device 1	137.25'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	138.70'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	135.00'	3.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.26 cfs @ 11.46 hrs HW=135.04' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.26 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=135.00' TW=133.82' (Dynamic Tailwater)

1=Culvert (Passes 0.00 cfs of 1.54 cfs potential flow)

2=Orifice/Grate (Controls 0.00 cfs)

-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: DMH#4

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 10-YEAR event

Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 10-YEAR Rainfall=4.45"

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Peak Elev= 133.82' @ 0.00 hrs

Flood Elev= 143.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	133.82'	12.0" Round Culvert
	·		L= 198.7' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 133.82' / 131.83' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=133.82' TW=127.70' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 3P: DCB#5

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 1.29" for 10-YEAR event Inflow = 3.41 cfs @ 12.08 hrs, Volume= 0.29 af

Outflow = 3.41 cfs @ 12.08 hrs, Volume= 0.29 af, Atten= 0%, Lag= 0.0 min

Primary = 3.41 cfs @ 12.08 hrs, Volume= 0.29 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.32' @ 12.08 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.20'	15.0" Round Culvert
			L= 119.6' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.20' / 135.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Primary OutFlow Max=3.38 cfs @ 12.08 hrs HW=137.32' TW=135.96' (Dynamic Tailwater) 1=Culvert (Barrel Controls 3.38 cfs @ 3.87 fps)

Summary for Pond 4P: DCB#50

Inflow Area = 0.993 ac. 36.54% Impervious, Inflow Depth > 1.60" for 10-YEAR event

Inflow = 1.57 cfs @ 12.08 hrs, Volume= 0.13 af

Outflow = 1.57 cfs @ 12.08 hrs, Volume= 0.13 af, Atten= 0%, Lag= 0.0 min

Primary = 1.57 cfs @ 12.08 hrs, Volume= 0.13 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.59' @ 12.10 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.74'	12.0" Round Culvert
			L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.74' / 136.30' S= 0.0200 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=1.43 cfs @ 12.08 hrs HW=137.57' TW=137.32' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.43 cfs @ 2.79 fps)

Type III 24-hr 10-YEAR Rainfall=4.45"

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Summary for Pond 5P: Infiltration Trench #1

Inflow Area = 0.540 ac, 12.75% Impervious, Inflow Depth > 0.60" for 10-YEAR event

Inflow = 0.22 cfs @ 12.22 hrs, Volume= 0.03 af

Outflow = 0.03 cfs @ 12.96 hrs, Volume= 0.03 af, Atten= 84%, Lag= 44.4 min

Discarded = 0.03 cfs @ 12.96 hrs, Volume= 0.03 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.10' @ 12.96 hrs Surf.Area= 498 sf Storage= 350 cf

Flood Elev= 141.00' Surf.Area= 1,572 sf Storage= 1,285 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 86.7 min (876.5 - 789.8)

Volume	Inve	ert Avai	il.Storage	Storage Description				
#1	138.0	0'	1,285 cf	Custom Stage Data (Prismatic) Listed below (Recalc)				
Elevatio		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
138.0	-	384	0.0	0	0			
140.0	00	384	40.0	307	307			
141.0	00	1,572	100.0	978	1,285			
Device	Routing	In	vert Out	et Devices				
#1	Primary	140	.75' 10. 0	10.0' long x 4.0' breadth Broad-Crested Rectangular Weir				
			Hea	Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00				
			2.50	3.00 3.50 4.00	4.50 5.00 5.50			
			Coe	f. (English) 2.38	2.54 2.69 2.68 2	2.67 2.67 2.65 2.66 2.66		
			2.68	3 2.72 2.73 2.76	2.79 2.88 3.07	3.32		
#2	Discarde	d 138	3.00' 3.00	0 in/hr Exfiltration	n over Surface ai	rea		

Discarded OutFlow Max=0.03 cfs @ 12.96 hrs HW=140.10' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=138.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Infiltration Trench #2

Inflow Area = 0.386 ac, 5.95% Impervious, Inflow Depth > 0.31" for 10-YEAR event
Inflow = 0.10 cfs @ 12.08 hrs, Volume= 0.01 af
Outflow = 0.02 cfs @ 11.88 hrs, Volume= 0.01 af
Outflow = 0.02 cfs @ 11.88 hrs, Volume= 0.01 af
Outflow = 0.02 cfs @ 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 137.52' @ 12.47 hrs Surf.Area= 333 sf Storage= 70 cf Flood Elev= 140.00' Surf.Area= 1,369 sf Storage= 1,117 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Type III 24-hr 10-YEAR Rainfall=4.45"

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Center-of-Mass det. time= 12.0 min (818.3 - 806.3)

Volume	Invert	Avai	I.Storage	Storage Descrip				
#1	#1 137.00' 1,117		1,117 cf	cf Custom Stage Data (Prismatic) Listed below (Recalc)				
Elevation	n 0.	unf Arma	Voide	Ino Ctoro	Cum Chana			
	8	ırf.Area	Voids	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)			
137.0	00	333	0.0	0	0			
139.0	00	333	40.0	266	266			
140.0	00	1,369		851	1,117			
			_					
<u>Device</u>	Routing	ln	vert Out	tlet Devices				
#1	#1 Primary 138.90'		.90' 10.	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir				
	-	•		ad (feet) 0.20 0.4	0 0.60 0.80 1.0	0 1.20 1.40 1.60		
						2.68 2.69 2.67 2.64		
#2	Discarded	137		3.000 in/hr Exfiltration over Su				

Discarded OutFlow Max=0.02 cfs @ 11.88 hrs HW=137.03' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=137.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 7P: DMH#3

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 10-YEAR event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af
Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 127.70' @ 0.00 hrs

Flood Elev= 137.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	127.70'	12.0" Round Culvert
			L= 15.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 127.70' / 126.50' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=127.70' TW=122.80' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 8P: DMH#2

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.00" for 10-YEAR event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af
Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af, Atten= 0%, Lag= 0.0 min
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 10-YEAR Rainfall=4.45"

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Peak Elev= 122.80' @ 0.00 hrs

Flood Elev= 130.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	122.80'	12.0" Round Culvert
			L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 122.80' / 122.00' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=122.80' TW=0.00' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Link A: Central Street

Inflow Area = 0.366 ac, 20.44% Impervious, Inflow Depth > 1.07" for 10-YEAR event

Inflow = 0.30 cfs @ 12.18 hrs, Volume= 0.03 af

Primary = 0.30 cfs @ 12.18 hrs, Volume= 0.03 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 1.882 ac, 9.53% Impervious, Inflow Depth > 0.27" for 10-YEAR event

Inflow = 0.33 cfs @ 12.26 hrs, Volume= 0.04 af

Primary = 0.33 cfs @ 12.26 hrs, Volume= 0.04 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link C: First Brook

Inflow Area = 7.860 ac. 16.72% Impervious, Inflow Depth > 0.28" for 10-YEAR event

Inflow = 1.35 cfs @ 12.30 hrs, Volume= 0.18 af

Primary = 1.35 cfs @ 12.30 hrs, Volume= 0.18 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Pond 7P: DMH#3

Type III 24-hr 25-YEAR Rainfall=5.62"

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Flow from Existing	Runoff Area=86,036 sf 16.27% Impervious Runoff Depth>1.19" Flow Length=162' Tc=24.2 min CN=WQ Runoff=1.32 cfs 0.20 af
Subcatchment 2S: Flow to DCB#5	Runoff Area=75,925 sf 24.53% Impervious Runoff Depth>1.57" Tc=6.0 min CN=WQ Runoff=2.34 cfs 0.23 af
Subcatchment 3S: Flow to DCB#50	Runoff Area=43,243 sf 36.54% Impervious Runoff Depth>2.18" Tc=6.0 min CN=WQ Runoff=1.99 cfs 0.18 af
Subcatchment 4S: Flow to Central Street	et Runoff Area=15,941 sf 20.44% Impervious Runoff Depth>1.52" Flow Length=125' Tc=13.7 min CN=WQ Runoff=0.38 cfs 0.05 af
Subcatchment 5S: Flow to Infiltration	Runoff Area=23,530 sf 12.75% Impervious Runoff Depth>0.90" Flow Length=269' Tc=16.8 min CN=WQ Runoff=0.28 cfs 0.04 af
Subcatchment 6S: Flow to Infiltration	Runoff Area=16,816 sf 5.95% Impervious Runoff Depth>0.52" Tc=6.0 min CN=WQ Runoff=0.13 cfs 0.02 af
Subcatchment 7S: Flow to Tributary	Runoff Area=58,458 sf 8.23% Impervious Runoff Depth>0.55" Flow Length=747' Tc=20.2 min CN=WQ Runoff=0.42 cfs 0.06 af
Subcatchment 8S: Flow to First Brook	Runoff Area=38,360 sf 0.00% Impervious Runoff Depth>0.10" Flow Length=200' Tc=14.3 min CN=WQ Runoff=0.02 cfs 0.01 af
Pond 1P: Undergound Infiltration System Discarded=	m Peak Elev=137.62' Storage=6,520 cf Inflow=4.32 cfs 0.41 af 0.26 cfs 0.36 af Primary=0.12 cfs 0.02 af Outflow=0.38 cfs 0.38 af
Pond 2P: DMH#4 12.0" Rou	Peak Elev=133.99' Inflow=0.12 cfs 0.02 af and Culvert n=0.013 L=198.7' S=0.0100 '/' Outflow=0.12 cfs 0.02 af
Pond 3P: DCB#5 15.0" Rou	Peak Elev=137.63' Inflow=4.32 cfs 0.41 af and Culvert n=0.013 L=119.6' S=0.0050 '/' Outflow=4.32 cfs 0.41 af
Pond 4P: DCB#50	Peak Elev=137.80' Inflow=1.99 cfs 0.18 af ound Culvert n=0.013 L=22.0' S=0.0200 '/' Outflow=1.99 cfs 0.18 af
Pond 5P: Infiltration Trench #1 Discarded=	Peak Elev=140.35' Storage=511 cf Inflow=0.28 cfs 0.04 af 0.06 cfs 0.04 af Primary=0.00 cfs 0.00 af Outflow=0.06 cfs 0.04 af
Pond 6P: Infiltration Trench #2	Peak Elev=138.06' Storage=141 cf Inflow=0.13 cfs 0.02 af

Pond 8P: DMH#2 Peak Elev=122.97' Inflow=0.12 cfs 0.02 af 12.0" Round Culvert n=0.013 L=10.0' S=0.0800 '/' Outflow=0.12 cfs 0.02 af

Discarded=0.02 cfs 0.02 af Primary=0.00 cfs 0.00 af Outflow=0.02 cfs 0.02 af

12.0" Round Culvert n=0.013 L=15.0' S=0.0800 '/' Outflow=0.12 cfs 0.02 af

Peak Elev=127.87' Inflow=0.12 cfs 0.02 af

Type III 24-hr 25-YEAR Rainfall=5.62"

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Link A: Central Street Inflow=0.38 cfs 0.05 af

Primary=0.38 cfs 0.05 af

Link B: First Brook Tributary Inflow=0.42 cfs 0.06 af

Primary=0.42 cfs 0.06 af

Link C: First Brook Inflow=1.74 cfs 0.29 af

Primary=1.74 cfs 0.29 af

Total Runoff Area = 8.226 ac Runoff Volume = 0.78 af Average Runoff Depth = 1.13" 83.12% Pervious = 6.837 ac 16.88% Impervious = 1.389 ac

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Subcatchment 1S: Flow from Existing House

Runoff = 1.32 cfs @ 12.32 hrs, Volume=

0.20 af, Depth> 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	Α	rea (sf)	CN	Description	n				
		8,242	98.0	Paved par	rking, HSG	A			
		5,752	98.0	Roofs, HS	SG A				
		28,793	30.0	Woods, Good, HSG A					
		40,866	39.0	>75% Grass cover, Good, HSG A					
		2,383	96.0	Gravel su	rface, HSG	6 A			
86,036 Weighted Average					Average				
72,042 37.3 83.73% Pervious Are				83.73% P	ervious Are	ea			
		13,994	98.0	16.27% In	npervious A	Area			
	Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	22.8	50	0.0050	0.04		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.84"			
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,			
_						Woodland Kv= 5.0 fps			
	24.2	162	Total						

Summary for Subcatchment 2S: Flow to DCB#5

Runoff = 2.34 cfs @ 12.08 hrs, Volume=

0.23 af, Depth> 1.57"

/	Area (sf)	CN	Description					
	8,986	98.0	Paved parking, HSG A					
	56,071	39.0	>75% Grass cover, Good, HSG A					
	637	98.0	Roofs, HSG A					
	1,231	30.0	Woods, Good, HSG A					
*	9,000	98.0	Lots, HSG A	_				
	75,925		Weighted Average					
	57,302	38.8	75.47% Pervious Area					
	18,623	98.0	24.53% Impervious Area					
To	= 10 3 10	Slope						
(min)	(feet)	(ft/ft)	(ft/sec) (cfs)					
6.0			Direct Entry,					

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Subcatchment 3S: Flow to DCB#50

Runoff = 1.99 cfs @ 12.08 hrs, Volume= 0.18 af, Depth> 2.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

_	Α	rea (sf)	CN	Description	Description					
		27,440	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
		10,803	98.0	Paved par	rking, HSG	3 A				
*		5,000	98.0	Lots, HSG	Lots, HSG A					
		43,243		Weighted	Weighted Average					
		27,440	39.0	63.46% Pervious Area						
		15,803	98.0	36.54% In	npervious A	Area				
	Тс	Length	Slope	Velocity	Capacity	Description				
(1	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·				
05	6.0			Direct Entry,						

Summary for Subcatchment 4S: Flow to Central Street

Runoff = 0.38 cfs @ 12.18 hrs, Volume= 0.05 af, Depth> 1.52"

6	A	rea (sf)	CN	Description	n	
		11,163	39.0	>75% Gra	ass cover, (Good, HSG A
		1,260	98.0	Roofs, HS	SG A	
		1,998	98.0	Paved pa	rking, HSG	A
		570	96.0	Gravel su	rface, HSG	S A
		950	30.0	Woods, G	lood, HSG	Α
35		15,941		Weighted	Average	
		12,683	40.9	79.56% P	ervious Are	ea
		3,258	98.0	20.44% Ir	npervious /	Area
					•	
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	11.0	40	0.0200	0.06		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.84"
	1.6	10	0.0200	0.10		Sheet Flow,
						Grass: Short n= 0.150 P2= 2.84"
	1.1	75	0.0285	1.18		Shallow Concentrated Flow,
72						Short Grass Pasture Kv= 7.0 fps
	13.7	125	Total			

Type III 24-hr 25-YEAR Rainfall=5.62" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 5S: Flow to Infiltration Trench #1

Runoff = 0.28 cfs @ 12.22 hrs, Volume= 0.04 af, Depth> 0.90"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

-	Α	rea (sf)	CN	Description	n					
*		3,000	98.0	Lots, HSG	Lots, HSG A					
		14,196	39.0	>75% Gra	ass cover, (Good, HSG A				
		6,334	30.0	Woods, G	Good, HSG	Α				
		23,530		Weighted	Veighted Average					
		20,530	36.2	87.25% P	ervious Are	ea ea				
		3,000	98.0	12.75% Ir	npervious A	Area				
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	13.1	50	0.0200	0.06		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.84"				
	3.1	185	0.0200	0.99		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,				
						Woodland Kv= 5.0 fps				
	0.0	12	0.3300	4.02		Shallow Concentrated Flow,				
-						Short Grass Pasture Kv= 7.0 fps				
	16.8	269	Total							

Summary for Subcatchment 6S: Flow to Infiltration Trench #2

Runoff = 0.13 cfs @ 12.09 hrs, Volume= 0.02 af, Depth> 0.52"

	Area (sf)	CN	Description	n					
	6,548	30.0	Woods, G	Woods, Good, HSG A					
	9,268	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
*	1,000	98.0	Lots, HSC	Lots, HSG A					
	16,816		Weighted	Average					
	15,816	35.3	94.05% P	ervious Are	rea				
	1,000	98.0	5.95% lm	pervious Ai	Area				
T (min	70 TO 10	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	•				
6.	0				Direct Entry,				

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Subcatchment 7S: Flow to Tributary

Runoff = 0.42 cfs @ 12.27 hrs, Volume= 0.06 af, Depth> 0.55"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 25-YEAR Rainfall=5.62"

	Α	rea (sf)	CN	Description	n						
		1,636	98.0	Roofs, HS	Roofs, HSG A						
		38,714	30.0	Woods, G	Woods, Good, HSG A						
		14,930	39.0	>75% Grass cover, Good, HSG A							
		3,178	98.0	Paved parking, HSG A							
		58,458		Weighted	Average						
		53,644	32.5	91.77% P	ervious Are	ea					
		4,814	98.0	8.23% lm	pervious Aı	rea					
	_										
	Tc	Length	Slope	Velocity	Capacity	Description					
ı, E	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	17.3	50	0.0100	0.05		Sheet Flow,					
						Woods: Light underbrush n= 0.400 P2= 2.84"					
	0.9	72	0.0694	1.32		Shallow Concentrated Flow,					
						Woodland Kv= 5.0 fps					
	2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,					
						Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'					
23						n= 0.025 Earth, clean & winding					
	20.2	747	Total								

Summary for Subcatchment 8S: Flow to First Brook

Runoff = 0.02 cfs @ 12.48 hrs, Volume= 0.01 af, Depth> 0.10"

	A	rea (sf)	CN	Description	n				
55		32,083	30.0	Woods, G	/oods, Good, HSG A				
		6,198	39.0	>75% Gra	75% Grass cover, Good, HSG A				
		79	96.0	Gravel su	ravel surface, HSG A				
	38,360 Weighted Average								
38,360 31.6 100.00% Pervious Area					rea				
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	13.1	50	0.0200	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.84"			
	1.2	150	0.1700	2.06		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
100	14.3	200	Total						

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Pond 1P: Undergound Infiltration System

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 1.79" for 25-YEAR event
Inflow = 4.32 cfs @ 12.08 hrs, Volume= 0.41 af
Outflow = 0.38 cfs @ 13.50 hrs, Volume= 0.38 af, Atten= 91%, Lag= 85.0 min
Discarded = 0.12 cfs @ 11.10 hrs, Volume= 0.36 af
Primary = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 137.62' @ 13.50 hrs Surf.Area= 3,776 sf Storage= 6,520 cf Flood Elev= 139.00' Surf.Area= 3,776 sf Storage= 8,688 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 150.4 min (926.6 - 776.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	4,277 cf	32.13'W x 117.54'L x 4.00'H Field A
			15,103 cf Overall - 4,410 cf Embedded = 10,693 cf x 40.0% Voids
#2A	135.50'	4,410 cf	ADS_StormTech SC-740 +Cap x 96 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			96 Chambers in 6 Rows
		8,688 cf	Total Available Storage

Storage Group A created with Chamber Wizard

D	evice	Routing	Invert	Outlet Devices
	#1	Primary	134.30'	12.0" Round Culvert
		-		L= 38.0' CPP, square edge headwall, Ke= 0.500
				Inlet / Outlet Invert= 134.30' / 133.92' S= 0.0100 '/' Cc= 0.900
				n= 0.013, Flow Area= 0.79 sf
	#2	Device 1	137.25'	3.0" Vert. Orifice/Grate C= 0.600
	#3	Device 1	138.70'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
	#4	Discarded	135.00'	3.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.26 cfs @ 11.10 hrs HW=135.04' (Free Discharge) —4=Exfiltration (Exfiltration Controls 0.26 cfs)

Primary OutFlow Max=0.12 cfs @ 13.50 hrs HW=137.62' TW=133.99' (Dynamic Tailwater)

-1=Culvert (Passes 0.12 cfs of 6.31 cfs potential flow)
-2=Orifice/Grate (Orifice Controls 0.12 cfs @ 2.40 fps)
-3=Sharp-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: DMH#4

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.11" for 25-YEAR event
Inflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af
Outflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min
Outflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 25-YEAR Rainfall=5.62"

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Peak Elev= 133.99' @ 13.50 hrs

Flood Elev= 143.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	133.82'	12.0" Round Culvert
			L= 198.7' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 133.82' / 131.83' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.12 cfs @ 13.50 hrs HW=133.99' TW=127.87' (Dynamic Tailwater)
1=Culvert (Barrel Controls 0.12 cfs @ 2.07 fps)

Summary for Pond 3P: DCB#5

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 1.79" for 25-YEAR event

Inflow = 4.32 cfs @ 12.08 hrs, Volume= 0.41 af

Outflow = 4.32 cfs @ 12.08 hrs, Volume= 0.41 af, Atten= 0%, Lag= 0.0 min

Primary = 4.32 cfs @ 12.08 hrs, Volume= 0.41 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.63' @ 13.51 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.20'	15.0" Round Culvert
			L= 119.6' CPP, square edge headwall, Ke= 0.500
			inlet / Outlet Invert= 136.20' / 135.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Primary OutFlow Max=4.29 cfs @ 12.08 hrs HW=137.54' TW=136.26' (Dynamic Tailwater) 1=Culvert (Barrel Controls 4.29 cfs @ 4.06 fps)

Summary for Pond 4P: DCB#50

Inflow Area = 0.993 ac, 36.54% Impervious, Inflow Depth > 2.18" for 25-YEAR event

Inflow = 1.99 cfs @ 12.08 hrs, Volume= 0.18 af

Outflow = 1.99 cfs @ 12.08 hrs, Volume= 0.18 af, Atten= 0%, Lag= 0.0 min

Primary = 1.99 cfs @ 12.08 hrs, Volume= 0.18 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 137.80' @ 12.10 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.74'	12.0" Round Culvert
			L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.74' / 136.30' S= 0.0200 '/' Cc= 0.900
			n= 0.013. Flow Area= 0.79 sf

Primary OutFlow Max=1.74 cfs @ 12.08 hrs HW=137.76' TW=137.54' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.74 cfs @ 2.68 fps)

Type III 24-hr 25-YEAR Rainfall=5.62"

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Summary for Pond 5P: Infiltration Trench #1

Inflow Area = 0.540 ac, 12.75% Impervious, Inflow Depth > 0.90" for 25-YEAR event

Inflow = 0.28 cfs @ 12.22 hrs, Volume= 0.04 af

Outflow = 0.06 cfs @ 13.08 hrs, Volume= 0.04 af, Atten= 80%, Lag= 51.0 min

Discarded = 0.06 cfs @ 13.08 hrs, Volume= 0.04 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.35' @ 13.08 hrs Surf.Area= 795 sf Storage= 511 cf Flood Elev= 141.00' Surf.Area= 1,572 sf Storage= 1,285 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 105.9 min (916.6 - 810.7)

Volume	Inve	rt Avai	I.Storage	Storage Description			
#1	138.0	138.00'		Custom Stage I	e Data (Prismatic) Listed below (Recalc)		
Elevation	on -	Surf.Area	Voids	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)		
138.0	00	384	0.0	0	0		
140.0	00	384	40.0	307	307		
141.0	00	1,572	100.0	978	1,285		
Device	Routing	ln	vert Out	let Devices			
#1	Primary	140).75' 10. 0)' long x 4.0' brea	adth Broad-Crest	ed Rectangular Weir	
	-		Hea	d (feet) 0.20 0.4	0 0.60 0.80 1.00	1.20 1.40 1.60 1.80 2.00	
			2.50	0 3.00 3.50 4.00 4.50 5.00 5.50			
			Coe	ef. (English) 2.38	2.54 2.69 2.68	2.67 2.67 2.65 2.66 2.66	
					2.79 2.88 3.07		
#2	Discarde	d 138	3.00' 3.0 0	00 in/hr Exfiltratio	n over Surface a	rea	

Discarded OutFlow Max=0.06 cfs @ 13.08 hrs HW=140.35' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.06 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=138.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Infiltration Trench #2

 Inflow Area =
 0.386 ac, 5.95% Impervious, Inflow Depth > 0.52" for 25-YEAR event

 Inflow =
 0.13 cfs @ 12.09 hrs, Volume=
 0.02 af

 Outflow =
 0.02 cfs @ 11.82 hrs, Volume=
 0.02 af, Atten= 82%, Lag= 0.0 min

Discarded = 0.02 cfs @ 11.82 hrs, Volume= 0.02 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 138.06' @ 12.97 hrs Surf.Area= 333 sf Storage= 141 cf Flood Elev= 140.00' Surf.Area= 1,369 sf Storage= 1,117 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

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Center-of-Mass det. time= 39.1 min (878.7 - 839.6)

Volume	Inve	ert Ava	il.Storage	e Storage Description			
#1	137.0	0'	1,117 cf	Custom Stage D	Pata (Prismatic) Lis	ted below (Recalc)	
Elevation	19545	Surf.Area	Voids	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)		
137.0	00	333	0.0	0	0		
139.0	00	333	40.0	266	266		
140.0	00	1,369	100.0	851	1,117		
Device	Routing	In	vert Out	let Devices			
#1 Primary 138.90' 10.0 '		0.0' long x 10.0' breadth Broad-Crested Rectangular Weir					
	,	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60			
				. ,		68 2.69 2.67 2.64	
#2	Discarde	d 137		100 in/hr Exfiltration over Surface area			

Discarded OutFlow Max=0.02 cfs @ 11.82 hrs HW=137.04' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=137.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 7P: DMH#3

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.11" for 25-YEAR event
Inflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af
Outflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min
Primary = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 127.87' @ 13.50 hrs

Flood Elev= 137.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	127.70'	12.0" Round Culvert
	_		L= 15.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 127.70' / 126.50' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.12 cfs @ 13.50 hrs HW=127.87' TW=122.97' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.12 cfs @ 1.38 fps)

Summary for Pond 8P: DMH#2

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.11" for 25-YEAR event
Inflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af
Outflow = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.0 min
Primary = 0.12 cfs @ 13.50 hrs, Volume= 0.02 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

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Peak Elev= 122.97' @ 13.50 hrs

Flood Elev= 130.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	122.80'	12.0" Round Culvert
			L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 122.80' / 122.00' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.12 cfs @ 13.50 hrs HW=122.97' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.12 cfs @ 1.38 fps)

Summary for Link A: Central Street

Inflow Area = 0.366 ac, 20.44% Impervious, Inflow Depth > 1.52" for 25-YEAR event

Inflow = 0.38 cfs @ 12.18 hrs, Volume= 0.05 af

Primary = 0.38 cfs @ 12.18 hrs, Volume= 0.05 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 1.882 ac, 9.53% Impervious, Inflow Depth > 0.39" for 25-YEAR event

Inflow = 0.42 cfs @ 12.27 hrs, Volume= 0.06 af

Primary = 0.42 cfs @ 12.27 hrs, Volume= 0.06 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link C: First Brook

Inflow Area = 7.860 ac, 16.72% Impervious, Inflow Depth > 0.44" for 25-YEAR event

Inflow = 1.74 cfs @ 12.31 hrs, Volume= 0.29 af

Primary = 1.74 cfs @ 12.31 hrs, Volume= 0.29 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

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Time span=0.00-24.00 hrs, dt=0.03 hrs, 801 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-Q
Reach routing by Dyn-Stor-Ind method

Subcatchment 1S: Flow from Existing	Runoff Area=86,036 sf 16.27% Impervious Runoff Depth>1.59" Flow Length=162' Tc=24.2 min CN=WQ Runoff=1.72 cfs 0.26 af
Subcatchment 2S: Flow to DCB#5	Runoff Area=75,925 sf 24.53% Impervious Runoff Depth>2.09" Tc=6.0 min CN=WQ Runoff=3.08 cfs 0.30 af
Subcatchment 3S: Flow to DCB#50	Runoff Area=43,243 sf 36.54% Impervious Runoff Depth>2.79" Tc=6.0 min CN=WQ Runoff=2.51 cfs 0.23 af
Subcatchment 4S: Flow to Central Street	Runoff Area=15,941 sf 20.44% Impervious Runoff Depth>2.02" Flow Length=125' Tc=13.7 min CN=WQ Runoff=0.50 cfs 0.06 af
Subcatchment 5S: Flow to Infiltration	Runoff Area=23,530 sf 12.75% Impervious Runoff Depth>1.27" Flow Length=269' Tc=16.8 min CN=WQ Runoff=0.39 cfs 0.06 af
Subcatchment 6S: Flow to Infiltration	Runoff Area=16,816 sf 5.95% Impervious Runoff Depth>0.82" Tc=6.0 min CN=WQ Runoff=0.20 cfs 0.03 af
Subcatchment 7S: Flow to Tributary	Runoff Area=58,458 sf 8.23% Impervious Runoff Depth>0.81" Flow Length=747' Tc=20.2 min CN=WQ Runoff=0.55 cfs 0.09 af
Subcatchment 8S: Flow to First Brook	Runoff Area=38,360 sf 0.00% Impervious Runoff Depth>0.26" Flow Length=200' Tc=14.3 min CN=WQ Runoff=0.05 cfs 0.02 af
Pond 1P: Undergound Infiltration System Discarded=	m Peak Elev=138.77' Storage=8,340 cf Inflow=5.59 cfs 0.53 af 0.26 cfs 0.37 af Primary=0.52 cfs 0.10 af Outflow=0.78 cfs 0.47 af
Pond 2P: DMH#4 12.0" Rou	Peak Elev=134.18' Inflow=0.52 cfs 0.10 af and Culvert n=0.013 L=198.7' S=0.0100 '/' Outflow=0.52 cfs 0.10 af
Pond 3P: DCB#5	Peak Elev=138.80' Inflow=5.59 cfs 0.53 af and Culvert n=0.013 L=119.6' S=0.0050 '/' Outflow=5.59 cfs 0.53 af
Pond 4P: DCB#50	Peak Elev=138.80' Inflow=2.51 cfs 0.23 afound Culvert n=0.013 L=22.0' S=0.0200'/' Outflow=2.51 cfs 0.23 af
Pond 5P: Infiltration Trench #1 Discarded=	Peak Elev=140.60' Storage=749 cf Inflow=0.39 cfs 0.06 af 0.08 cfs 0.05 af Primary=0.00 cfs 0.00 af Outflow=0.08 cfs 0.05 af
Pond 6P: Infiltration Trench #2 Discarded=	Peak Elev=138.91' Storage=255 cf Inflow=0.20 cfs 0.03 af 0.02 cfs 0.02 af Primary=0.03 cfs 0.00 af Outflow=0.05 cfs 0.03 af
Pond 7P: DMH#3	Peak Elev=128.06' Inflow=0.52 cfs 0.10 af ound Culvert n=0.013 L=15.0' S=0.0800'/' Outflow=0.52 cfs 0.10 af
Pond 8P: DMH#2	Peak Elev=123.16' Inflow=0.52 cfs 0.10 af

12.0" Round Culvert n=0.013 L=10.0' S=0.0800 '/' Outflow=0.52 cfs 0.10 af

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Link A: Central Street

Inflow=0.50 cfs 0.06 af
Primary=0.50 cfs 0.06 af

Link B: First Brook Tributary

Inflow=0.55 cfs 0.09 af
Primary=0.55 cfs 0.09 af

Link C: First Brook Inflow=2.48 cfs 0.47 af

Primary=2.48 cfs 0.47 af

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Total Runoff Area = 8.226 ac Runoff Volume = 1.05 af Average Runoff Depth = 1.53" 83.12% Pervious = 6.837 ac 16.88% Impervious = 1.389 ac

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Summary for Subcatchment 1S: Flow from Existing House

Runoff = 1.72 cfs @ 12.34 hrs, Volume= 0.26 af, Depth> 1.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

	A	rea (sf)	CN	Description	n				
		8,242	98.0	Paved par	Paved parking, HSG A				
		5,752	98.0	Roofs, HS	Roofs, HSG A				
		28,793	30.0	Woods, G	Woods, Good, HSG A				
		40,866	39.0	>75% Gra	>75% Grass cover, Good, HSG A				
_		2,383	96.0	Gravel su	Gravel surface, HSG A				
		86,036		Weighted	Weighted Average				
		72,042	37.3	83.73% P	ervious Are	ea			
		13,994	98.0	16.27% In	npervious A	Area			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	22.8	50	0.0050	0.04		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.84"			
	1.4	112	0.0714	1.34		Shallow Concentrated Flow,			
						Woodland Kv= 5.0 fps			
	24.2	162	Total						

Summary for Subcatchment 2S: Flow to DCB#5

Runoff = 3.08 cfs @ 12.09 hrs, Volume= 0.30 af, Depth> 2.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

Α	Area (sf)	CN	Description						
	8,986	98.0	Paved parl	Paved parking, HSG A					
	56,071	39.0	>75% Gras	>75% Grass cover, Good, HSG A					
	637	98.0	Roofs, HS	Roofs, HSG A					
	1,231	30.0	Woods, Go	Woods, Good, HSG A					
*	9,000	98.0	Lots, HSG	Lots, HSG A					
	75,925		Weighted Average						
	57,302	38.8	75.47% Pe	ervious Are	rea				
	18,623	98.0	24.53% Impervious Are		s Area				
Tc	, O . , , , , , , , , , , , , , , , , ,	Slope	1000 D	Capacity					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Discot Entre				

6.0 Direct Entry,

Type III 24-hr 50-YEAR Rainfall=6.72" Revised June 8. 2022 Printed 6/9/2022

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Summary for Subcatchment 3S: Flow to DCB#50

Runoff = 2.51 cfs @ 12.09 hrs, Volume=

0.23 af, Depth> 2.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

	Area (sf)	CN	Description						
	27,440	39.0	>75% Gra	>75% Grass cover, Good, HSG A					
	10,803	98.0	Paved pa	Paved parking, HSG A					
*	5,000	98.0	Lots, HSC	Lots, HSG A					
	43,243		Weighted Average						
	27,440	39.0	63.46% P	ervious Are	rea				
	15,803	98.0	36.54% Ir	npervious /	Area				
	Tc Length	Slope	Velocity	Capacity					
(m	in) (feet)	(ft/ft)	(ft/sec)	(cfs)					
6	3.0				Direct Entry,				

Summary for Subcatchment 4S: Flow to Central Street

Runoff = 0.50 cfs @ 12.19 hrs, Volume=

0.06 af, Depth> 2.02"

A	rea (sf)	CN	Description	n				
	11,163	39.0	>75% Gra	75% Grass cover, Good, HSG A				
	1,260	98.0	Roofs, HS	SG A				
	1,998	98.0	Paved par	Paved parking, HSG A				
	570	96.0	Gravel su	rface, HSG	S A			
	950	30.0	Woods, G	Good, HSG	Α			
	15,941		Weighted	Average				
	12,683	40.9	79.56% P	ervious Are	e a			
	3,258	98.0	20.44% In	npervious A	Area			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)_	(feet)	(ft/ft)	(ft/sec)	(cfs)				
11.0	40	0.0200	0.06		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.84"			
1.6	10	0.0200	0.10		Sheet Flow,			
					Grass: Short n= 0.150 P2= 2.84"			
1.1	75	0.0285	1.18		Shallow Concentrated Flow,			
					Short Grass Pasture Kv= 7.0 fps			
13.7	125	Total						

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Summary for Subcatchment 5S: Flow to Infiltration Trench #1

Runoff = 0.39 cfs @ 12.25 hrs, Volume= 0.06 af, Depth> 1.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

	Α	rea (sf)	CN	Description	n			
*		3,000	98.0	Lots, HSC	A G			
		14,196	39.0	>75% Gra	ass cover, (Good, HSG A		
		6,334	30.0	Woods, Good, HSG A				
		23,530		Weighted Average				
		20,530	36.2	87.25% P	ervious Are	ea		
		3,000	98.0	12.75% Ir	npervious /	Area		
	Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	13.1	50	0.0200	0.06		Sheet Flow,		
						Woods: Light underbrush n= 0.400 P2= 2.84"		
	3.1	185	0.0200	0.99		Shallow Concentrated Flow,		
						Short Grass Pasture Kv= 7.0 fps		
	0.5	22	0.0200	0.71		Shallow Concentrated Flow,		
						Woodland Kv= 5.0 fps		
	0.0	12	0.3300	4.02		Shallow Concentrated Flow,		
						Short Grass Pasture Kv= 7.0 fps		
•	16.8	269	Total					

Summary for Subcatchment 6S: Flow to Infiltration Trench #2

Runoff = 0.20 cfs @ 12.11 hrs, Volume= 0.03 af, Depth> 0.82"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

,	Α	rea (sf)	CN	Description					
6,548 30.0 Woods, Good, HSG A						A			
		9,268	39.0	>75% Gra					
*		1,000	98.0	Lots, HSC	Lots, HSG A				
		16,816		Weighted Average					
		15,816	35.3	94.05% Pervious Area					
		1,000	98.0	5.95% Impervious Area					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
	0.0					Discort Forton			

6.0 Direct Entry,

Type III 24-hr 50-YEAR Rainfall=6.72" Revised June 8, 2022 Printed 6/9/2022

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Summary for Subcatchment 7S: Flow to Tributary

Runoff = 0.55 cfs @ 12.29 hrs, Volume= 0.09 af, Depth> 0.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-Q, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Type III 24-hr 50-YEAR Rainfall=6.72"

A	rea (sf)	CN	Description	n	
	1,636	98.0	Roofs, HS	SG A	
	38,714	30.0	Woods, G	Good, HSG	A
	14,930	39.0	>75% Gra	ass cover, (Good, HSG A
	3,178	98.0	Paved par	rking, HSG	Α
	58,458		Weighted	Average	
	53,644 32.5		91.77% P	ervious Are	ea
	4,814	98.0	8.23% lm	pervious Ai	rea
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
17.3	50	0.0100	0.05		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 2.84"
0.9	72	0.0694	1.32		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
2.0	625	0.0100	5.11	66.39	Trap/Vee/Rect Channel Flow,
					Bot.W=10.00' D=1.00' Z= 3.0 '/' Top.W=16.00'
					n= 0.025 Earth, clean & winding
20.2	747	Total			

Summary for Subcatchment 8S: Flow to First Brook

Runoff = 0.05 cfs @ 12.38 hrs, Volume= 0.02 af, Depth> 0.26"

ΑΑ	rea (sf)	CN	Description	n			
	32,083	30.0	Woods, G	lood, HSG	A		
	6,198	39.0	>75% Gra	iss cover, (Good, HSG A		
·	79	96.0	Gravel su	rface, HSG	6 A		
	38,360		Weighted	Weighted Average			
	38,360	31.6	100.00%	Pervious A	rea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
13.1	50	0.0200	0.06		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 2.84"		
1.2	150	0.1700	2.06		Shallow Concentrated Flow,		
·					Woodland Kv= 5.0 fps		
14.3	200	Total					

Type III 24-hr 50-YEAR Rainfall=6.72"

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Summary for Pond 1P: Undergound Infiltration System

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 2.34" for 50-YEAR event

Inflow 5.59 cfs @ 12.09 hrs. Volume= 0.53 af

Outflow = 0.78 cfs @ 12.80 hrs, Volume= 0.47 af. Atten= 86%. Lag= 42.7 min

0.26 cfs @ 10.65 hrs, Volume= Discarded = 0.37 af 0.52 cfs @ 12.80 hrs, Volume= Primary = 0.10 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 138.77' @ 12.80 hrs Surf.Area= 3,776 sf Storage= 8,340 cf

Flood Elev= 139.00' Surf.Area= 3,776 sf Storage= 8,688 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 120.3 min (902.3 - 782.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	135.00'	4,277 cf	32.13'W x 117.54'L x 4.00'H Field A
			15,103 cf Overall - 4,410 cf Embedded = 10,693 cf x 40.0% Voids
#2A	135.50'	4,410 cf	ADS_StormTech SC-740 +Cap x 96 Inside #1
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			96 Chambers in 6 Rows
		8,688 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	134.30'	12.0" Round Culvert
			L= 38.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 134.30' / 133.92' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf
#2	Device 1	137.25'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	138.70'	4.0' long Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Discarded	135.00'	3.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.26 cfs @ 10.65 hrs HW=135.04' (Free Discharge) **-4=Exfiltration** (Exfiltration Controls 0.26 cfs)

Primary OutFlow Max=0.52 cfs @ 12.80 hrs HW=138.77' TW=134.18' (Dynamic Tailwater)

-1=Culvert (Passes 0.52 cfs of 7.53 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.28 cfs @ 5.69 fps)

-3=Sharp-Crested Rectangular Weir (Weir Controls 0.24 cfs @ 0.86 fps)

Summary for Pond 2P: DMH#4

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.44" for 50-YEAR event

Inflow 0.52 cfs @ 12.80 hrs, Volume= 0.10 af

Outflow 0.52 cfs @ 12.80 hrs, Volume= = 0.10 af, Atten= 0%, Lag= 0.0 min

Primary 0.52 cfs @ 12.80 hrs, Volume= 0.10 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 50-YEAR Rainfall=6.72"

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Peak Elev= 134.18' @ 12.80 hrs

Flood Elev= 143.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	133.82'	12.0" Round Culvert
	_		L= 198.7' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 133.82' / 131.83' S= 0.0100 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.52 cfs @ 12.80 hrs HW=134.18' TW=128.06' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.52 cfs @ 2.04 fps)

Summary for Pond 3P: DCB#5

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth > 2.34" for 50-YEAR event

Inflow = 5.59 cfs @ 12.09 hrs, Volume= 0.53 af

Outflow = 5.59 cfs @ 12.09 hrs, Volume= 0.53 af, Atten= 0%, Lag= 0.0 min

Primary = 5.59 cfs @ 12.09 hrs, Volume= 0.53 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 138.80' @ 12.81 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.20'	15.0" Round Culvert
			L= 119.6' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.20' / 135.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013, Flow Area= 1.23 sf

Primary OutFlow Max=5.56 cfs @ 12.09 hrs HW=138.22' TW=136.66' (Dynamic Tailwater)
1=Culvert (Barrel Controls 5.56 cfs @ 4.53 fps)

Summary for Pond 4P: DCB#50

Inflow Area = 0.993 ac, 36.54% Impervious, Inflow Depth > 2.79" for 50-YEAR event

Inflow = 2.51 cfs @ 12.09 hrs, Volume= 0.23 af

Outflow = 2.51 cfs @ 12.09 hrs, Volume= 0.23 af, Atten= 0%, Lag= 0.0 min

Primary = 2.51 cfs @ 12.09 hrs, Volume= 0.23 af

Routing by Dvn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 138.80' @ 12.83 hrs

Flood Elev= 140.38'

Device	Routing	Invert	Outlet Devices
#1	Primary	136.74'	12.0" Round Culvert
			L= 22.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 136.74' / 136.30' S= 0.0200 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=1.89 cfs @ 12.09 hrs HW=138.48' TW=138.23' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.89 cfs @ 2.40 fps)

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Summary for Pond 5P: Infiltration Trench #1

Inflow Area = 0.540 ac, 12.75% Impervious, Inflow Depth > 1.27" for 50-YEAR event

Inflow = 0.39 cfs @ 12.25 hrs, Volume= 0.06 af

Outflow = 0.08 cfs @ 13.19 hrs, Volume= 0.05 af, Atten= 81%, Lag= 56.4 min

Discarded = 0.08 cfs @ 13.19 hrs, Volume= 0.05 af Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.60' @ 13.19 hrs Surf.Area= 1,094 sf Storage= 749 cf

Avail Storage Storage Description

Flood Elev= 141.00' Surf.Area= 1,572 sf Storage= 1,285 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Center-of-Mass det. time= 96.2 min (919.5 - 823.3)

Invort

Volume

volulile		en Ava	II.Storage	Storage Descrip	uori	
#1	138.0	0'	1,285 cf	Custom Stage I	Data (Prismatic) L	isted below (Recalc)
Elevatio		Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
138.0	00	384	0.0	0	0	
140.0	00	384	40.0	307	307	
141.0	00	1,572	100.0	978	1,285	
Device	Routing	In	vert Outl	et Devices		
#1	Primary	140).75' 10.0	long x 4.0' brea	dth Broad-Creste	ed Rectangular Weir
	•			_		1.20 1.40 1.60 1.80 2.00
			2.50	3.00 3.50 4.00	4.50 5.00 5.50	
			Coe	f. (English) 2.38	2.54 2.69 2.68 2	2.67 2.67 2.65 2.66 2.66
			2.68	2.72 2.73 2.76	2.79 2.88 3.07	3.32
#2	Discarde	d 138	3.00' 3.00	0 in/hr Exfiltratio	n over Surface ar	ea

Discarded OutFlow Max=0.08 cfs @ 13.19 hrs HW=140.60' (Free Discharge) 2=Exfiltration (Exfiltration Controls 0.08 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=138.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Infiltration Trench #2

Inflow Area = 0.386 ac, 5.95% Impervious, Inflow Depth > 0.82" for 50-YEAR event
Inflow = 0.20 cfs @ 12.11 hrs, Volume= 0.03 af
Outflow = 0.05 cfs @ 12.64 hrs, Volume= 0.03 af, Atten= 73%, Lag= 31.5 min
Outflow = 0.02 cfs @ 11.76 hrs, Volume= 0.02 af
Primary = 0.03 cfs @ 12.64 hrs, Volume= 0.00 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 138.91' @ 12.64 hrs Surf.Area= 333 sf Storage= 255 cf Flood Elev= 140.00' Surf.Area= 1,369 sf Storage= 1,117 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow)

Type III 24-hr 50-YEAR Rainfall=6.72"

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Center-of-Mass det. time= 93.2 min (947.6 - 854.5)

Volume	Inve	rt Ava	il.Storage	Storage Descr	iption	
#1	137.00)'	1,117 cf	Custom Stage	Data (Prismatic	Listed below (Recalc)
Elevation	n G	Surf.Area	Voids	Inc.Store	Cum.Store	
(fee		(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
				(cubic-leet)	(cabic-leet)	
137.0	00	333	0.0	0	0	
139.0	00	333	40.0	266	266	
140.0	00	1,369	100.0	851	1,117	
Device	Routing	In	vert Ou	tlet Devices		
#1	Primary	138			readth Broad-Cr	ested Rectangular Weir
			He	ad (feet) 0.20 0.	40 0.60 0.80 1.	00 1.20 1.40 1.60
						9 2.68 2.69 2.67 2.64
#2	Discarded	d 137			ion over Surface	

Discarded OutFlow Max=0.02 cfs @ 11.76 hrs HW=137.03' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.02 cfs)

Primary OutFlow Max=0.03 cfs @ 12.64 hrs HW=138.91' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.03 cfs @ 0.26 fps)

Summary for Pond 7P: DMH#3

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.44" for 50-YEAR event
Inflow = 0.52 cfs @ 12.80 hrs, Volume= 0.10 af
Outflow = 0.52 cfs @ 12.80 hrs, Volume= 0.10 af, Atten= 0%, Lag= 0.0 min
Outflow = 0.52 cfs @ 12.80 hrs, Volume= 0.10 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 128.06' @ 12.80 hrs

Flood Elev= 137.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	127.70'	12.0" Round Culvert
			L= 15.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 127.70' / 126.50' S= 0.0800 '/' Cc= 0.900
			n= 0.013. Flow Area= 0.79 sf

Primary OutFlow Max=0.52 cfs @ 12.80 hrs HW=128.06' TW=123.16' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.52 cfs @ 2.04 fps)

Summary for Pond 8P: DMH#2

Inflow Area = 2.736 ac, 28.89% Impervious, Inflow Depth = 0.44" for 50-YEAR event Inflow = 0.52 cfs @ 12.80 hrs, Volume= 0.10 af Outflow = 0.52 cfs @ 12.80 hrs, Volume= 0.10 af, Atten= 0%, Lag= 0.0 min O.52 cfs @ 12.80 hrs, Volume= 0.10 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Type III 24-hr 50-YEAR Rainfall=6.72"
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Peak Elev= 123.16' @ 12.80 hrs

Flood Elev= 130.70'

Device	Routing	Invert	Outlet Devices
#1	Primary	122.80'	12.0" Round Culvert
			L= 10.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 122.80' / 122.00' S= 0.0800 '/' Cc= 0.900
			n= 0.013, Flow Area= 0.79 sf

Primary OutFlow Max=0.52 cfs @ 12.80 hrs HW=123.16' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.52 cfs @ 2.04 fps)

Summary for Link A: Central Street

Inflow Area = 0.366 ac, 20.44% Impervious, Inflow Depth > 2.02" for 50-YEAR event

Inflow = 0.50 cfs @ 12.19 hrs, Volume= 0.06 af

Primary = 0.50 cfs @ 12.19 hrs, Volume= 0.06 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link B: First Brook Tributary

Inflow Area = 1.882 ac, 9.53% Impervious, Inflow Depth > 0.58" for 50-YEAR event

Inflow = 0.55 cfs @ 12.29 hrs, Volume= 0.09 af

Primary = 0.55 cfs @ 12.29 hrs, Volume= 0.09 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Summary for Link C: First Brook

Inflow Area = 7.860 ac, 16.72% Impervious, Inflow Depth > 0.72" for 50-YEAR event

Inflow = 2.48 cfs @ 12.34 hrs, Volume= 0.47 af

Primary = 2.48 cfs @ 12.34 hrs, Volume= 0.47 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow. Time Span= 0.00-24.00 hrs. dt= 0.03 hrs.

2109281-POST DEVELOPMENT FROZEN

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Summary for Pond 5P: Infiltration Trench #1

Inflow Area = 0.540 ac, 12.75% Impervious, Inflow Depth > 1.27" for 50-YEAR event

Inflow = 0.39 cfs @ 12.25 hrs, Volume= 0.06 af

Outflow = 0.27 cfs @ 12.49 hrs, Volume= 0.04 af, Atten= 30%, Lag= 14.5 min

Primary = 0.27 cfs @ 12.49 hrs, Volume= 0.04 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs Peak Elev= 140.80' @ 12.49 hrs Surf.Area= 1,335 sf Storage= 996 cf

Flood Elev= 141.00' Surf.Area= 1,572 sf Storage= 1,285 cf

Plug-Flow detention time= 250.4 min calculated for 0.04 af (62% of inflow)

Center-of-Mass det. time= 116.3 min (939.6 - 823.3)

Volume	lnv	vert Ava	il.Storage	Storage Descrip	otion	
#1	138.	00'	1,285 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevation (fee	1.0	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
138.0		384	0.0	0	0	
140.0	00	384	40.0	307	307	
141.0	00	1,572	100.0	978	1,285	
Device	Routing	ln ln	vert Out	let Devices		
#1	Primary	140				sted Rectangular Weir
			Hea	nd (feet) 0.20 0.4	10 0.60 0.80 1.0	00 1.20 1.40 1.60 1.80 2.00
				3.00 3.50 4.00		_
			Coe	ef. (English) 2.38	2.54 2.69 2.68	2.67 2.67 2.65 2.66 2.66
			2.68	3 2.72 2.73 2.76	3 2.79 2.88 3.07	7 3.32

Primary OutFlow Max=0.27 cfs @ 12.49 hrs HW=140.80' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 0.27 cfs @ 0.54 fps)

2109281-POST DEVELOPMENT_FROZEN

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Summary for Pond 6P: Infiltration Trench #2

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

Inflow Area = 0.386 ac, 5.95% Impervious, Inflow Depth > 0.82" for 50-YEAR event

Inflow = 0.20 cfs @ 12.11 hrs, Volume= 0.03 af

Outflow = 0.22 cfs @ 12.12 hrs, Volume= 0.02 af, Atten= 0%, Lag= 0.8 min

Primary = 0.22 cfs @ 12.12 hrs, Volume= 0.02 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.03 hrs

Peak Elev= 138.94' @ 12.12 hrs Surf.Area= 333 sf Storage= 259 cf

Flood Elev= 140.00' Surf.Area= 1,369 sf Storage= 1,117 cf

Plug-Flow detention time= 170.0 min calculated for 0.02 af (78% of inflow)

Center-of-Mass det. time= 71.6 min (926.1 - 854.5)

Volume	Inv	ert Ava	il.Storage	Storage Descri	ption	
#1	137.0	00'	1,117 cf	Custom Stage	Data (Prismatic)	Listed below (Recalc)
Elevatio (feet		Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
137.0	0	333	0.0	0	0	
139.0	0	333	40.0	266	266	
140.0	0	1,369	100.0	851	1,117	
Device	Routing	In	vert Ou	tlet Devices		
#1	Primary	138	He	ad (feet) 0.20 0.4	40 0.60 0.80 1.0	sted Rectangular Weir 0 1.20 1.40 1.60 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.22 cfs @ 12.12 hrs HW=138.94' TW=0.00' (Dynamic Tailwater) —1=Broad-Crested Rectangular Weir (Weir Controls 0.22 cfs @ 0.51 fps)

APPENDIX

*OPERATION AND MAINTENANCE MANUAL *PRE-DEVELOPMENT DRAINAGE AREA PLAN *POST DEVELOPMENT DRAINAGE AREA PLAN

STORMWATER OPERATION & MAINTENANCE PLAN

Frenette Gardens

Map 182; Lot 3 65 Central Street Hudson, New Hampshire

April 22, 2022



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General Maintenance Requirements

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Long-Term Inspection & Maintenance Plan Checklist
Long-Term Inspection & Maintenance Log
Anti-icing Route Data Form

III. Control of Invasive Plants

Invasive Plant Guide

IV. Stormwater Practice Location Plan

11"x17" "Grading and Drainage Plan"

I. General

Introduction

The project owners or their assigned heirs will maintain the stormwater treatment facilities after construction is completed. The owners of the project are Laura Ripaldi of 46 Bush Hill Road, Hudson, NH 03051, Kimberley Frenette of 8B Dumont Road, Hudson, NH 03051, and Ricky Frenette of 14 Tate Street, Hudson, NH 03051. Peter Ripaldi will be responsible for the reporting, inspection, and maintenance activities identified in this report. He can be reached at (603) 557-6510.

The subject property is referenced on Hudson's Tax Map 182 as Lot 3. Any transfer of responsibility for inspection and maintenance activities or transfer of ownership shall be documented to the Town of Hudson in writing. The contract documents will require the contractor to designate a person responsible for maintenance of the sedimentation control features during construction. Long-term operation and maintenance for the stormwater management facilities are presented below.

Maintenance will be performed as described and required in this document unless and until the system is formally accepted by a municipality or quasi-municipal district or is placed under the jurisdiction of a legally created association that will be responsible for the maintenance of the system.

Post Construction:

The following standards will be met after construction is complete:

Documentation:

A maintenance log will be kept summarizing inspections, maintenance, and any corrective actions taken. The log will include the date on which each inspection or maintenance task was performed, a description of the inspection findings or maintenance completed, and the name of the inspector or maintenance personnel performing the task. If a maintenance task requires the clean out of any sediments or debris, the location where the sediment and debris was disposed after removal will be indicated. The log will be made accessible to department and/or Town staff and a copy provided upon request.

Maintenance Requirements

Subsurface Systems:

- Removal of accumulated sediment.
- Systems should be inspected at least twice annually with maintenance or rehabilitation conducted as warranted by such inspection.
- Trash and debris should be removed at each inspection.
- At least once annually, the system should be inspected for drawdown time.
 If the pond does not drain within 72-hours following a rainfall event, a
 qualified professional should assess the condition of the facility to determine
 measures required to restore filtration function or infiltration function (as
 applicable), including but not limited to the removal of accumulated
 sediments or reconstruction of the filter media.
- For more specific maintenance requirement for the Stormtech system follow all the manufactures requirements.

Isolator Rows:

- Inspect Isolator Row for Sediment
 - A) Inspection ports (if present)
 - i. Remove lid from floor box frame.
 - ii. Remove cap from inspection riser.
 - iii. Using a flashlight and stadia rod, measure the depth of sediment and record results on maintenance log.
 - iv. If sediment is at, or above, 3 inch depth, clean out Isolator Row using the JetVac Process.
 - B) All Isolator Rows
 - i. Remove cover from manhole at upstream end of Isolator Row.
 - ii. Using a flashlight, inspect down Isolator Row through outlet pipe. (Mirrors on poles or cameras may be used to avoid confined space entry). Follow OSHA regulations for confined space entry if entering manhole.
 - iii. If sediment is at or above the lower row of sidewall holes (approximately 3 inches) clean out Isolator Row using the JetVac Process.
- Clean out Isolator Row using the JetVac Process
 - A) A fixed culvert cleaning nozzle with rear facing nozzle spread of 45 inches or more is preferable
 - B) Apply multiple passes of JetVac until backflush water is clean
 - C) Vacuum manhole sump as required
- Replace all caps, lids and covers, record observations and actions
- Inspect & clean catch basins and manholes upstream of the StormTech system

Infiltration Trenches:

- Systems should be inspected at least twice annually, and following any rainfall event exceeding 2.5 inches in a 24-hour period, with maintenance or rehabilitation conducted as warranted by such inspection.
- Trash and debris should be removed at each inspection.

- Inspection of pre-treatment measures at least twice annually and removal of accumulated sediment as warranted by inspection, but no less than once annually.
- At least once annually, the system should be inspected for drawdown time.
 If the pond does not drain within 72-hours following a rainfall event, a
 qualified professional should assess the condition of the facility to determine
 measures required to restore filtration function or infiltration function (as
 applicable), including but not limited to the removal of accumulated
 sediments or reconstruction of the basin bottom.

Catch Basins and Closed Drainage Network:

- Catch basins may require frequent maintenance. This may require several cleanings of the sumps each year. At a minimum, it is recommended that catch basins be inspected at least twice annually.
- Sediment should be removed when it approaches half of the sump depth.
- If floating hydrocarbons are observed during an inspection, the material should be removed immediately by skimming, absorbent materials, or other methods and disposed in conformance with the applicable state and federal regulations.

Level Spreaders:

- Systems should be inspected at least annually with maintenance or rehabilitation conducted as warranted by such inspection.
- Remove debris and accumulated sediment when exceeds 25% of spreader depth. Disposal of sediment to be done properly.
- Repair eroded areas; remove invasive species and dead vegetation.
- Perform periodic mowing.
- Snow should not be stored within or down-slope of the level spreader.
- Repair any erosion and re-grade was warranted by inspection.
- Reconstruct the spreader if down-slope channelization indicates that the spreader is not level or that discharge has become concentrated, and corrections cannot be made through minor re-grading.

General:

- If any invasive species begin to grow in the stormwater management practices the species shall be disposed of in an appropriate manner that will not allow the pest to survive or spread. The disposal of such species shall be witnessed or approved by a state inspector. Methods for disposal may include, but not be limited to:
 - Encapsulating the plant(s) in plastic bags and disposing of the plant material in one of the following ways:
 - Trash pickup;
 - Discarding;
 - Open burning:
 - Incineration; or
 - Burial of infested nursery.

II. Supporting Documents

Annual Inspection and Maintenance Reporting Form Frenette Gardens

Hudson, New Hampshire

Date:	·	
To:	Project Owner	
Re:	Certification of Inspection and Maintenand	ce; Submittal of Forms
Prope	erty Name:	
Prope	erty Address:	
Conta	act Name:	
Conta	act Phone #:	
	act Email Address:	
have assoc	y that the required stormwater facility inspection been completed in accordance with the Orditated with the above referenced property. Equired Long-Term Inspection & Maintenance form.	peration & Maintenance Plan
	of Party Responsible for Inspection ntenance	Property Owner
Autho	rized Signature	Signature

Long-Term Inspection & Maintenance Plan Checklist Frenette Gardens – Hudson, NH

Current Owner Name:			Date	e:				
Business Address:			Insp	ector:				
Weather:								
Date of Last Rainfall:			Amo	ount:		Inc	hes:	
Best Management Practice								
Subsurface Infiltration System			Rea	son for	· Ins	pection	on	
	Spring		Fall	Fall/Yearly ☐ After Major S				
Maintenance Required? Corrective Action Needed & Notes:	Yes 🗆	١	No					
Visual inspection of drawdown time? Drawdown time less than 72 hours? (if no, call a qualified professional for insp	Yes ☐ Yes ☐ pection)		No No					
Isolator Rows			Reas	son for	Insp	pectio	n	
	Corios	\neg	Eall/	Yearly		۸ ش	Major	Storm 🖂
	Spring	\sqcup	гаш	Carry	ш	Aπer	iviajoi	о.о <u>П</u>
Stadia Rod Readings: Observations/Actions:	Fixed Poil		Chai Top	mber B	otto imei	m – nt		
	Fixed Poi		Chai Top Sed	mber B of Sedi	otto imei Depi	m – nt th = _		
Observations/Actions:	Fixed Poi		Char Top Sed	mber B of Sedi iment [otto imer Depi	m _ nt th = _ pectio	n	
Observations/Actions:	Fixed Poi	nt to	Char Top Sed	mber B of Sedi liment [otto imer Depi	m _ nt th = _ pectio	n	
Observations/Actions: Infiltration Trench #1 Maintenance Required?	Fixed Point Fixed Fixed Point Fixed	nt to	Char Top Sed Reas	mber B of Sedi liment [otto imer Depi	m _ nt th = _ pectio	n	

Infiltration Trench #2	Reason for Inspection		
	Spring ☐ Fall/Yearly ☐ After Major Storm ☐		
Maintenance Required? Corrective Action Needed & Notes:	Yes No		
Visual Inspection of vegetation? Maintenance Required? Corrective Action Needed & Notes:	Yes No Yes No		
Visual inspection of drawdown time? Drawdown time less than 72 hours? (if no, call a qualified professional for insp	Yes No Section)		
Catch Basins & Closed Drainage			
Network	Spring Fall/Yearly After Major Storm		
Maintenance Required? Corrective Action Needed & Notes:	Yes 🗆 No 🗆		
Level Spreaders	Reason for Inspection		
	Spring ☐ Fall/Yearly ☐ After Major Storm ☐		
Maintenance Required? Corrective Action Needed & Notes:	Yes No 🗆		
Need Repairs?	Yes □ No □		
General	Reason for Inspection		
	Spring ☐ Fall/Yearly ☐ After Major Storm ☐		
Maintenance Required? Corrective Action Needed & Notes:	Yes □ No □		

Long-Term Inspection & Maintenance Log Frenette Gardens – Hudson, NH

Date	Inspection (Yes or No)	Maintenance (Yes or No)	List BMPs Inspected and/or Provide Comments	Inspected By:
-				

Anti-icing Route Data Form Frenette Gardens – Hudson, NH

Truck Station:				
Date:				
Temperature:	Pavement Temperature:	Relative Humidity:	Dew Point:	Sky:
Reason For Ap	pplying:			
Route:				
Chemical:				
Application Tim	ne:			
Application Am	ount:			
Observation (fi				
Observation (a	fter event):			
Observation (b	efore next application):			
Name:				

III. Control of Invasive Plants

Invasive plants are introduced, alien, or non-native plants, which have been moved by people from their native habitat to a new area. Some Exotic plants are imported for human use such as landscaping, erosion control, or food crops. They also can arrive as "hitchhikers" among shipments of other plants, seeds, packing materials, or fresh produce. Some exotic plants become invasive and cause harm by:

- becoming weedy and overgrown;
- killing established shade trees;
- obstructing pipes and drainage systems;
- forming dense beds in water;
- lowering water levels in lakes, streams, and wetlands;
- destroying natural communities;
- promoting erosion on stream banks and hillsides; and
- resisting control except by hazardous chemical.

During maintenance activities, check for the presence of invasive plants and suitably remove according to the methods provided in the table below. The following table, based on the "Control of Invasive Plants" published by the New Hampshire Department of Agriculture, describes the most common invasive plants in this region and proper methods of disposal.

Name	Description	Invasive Qualities	Control Methods

	Invasive Trees			
Norway Maple	- Large leaves - Will exude milky white sap when leaves are broken - Leaves turn color in Late October (fall foliage is yellow)	- Suppresses growth of grass, garden plants, and forest understory -Wind-borne seeds can germinate and grow in deep shade	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out plants, including the root systems. Use a forked spade or weed wrench. Cut down the tree. Grind out the stump, or clip off re-growth. Girdle¹ Frill² Cut stem/ cut stump with glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Foliar spray with glyphosate ³* (mid-October to early November). 	
Tree of Heaven	- Long compound leaves with 11-25 lance shaped leaflets - Smell like peanut butter or burnt coffee when crushed	- Tough, can grow in poor conditions - Produces large quantities of wind-borne seeds - Grows rapidly - Secretes a toxin that kills other plants - Cannot be removed by mechanical means alone	 Pull seedlings when soil is moist. Frill² (no more than 1" gap between cuts). Use Garlon 3a herbicide. Cut stem/ cut stump with Garlon 3a. Follow label directions for cut stump application. Clip off sucker sprouts or paint with Garlon 3a.* Foliar spray³* (on regrowth) Paint bottom 12" of bark with Garlon 4 Ultra (February/March). Use maximum strength specified on label for all herbicide applications. 	

	Invasive Shrubs				
Autumn Olive	- Formerly recommended for erosion control and wildlife value	- Highly invasive, diminishes the overall quality of wildlife habitat	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs (up to 4" diameter trunks). Cut down the tree. Grind out the stump, or clip off re-growth. Cut stem/ cut stump with glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Bury stump Do not mow 		

Invasive Shrubs (continued)			
Multiflora Rose	- Formerly recommended for erosion control, hedges, and wildlife habitat - Covered in white flowers in June - Very hard, curved thorns - Fringed edge to leaf stalk	- Huge shrub that chokes out all other vegetation - Too dense for most birds to nest in - Grows up trees like a vine in Shade	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems (at least 6" from the crown and 6" down). Use a forked spade or weed wrench for trees or shrubs. Controlled burning⁴ (on extensive infestations) Cut stem/ cut stump with glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Foliar spray^{3*} (mix Rodeo with extra sticker-spreader, or use Roundup Sure Shot Foam on small plants) Herbicide may be applied in winter when other plants are dormant.
Bush Honeysuckles	- Includes Belle, Amur, Morrow's, and Tatarian Honeysuckle	- Creates dense shade reducing plant diversity and eliminating nest sites in forest interior spaces	 Deadhead to prevent spread of seeds (on ornamentals). Cut off seeds or fruits before they ripen. Bag and burn, or send to a landfill. Pull seedlings and small or shallowrooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Mow or cutting at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year (on shady sites only, brush cut in early spring and fall). Controlled burning⁴ (during growing season) Cut down the tree. Grind out the stump, or clip off re-growth. Cut stem/ cut stump with Glyphosate (late in the growing season). Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.*

Invasive Shrubs (continued)			
Blunt-Leaved Privet	- Medium sized shrub - Simple, oblong, dark green leaves 1-2" in length - Fragrant white flowers (spring) - Blackish-purple fruit (late summer)	- Toxic to mammals - Loss of valuable habitat	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Cut down the tree. Grind out the stump, or clip off re-growth. Cut stem/ cut stump with Glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Trim off all flowers Do not cut back or mow
Burning Bush, Winged Euonymus	- Wide, corky wings on the Branches - Brilliant red autumn leaves - Fruit	- High seed production	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Cut down the tree. Grind out the stump, or clip off re-growth. Cut stem/ cut stump with Glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Trim off all flowers
Japanese Barberry	- Spiny deciduous shrub - Small leaves	- Very dense, displaces native plants - Can change chemistry of soil	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Cut down the tree. Grind out the stump, or clip off re-growth. Cut stem/ cut stump with Glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Trim off all flowers

Invasive Woody Vines			
Japanese Honeysuckle	- Gold and White flowers - Heavy scent and sweet nectar in June	- Shade shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle - Rampant grower - Spirals around trees, often strangling them	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Mow or cutting at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year. Cut stem/ cut stump with Glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Foliar spray^{3*} (fall or early spring when native vegetation is dormant) Plan to re-treat repeatedly
Oriental Bittersweet	- Bright orange seed capsules in clusters all along the stem - Flowers	- Shade shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle	 Pull seedlings and small or shallow-rooted plants when soil is moist. Dig out larger plants, including the root systems. Use a forked spade or weed wrench for trees or shrubs. Keep ornamental plants cut back, remove all fruits as soon as they open, and bag or burn fruits. Cut stem/ cut stump with Garlon 3a. Follow label directions for cut stump application. Clip off sucker sprouts or paint with Garlon 3a.*
Japanese Knotweed, Mexican Bamboo	- The stems have knotty joints, similar to bamboo - Grows 6-10' tall - Large, pointed oval or triangular leaves	- Shade shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle - Can grow in shade	- Cut stem/ cut stump with Glyphosate (at least 3 times each during growing season). Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* - Foliar spray ^{3*} - Treat with Rodeo - In gardens, heavy mulch or dense shade may kill it.

Invasive Herbaceous Plants			
Garlic Mustard	- White-flowered biennial - Rough scalloped leaves (kidney, heart, or arrow shaped) - Garlic smell, mustard taste when its leaves are crushed	- Shade shrubs and young trees of the forest understory, eventually killing them, and changing the open structure of the forest into a dense tangle - Rampant grower - Spirals around trees, often strangling them	 Pull seedlings and small or shallow-rooted plants when soil is moist (before it flowers in spring). Dig out larger plants, including the crown and root systems. Use a forked spade or weed wrench for trees or shrubs. Tamp down soil afterwards. Deadhead to prevent spread of seeds. Cut off seeds or fruits before they ripen. Bag and burn or send to a landfill. Foliar spray³* (may be appropriate in some settings)
Japanese Stilt Grass	- Lime green color - Line of silvery hairs down the middle of the 2-3" long blade	- Tolerates sun or dense shade -Quickly invades areas left bare or disturbed by tilling or flooding - Builds a large seed bank in the soil	 Pull seedlings and small or shallow-rooted plants when soil is moist (pulled easily in early to midsummer). Dig out larger plants, including root systems. Use a forked spade or weed wrench for trees or shrubs. Be sure to pull before it goes to seed. If seeds have formed, bag and burn or send to a landfill. Mow or cutting at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year. Mowing weekly or when it has just begun to flower may prevent it from setting seed. Foliar spray³* (use glyphosate or herbicidal soap on large infestations. Use a corn-based pre-emergence herbicide on annual weeds (spring). This product is also an organic fertilizer, i.e., it can stimulate growth of existing plants, including weeds, so it is appropriate for lawns and gardens but may not be appropriate in woodlands.

	Invasive He	rbaceous Plants (continu	ed)
Mile-A-Minute Vine, Devil's Tail Tearthumb	- Triangular leaves - Barbed stems - Turquoise berries	- Rapid growth - Quickly covers and shades out herbaceous plants	 Pull seedlings and small or shallow-rooted plants when soil is moist (pulled easily in early to midsummer). Dig out larger plants, including root systems. Use a forked spade or weed wrench for trees or shrubs. Be sure to pull before it goes to seed. If seeds have formed, bag and burn or send to a landfill. Mow or cutting at least 4 times a season to deplete plants' store of nutrients and carbohydrates, reduce seed formation, and kill or minimize spread of plants. If necessary, repeat each year. Mowing weekly or when it has just begun to flower may prevent it from setting seed. Foliar spray³* (use glyphosate or herbicidal soap on large infestations. Use a corn-based pre-emergence herbicide on annual weeds (spring). This product is also an organic fertilizer, i.e., it can stimulate growth of existing plants, including weeds, so it is appropriate for lawns and gardens but may not be appropriate in woodlands.
Spotted Knapweed	- Thistle-like flowers	- Dense, crowds out native species	 Do not pull unless the plant is young and the ground is very soft. The root will break and produce several new plants. Wear sturdy gloves Deadhead to prevent spread of seeds. Cut off seeds or fruits before they ripen. Bag and burn, or send to a landfill. In lawns, spot treat with broad-leaf weed killer. Good lawn care practices (test soil; use lime and fertilizer only when soil test shows a need; mow high and frequently; leave clippings on lawn) reduce weed infestations. Cut stem/ cut stump with Glyphosate. Follow label directions for cut stump application. Clip off sucker sprouts or paint with glyphosate.* Foliar spray^{3*}

<u>1Girdle:</u> Cut through the bark and growing layer all around the trunk, about 6" above the ground. Girdling is most effective in spring (when the sap is rising) & middle-late summer (when the tree is sending food to the roots). Clip off sucker sprouts.

²<u>Frill:</u> Using a machete, hatchet, or similar device, hack scars (several holes in larger trees) downward into the growing layer, and squirt in glyphosate (or triclopyr if specified in table). Follow label directions for injection and frill applications. This is most effective from middle to late summer. Clip off any sucker sprouts or treat with glyphosate.

<u>*Foliar Spray:</u> Use a backpack or garden sprayer or mist blower, following label directions. Avoid overspray and/or dripping onto non-target plants, because glyphosate kills most plants except moss. If it rolls off waxy or grass-like foliage, use additional sticker-spreader. Deciduous trees, shrubs, and perennials move nutrients down to the roots in late summer. Glyphosate is particularly effective at this time and when plants have just gone out of flowering. Several invasive species retain their foliage after native plants have lost theirs, and resume growth earlier in spring than most natives. This allows you to treat them without harming the natives. However, the plant must be actively growing for the herbicide to work. Retreatments may be necessary the following year if suckering occurs or the plant hasn't been entirely killed.

<u>4Controlled Burning:</u> Burning during the spring (repeated over several years) will allow native vegetation to compete more effectively with the invasive species. This requires a permit. Spot treatment with glyphosate in late fall can be used to make this method more effective

*Herbicides: It is highly recommended that small populations try to be controlled using non-chemical methods where feasible. However, for large infestations, and for a few plants herbicide use is essential. Apply herbicides carefully to avoid non-target plants, glyphosate is the least environmentally damaging herbicide in most cases. Add food coloring for visibility, and a soap-based sticker such as Cide-Kick. Glyphosate is ineffective on some plants; for these, triclopyr or Garlon 3a may be indicated. When using herbicides read the entire label and observe all precautions listed, including proper disposal. If in doubt, call your local Cooperative Extension Service.

